

# **Optoelectronică, structuri și tehnologii**

Curs 5  
2014/2015

# Fotografii

**Studentii care au trimis fotografiile 📸**

**Grupa: 5402**

**Grupa: 5403**

**Grupa: 5404**

**Grupa: 5405**

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Nr.	Nume
1	ALEXANDRESCU SEBASTIAN

Nr.	Nume
1	APERGHIS MIHAI-ALIN

Nr.	Nume
1	ANGHELUS MARIL

**Studentii care **inca** nu au trimis fotografiile 📸**

**Grupa: 5304**

**Grupa: 5402**

**Grupa: 5403**

**Grupa: 5404**

Nr.	Nume

Nr.	Nume

Nr.	Nume

Nr.	Nume

# Reprezentare logaritmică

$$\text{dB} = 10 \cdot \log_{10} (P_2 / P_1)$$

$$\text{dBm} = 10 \cdot \log_{10} (P / 1 \text{ mW})$$

$$0 \text{ dB} = 1$$

$$+ 0.1 \text{ dB} = 1.023 (+2.3\%)$$

$$+ 3 \text{ dB} = 2$$

$$+ 5 \text{ dB} = 3$$

$$+ 10 \text{ dB} = 10$$

$$-3 \text{ dB} = 0.5$$

$$-10 \text{ dB} = 0.1$$

$$-20 \text{ dB} = 0.01$$

$$-30 \text{ dB} = 0.001$$

$$0 \text{ dBm} = 1 \text{ mW}$$

$$3 \text{ dBm} = 2 \text{ mW}$$

$$5 \text{ dBm} = 3 \text{ mW}$$

$$10 \text{ dBm} = 10 \text{ mW}$$

$$20 \text{ dBm} = 100 \text{ mW}$$

$$-3 \text{ dBm} = 0.5 \text{ mW}$$

$$-10 \text{ dBm} = 100 \mu\text{W}$$

$$-30 \text{ dBm} = 1 \mu\text{W}$$

$$-60 \text{ dBm} = 1 \text{ nW}$$

$$[\text{dBm}] + [\text{dB}] = [\text{dBm}]$$

$$[\text{dBm}/\text{Hz}] + [\text{dB}] = [\text{dBm}/\text{Hz}]$$

$$[x] + [\text{dB}] = [x]$$

# Lumina ca undă electromagnetică

Capitolul 2

# Parametri, dependenta de mediu

$$\eta_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 377\Omega$$

$$c_0 = \frac{1}{\sqrt{\epsilon_0 \cdot \mu_0}} = 2,99790 \cdot 10^8 \text{ m/s}$$

$$n = 1$$

$$T = \frac{2\pi}{\omega} = \frac{1}{f}$$

$$\lambda_0 = \frac{2\pi}{\beta} = \frac{c_0}{f}$$

$$\eta = \frac{\eta_0}{n}$$

$$c = \frac{c_0}{n}$$

$$n = \sqrt{\epsilon_r}$$

$$T = \frac{2\pi}{\omega} = \frac{1}{f}$$

$$\lambda = \frac{c_0}{n \cdot f} = \frac{\lambda_0}{n}$$

ITU G.692

"the allowed channel frequencies are based on a 50 GHz grid with the reference frequency at 193.10 THz"

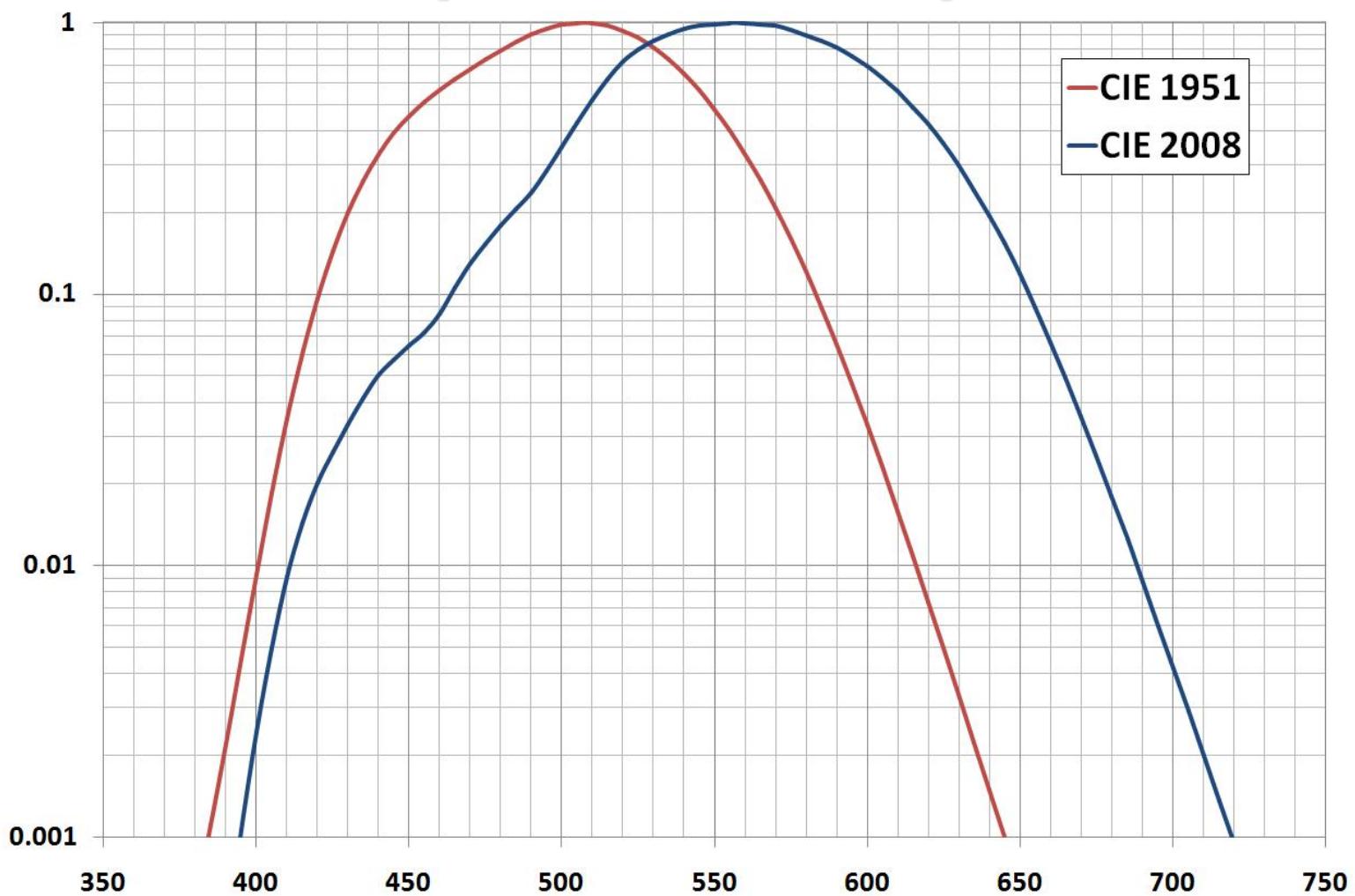
SI

"a source that emits monochromatic radiation of frequency  $540 \cdot 10^{12}$  Hz"

# Fotometrie și radiometrie

Capitolul 4

# CIE $V(\lambda)$ fotopic / scotopic



# Marimi luminoase

## ▶ Intensitatea

- raportul dintre fluxul care părăsește sursa și se propagă într-un element de unghi solid ce conține direcția de propagare și elementul de unghi solid.
- o masura a puterii emise de o sursa într-un element de unghi solid

Intensitatea			
Fotometrie		Radiometrie	
$I_v = \frac{d\Phi_v}{d\Omega}$	SI: cd	$I_e = \frac{d\Phi_e}{d\Omega}$	SI: W/sr

# Marimi luminoase

## ▶ Iluminarea

- raportul dintre fluxul primit de un element de suprafață conținînd punctul și aria acestui element (definită într-un punct al unei suprafete la receptie):
- o masura a intensitatii luminii incidente pe o suprafata

Iluminarea			
Fotometrie		Radiometrie	
$E_v = \frac{d\Phi_v}{dS}$	SI: lx	$E_e = \frac{d\Phi_e}{dS}$	SI: W/m <sup>2</sup>

# Probleme

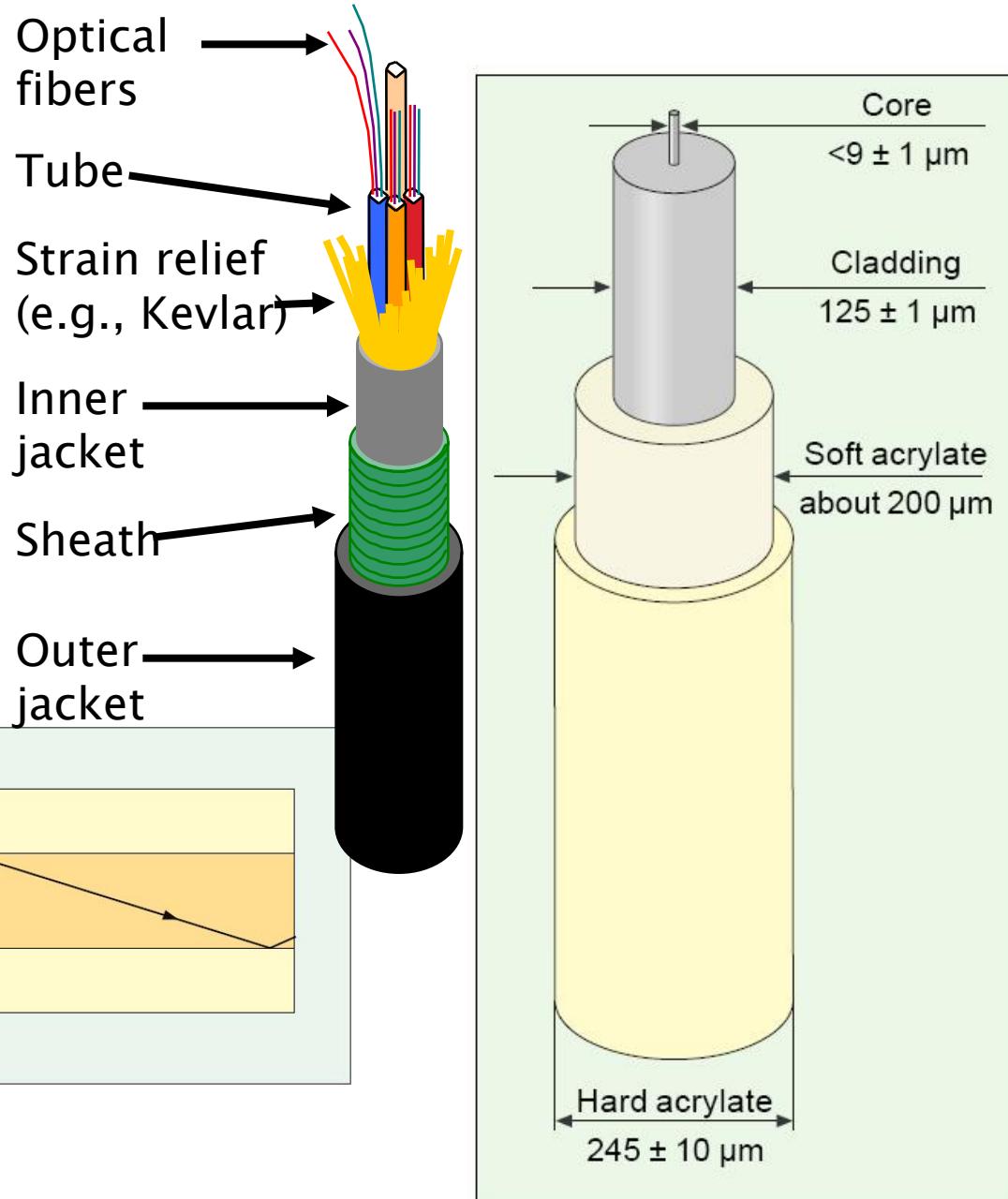
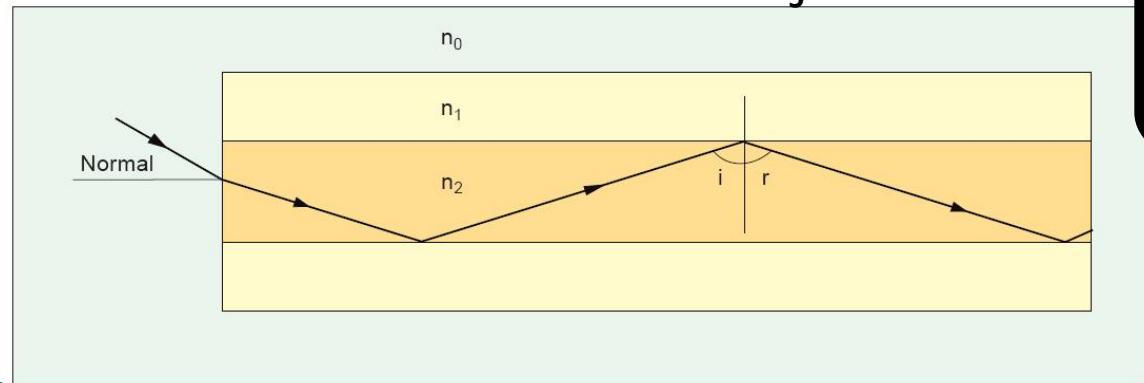
- ▶ Trebuie să proiectați un semafor cu LED-uri. LED-urile care intră în compoñența sa sunt caracterizate de eficiență cuantică egală (aceeași tehnologie), iar parametrii de catalog pentru LED-ul roșu sunt ...
- ▶ Proiectați semaforul, pentru a obține o iluminare la 5m, pe direcție normală, de 50 lx pe timp de zi și 2 lx pe timp de noapte.
- ▶ Cerințe: luminozitate egală pentru cele 3 culori, alegerea numărului de LED-uri (considerente electronice/practice), necesitățile de curent ale fiecărui LED, parametrii pentru sursa de alimentare, parametrii unui sistem de control a intensității luminoase pentru reglare zi/noapte.
- ▶ Rezolvari: <http://rf-opto.etti.tuiasi.ro>

# Fibra optică

Capitolul 5

# Fibra optica

- ▶ un ghid de unda dielectric
  - miez
  - teaca



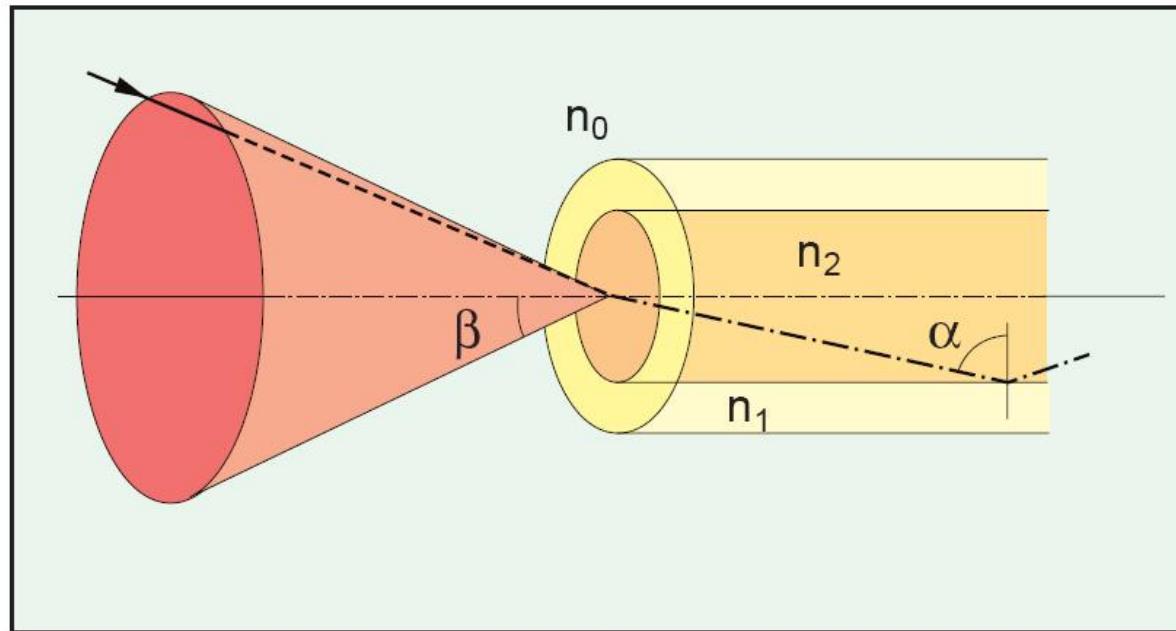
# Unghi de acceptanta, apertura numerica

- ▶ Unghi de acceptanta

$$n_0 \cdot \sin \theta_{ACC} = n_2 \cdot \sin \phi_c$$

- ▶ Apertura numerica

$$NA = n_0 \cdot \sin \theta_{ACC}$$

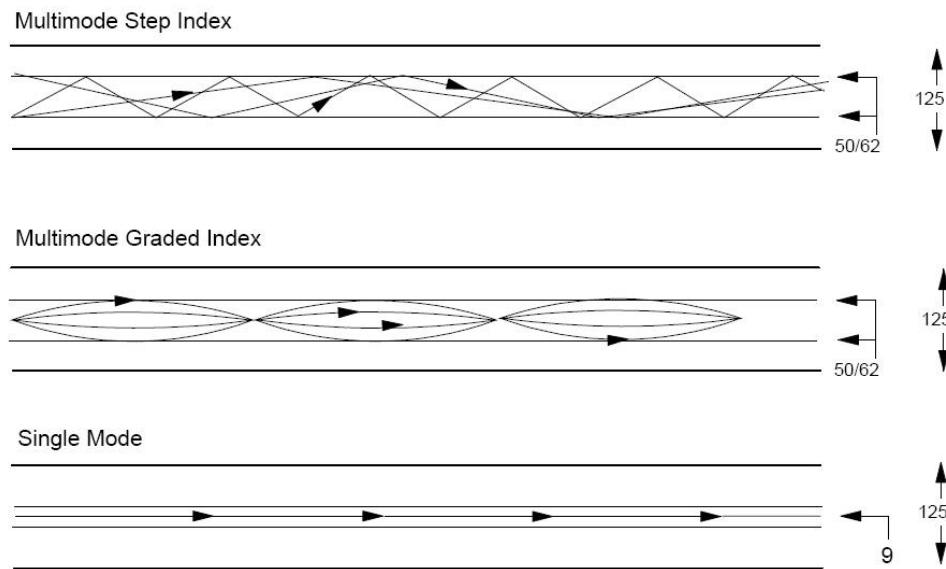
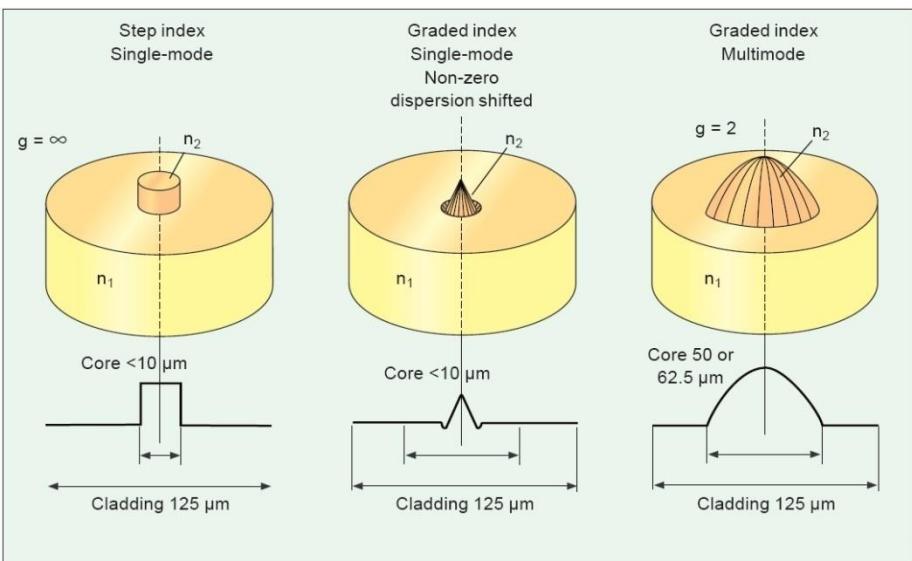
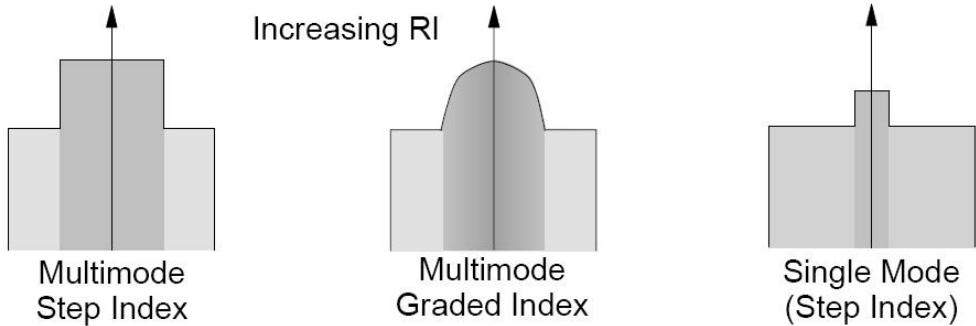


$$NA = n_2 \sqrt{\frac{n_2^2 - n_1^2}{n_2^2}} = \sqrt{n_2^2 - n_1^2}$$

$n_2$  – miez  
 $n_1$  – teaca  
 $n_2 > n_1 !!$

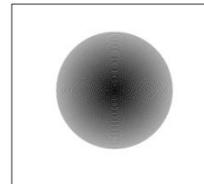
# Tipuri de fibra

- ▶ Monomod
- ▶ Multimod
  - cu salt de indice
  - cu indice gradat

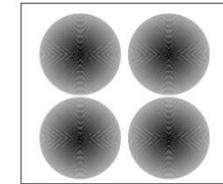


# Moduri in fibra

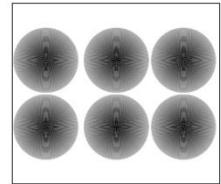
- ▶ Moduri in ghid rectangular



TEM<sub>00</sub>

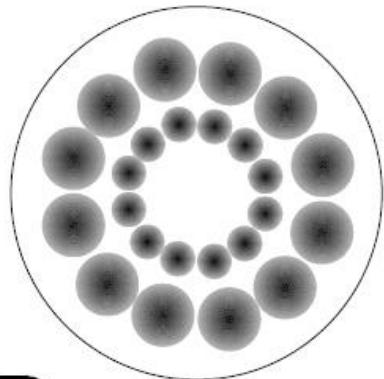


TEM<sub>11</sub>

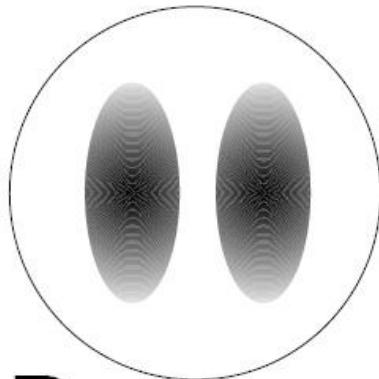


TEM<sub>21</sub>

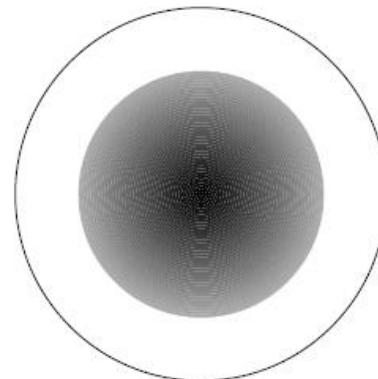
- ▶ Moduri linear polarizate in fibra



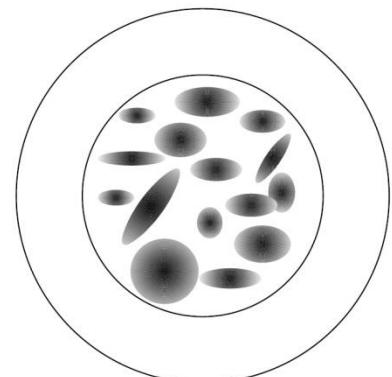
LP<sub>62</sub>



LP<sub>11</sub>



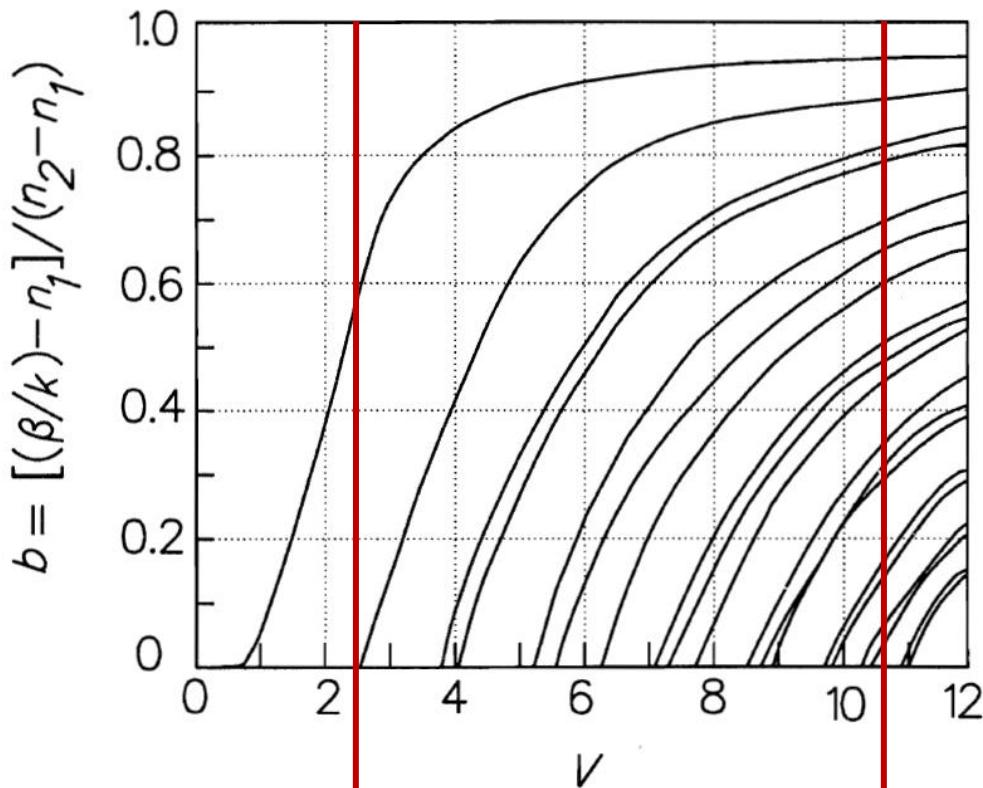
LP<sub>01</sub>



"Sparkle" pattern

# Frecventa normalizata – monomod

## ► Fibre monomod



$b$  – coeficient de propagare modal relativ

$$V \leq V_C = 2.405$$

există un singur mod (solutii fc. Bessel)

$$\lambda \geq \lambda_C = \pi \frac{2a}{V_C} NA = \pi \frac{2a}{2.405} NA$$

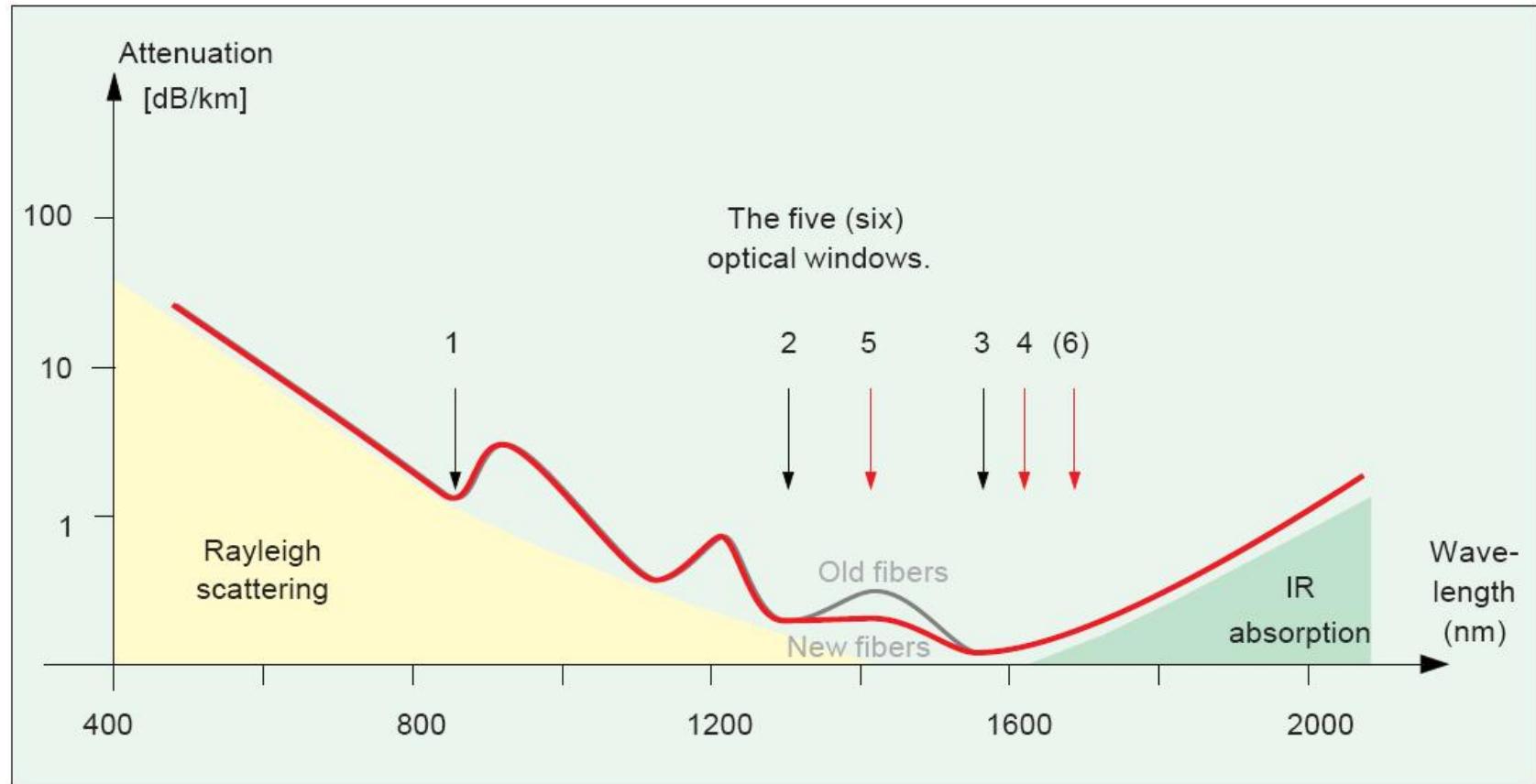
Exemplu:  
 $2a = 8.5 \mu\text{m}$   
 $NA = 0.11$

$$\lambda_C = \pi \frac{8.5}{2.405} 0.11 = 1210 \text{ nm}$$

# ATENUAREA

- ▶ Macrocurburi
- ▶ Microcurburi
- ▶ Imprastiere
- ▶ Absorbtie

# Absorbtie



# Calculul atenuarii

$$\text{Pierderi} = \frac{P_{out}}{P_{in}}$$



$$\text{Pierderi [dB]} = [-] 10 \cdot \log_{10} \left( \frac{P_{out}}{P_{in}} \right)$$

$$\text{Pierderi [dB]} = [-] (P_{out} [\text{dBm}] - P_{in} [\text{dBm}])$$



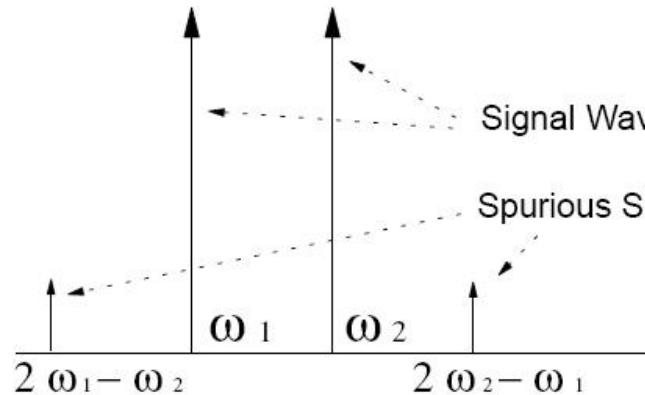
$$\text{Atenuare [dB/km]} = \frac{\text{Pierderi [dB]}}{\text{lungime [km]}}$$

# Efecte neliniare in fibra

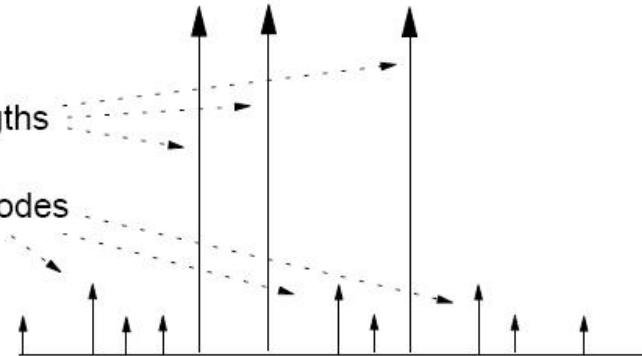
- ▶ Stimulated Brillouin Scattering, SBC
  - difractia luminii inspre emitator datorita undelor mecano-acustice generate in fibra
  - 6–10 dBm
- ▶ Stimulated Raman Scattering, SRS
  - interactiunea luminii cu vibratiile moleculare
  - 27 dBm (~1W)
- ▶ Self Phase Modulation, SPM
  - Frontiera impulsului implica indice de refractie variabil in timp moduland faza impulsului
  - 5 dBm
  - Cross Phase Modulation, CPM
- ▶ Four-Wave Mixing, FWM
  - 0 dBm

# Four-Wave Mixing, FWM

Two Channels



Three Channels

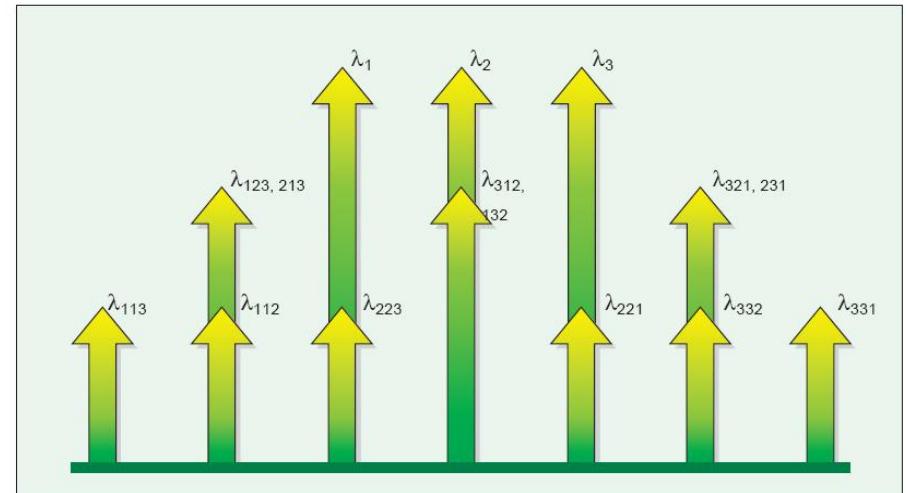


$$NL = \frac{1}{2} (N^3 - N^2)$$

$N = 2, NL = 4$

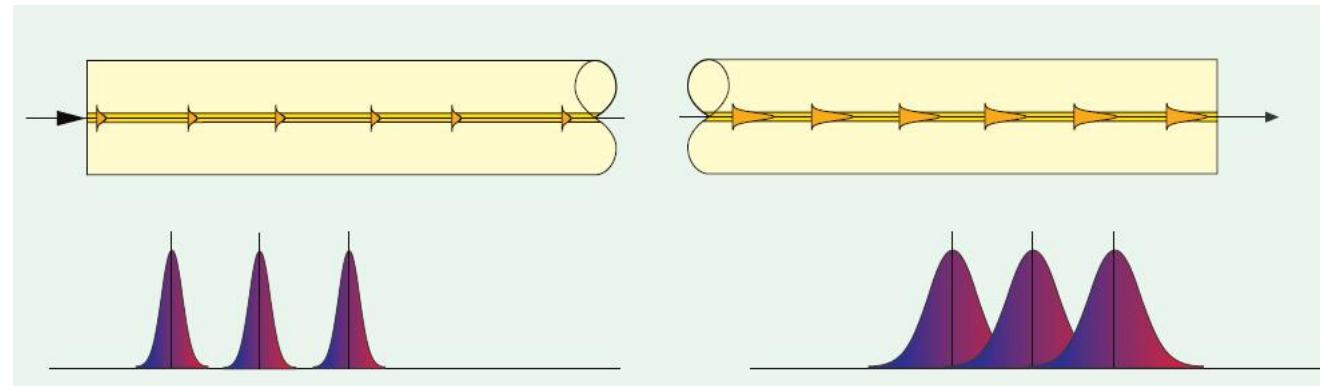
$N = 3, NL = 9$

$N = 16, NL = 1920$

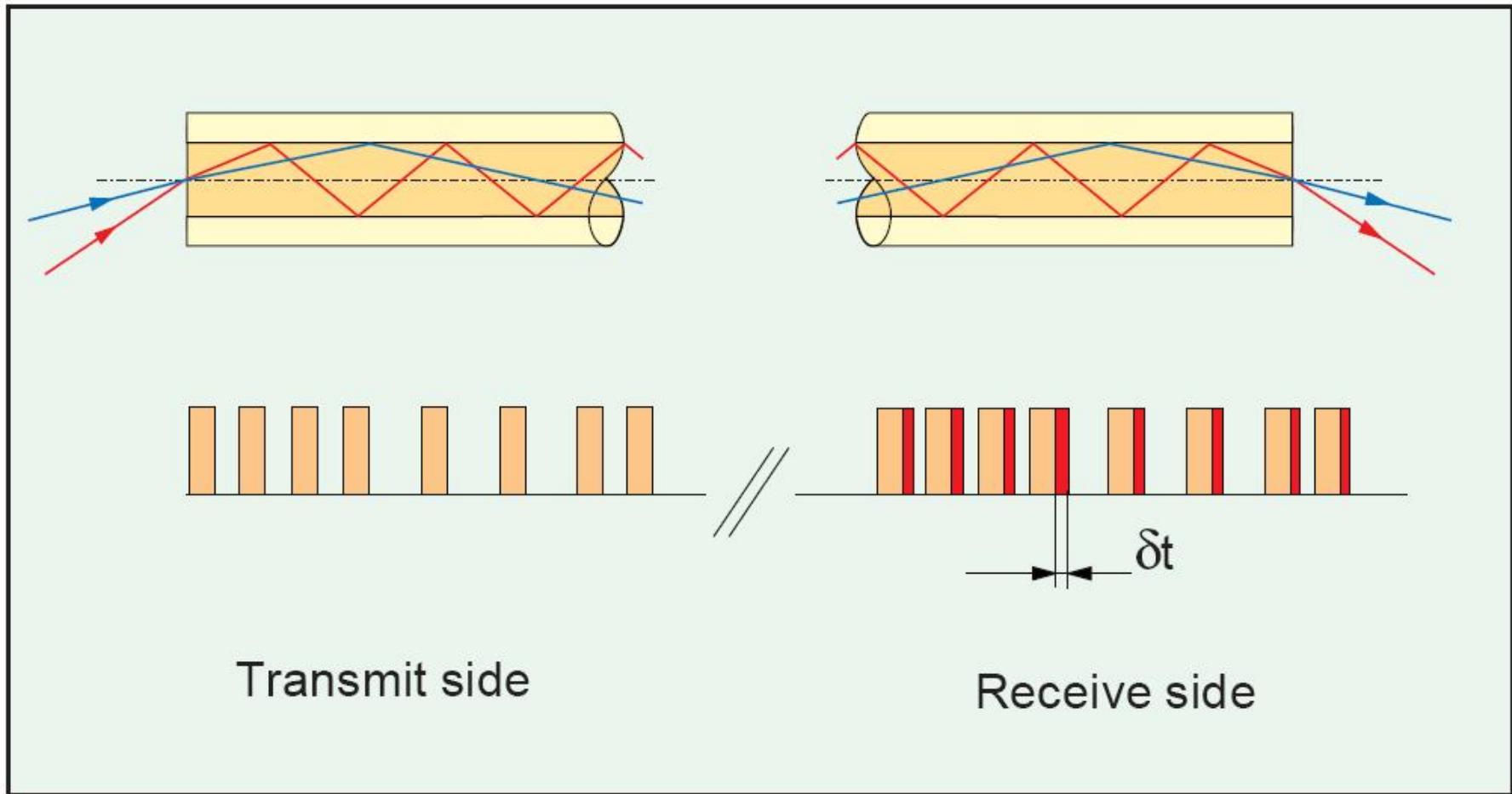


# Dispersia

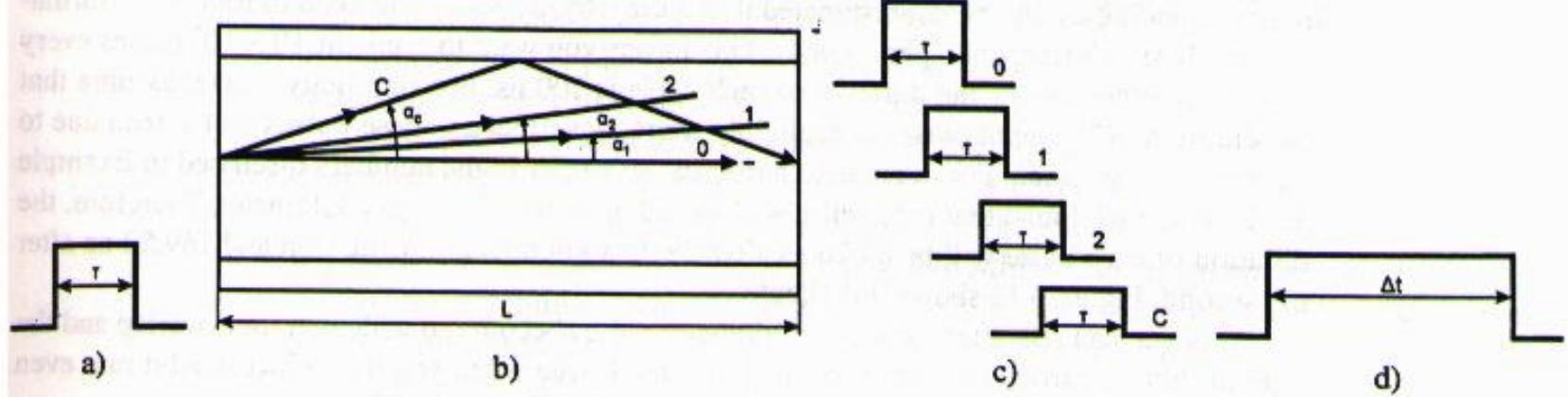
- ▶ Propagarea cu viteze diferite a radiatiilor cu lungimi de unda diferite
  - intermodala (modala – depinde de prezența modurilor)
  - intramodala (cromatică – depinde de lungimea de undă)
    - de material
    - de ghid



# Dispersia modala



# Dispersia modala



$$t_0 = \frac{L}{v}$$

$$t_C = \frac{L}{v \cdot \cos \alpha_C}$$

$$v = \frac{c}{n_2}$$

$$\cos \alpha_C = NA$$

$$\Delta t_{SI} = t_C - t_0 = \frac{L \cdot n_2}{c} \cdot \left( \frac{n_2 - n_1}{n_2} \right)$$

$$\Delta = \frac{n_2 - n_1}{n_1} \ll 1$$

$$\Delta t_{SI} = t_C - t_0 = \frac{L \cdot n_2}{c} \cdot \Delta$$

$$\Delta t_{SI} = t_C - t_0 \approx \frac{L}{2 \cdot c \cdot n_2} \cdot (NA)^2$$

# Dispersia modala

## ► salt de indice

$$dt = \frac{L \cdot n_2^2}{c \cdot n_1} \left( \frac{n_2 - n_1}{n_2} \right) \approx \frac{L \cdot NA^2}{2 \cdot c \cdot n_2}$$

intarzierea intre  
moduri cand

$$\Delta = \frac{n_2 - n_1}{n_1} \ll 1$$

$$\Delta \tau_{\text{mod}}^2 = \frac{1}{3} \left( \frac{dt}{2} \right)^2$$

$$\Delta \tau_{\text{mod}} \approx \frac{L \cdot n_2 \cdot \Delta}{2\sqrt{3} \cdot c} \approx \frac{L \cdot NA^2}{4\sqrt{3} \cdot c \cdot n_2}$$

## ► indice gradat

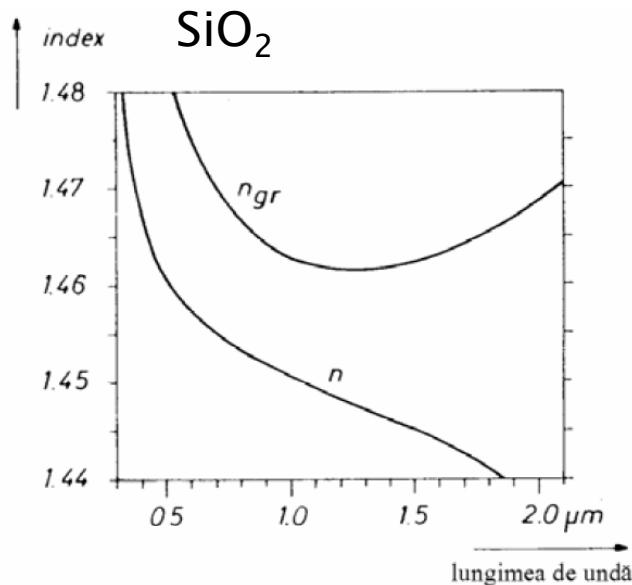
$$dt = \frac{L \cdot n_2 \cdot \Delta^2}{2c} \approx \frac{L \cdot NA^4}{8 \cdot c \cdot n_2^3}$$

$$NA = 0.1 \div 0.2 < 1$$

$$\Delta \tau_{\text{mod}} \approx \frac{L \cdot n_2 \cdot \Delta^2}{4\sqrt{3} \cdot c}$$

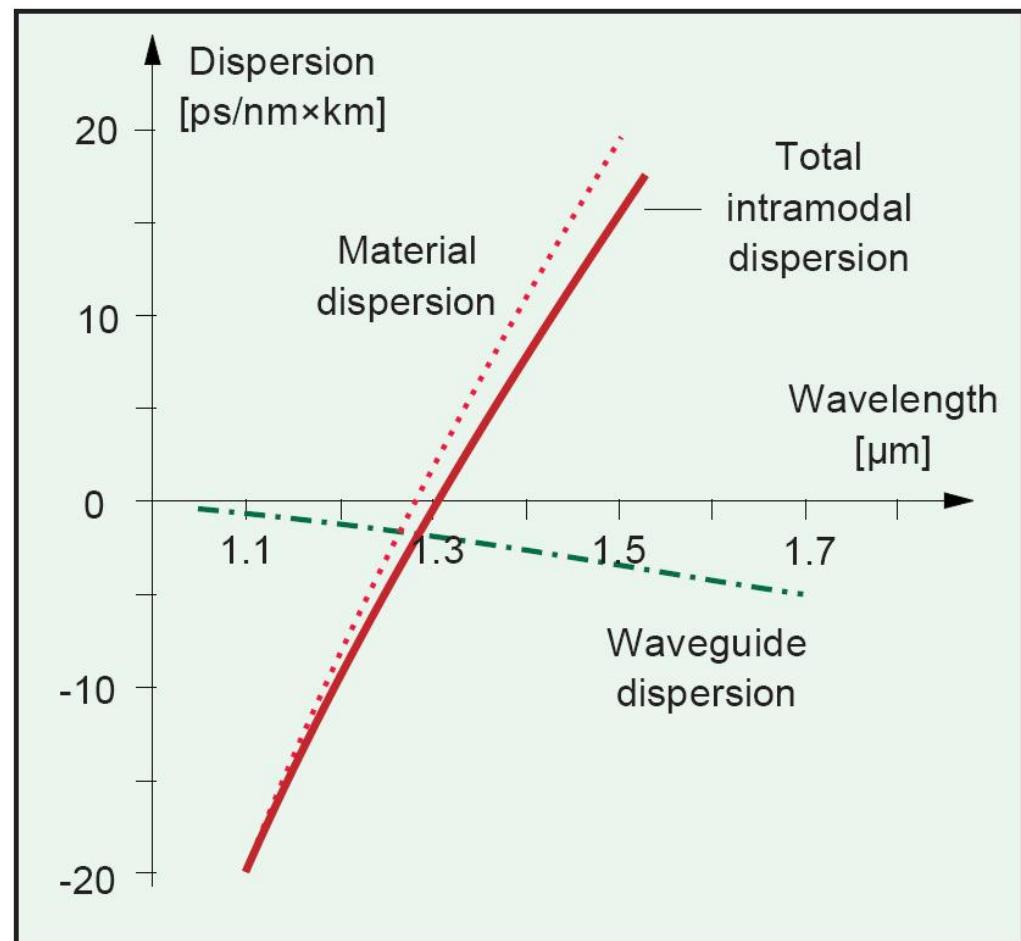
$n_2$  - miez  
 $n_1$  - teaca  
 $n_2 > n_1 !!$

# Dispersia de material



$$n_{gr} = n - \lambda \frac{dn}{d\lambda}$$

$$\Delta\tau_{mat} = \frac{L \cdot \lambda \cdot \Delta\lambda}{c} \cdot \frac{d^2n}{d\lambda^2}$$

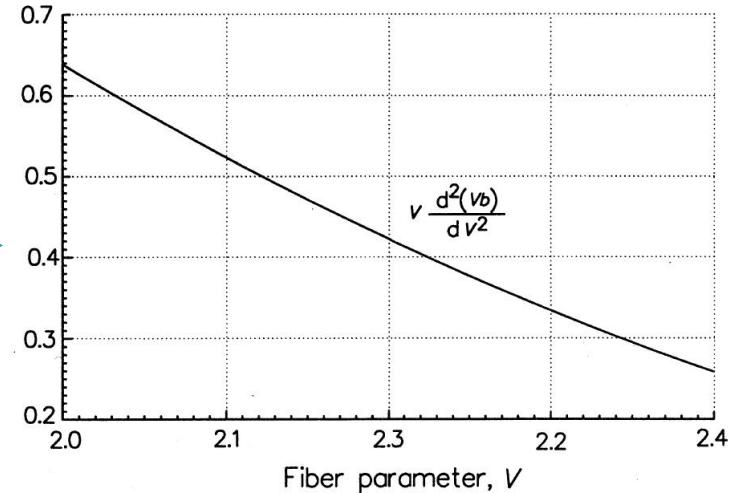
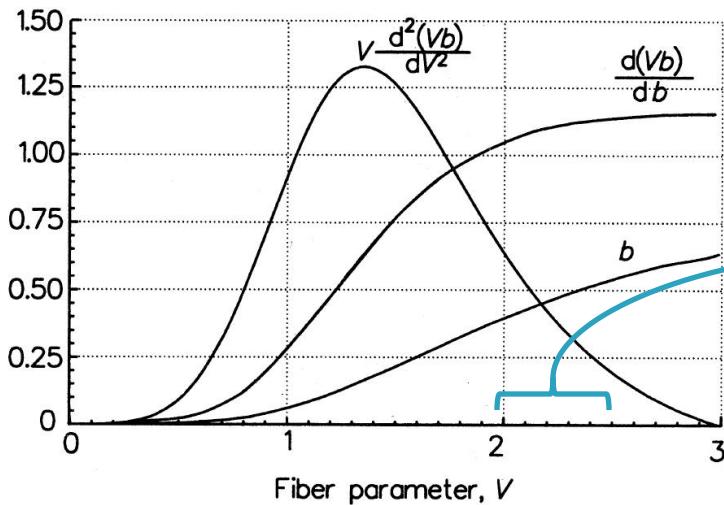


# Dispersia de ghid

- ▶ Neglijabila in fibrele multimod fata de dispersia modală

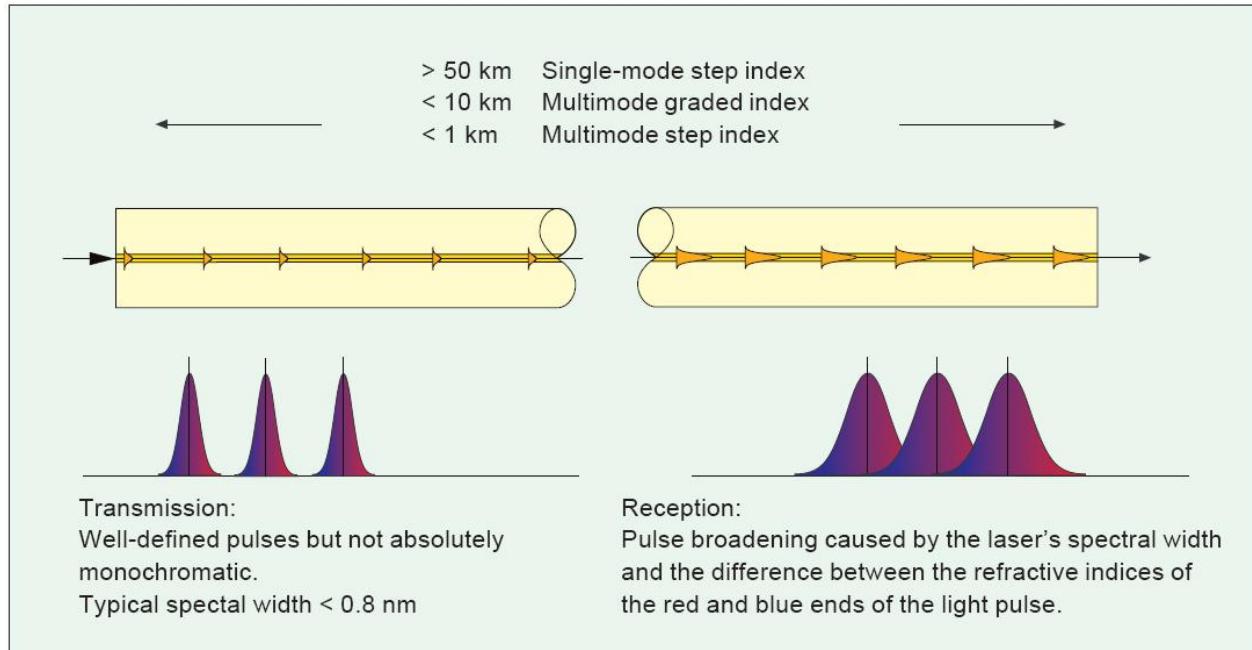
$$\Delta\tau_{gh} = \frac{n \cdot L \cdot \Delta}{c} \cdot \frac{\Delta\lambda}{\lambda} \cdot \left( V \frac{d^2(Vb)}{dV^2} \right)$$

b - constanta de propagare  
normalizata



$$V \leq V_C = 2.405$$

# Dispersia cromatica (gh+mat)



$$\Delta\tau_{cr} = D(\lambda) \cdot \Delta\lambda \cdot L$$

$$D(\lambda) = \frac{S_0}{4} \cdot \left( \lambda - \frac{\lambda_0^4}{\lambda^3} \right)$$

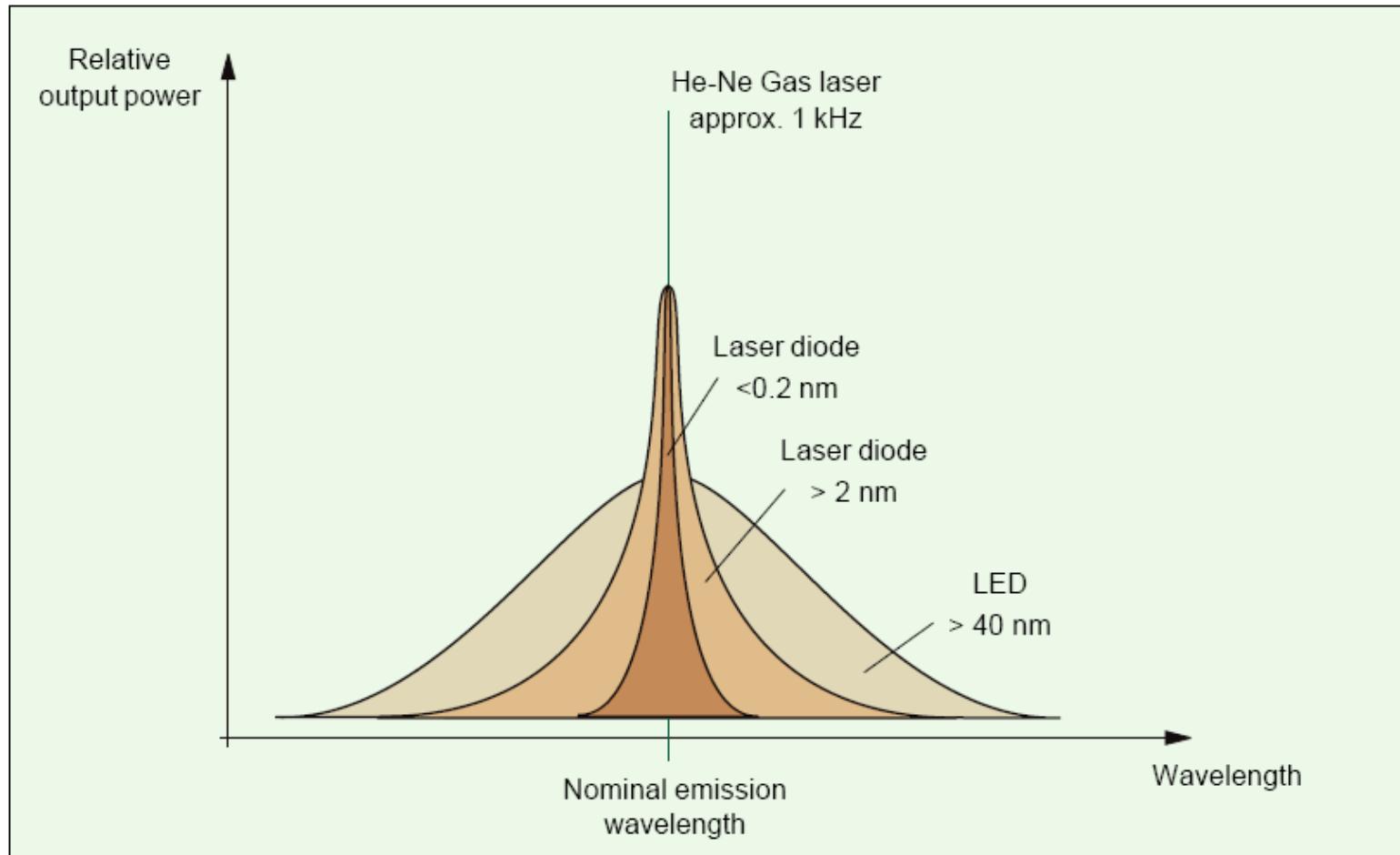
$S_0$  panta dispersiei –  
 $\text{ps}/\text{nm}^2/\text{km}$

$$D(\lambda_0) = 0$$

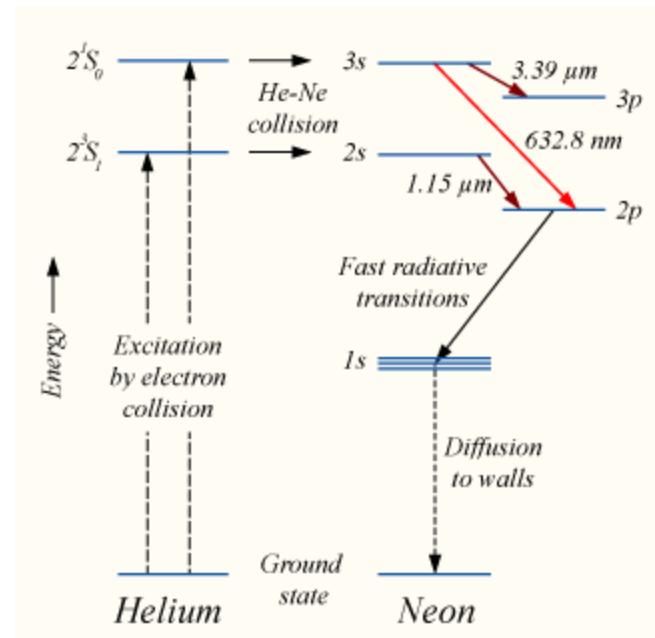
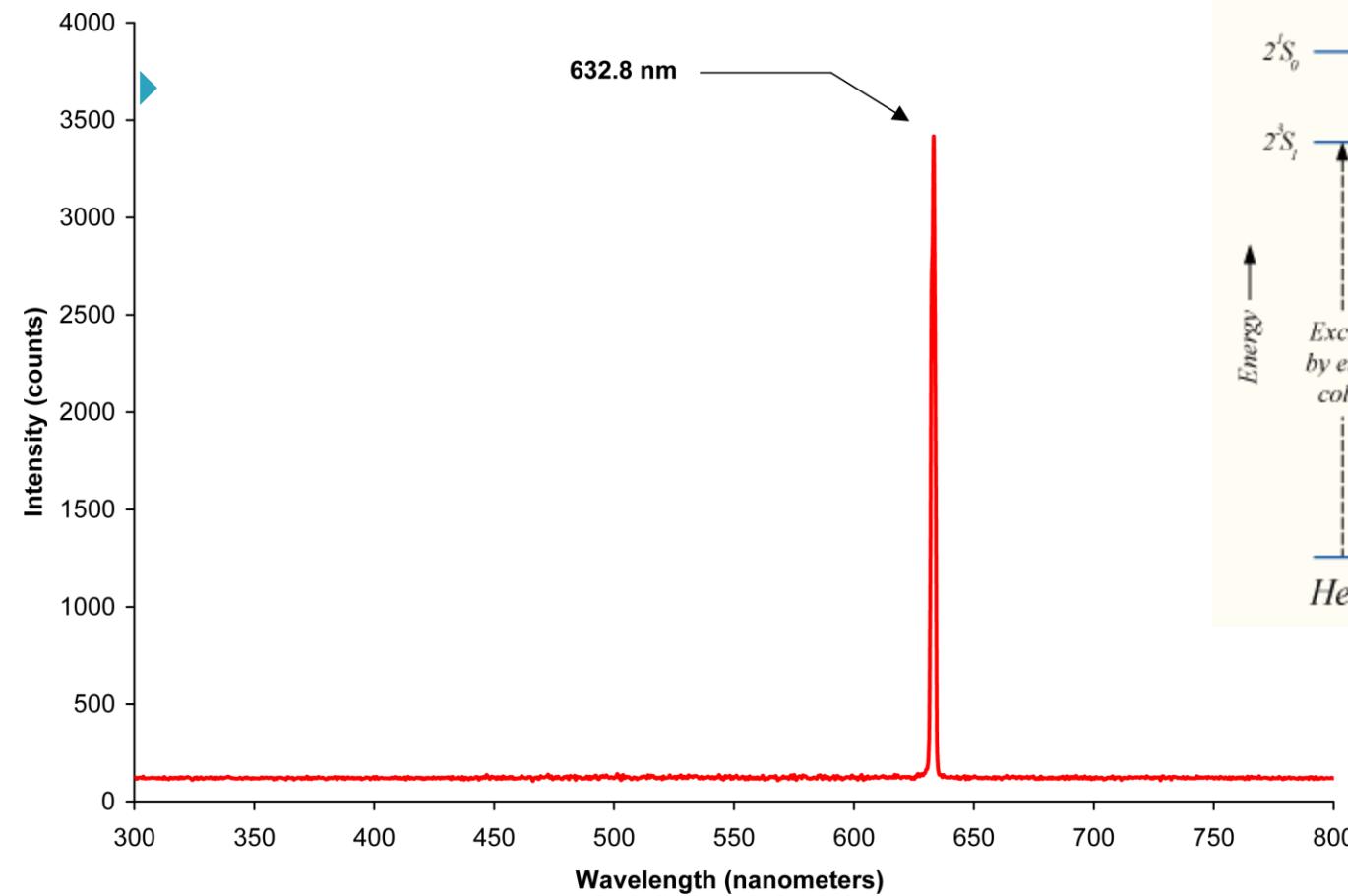
- ▶  $D(\lambda) \approx 100 + 0.4 (850 - \lambda)$  [ps/nm/km]  
pentru  $800 < \lambda < 900$  nm
- ▶  $D(\lambda) \leq 3,5$  ps/nm/km  
pentru  $1285 < \lambda < 1330$  nm
- ▶  $D(\lambda) \leq 17$  ps/nm/km  
pentru  $1525 < \lambda < 1575$  nm

$$D(\lambda) = \frac{S_0}{4} \cdot \left( \lambda - \frac{\lambda_0^4}{\lambda^3} \right)$$

# Calitatea spectrală a emițătorilor optici



# He-Ne Laser



$$\Delta\lambda = 0.002 \text{ nm}$$

# Banda

- ▶ Dispersia totală

$$\Delta\tau_{tot} = \sqrt{\Delta\tau_{cr}^2 + \Delta\tau_{mod}^2}$$

- ▶ Banda

$$B_{opt} = \frac{0.44}{\Delta\tau_{tot}[ns]} \quad [GHz]$$

- ▶ Banda optică la 3 dB corespunde unei benzi electrice la 6 dB

- $P_{opt} \sim I; \quad P_{el} \sim I^2$

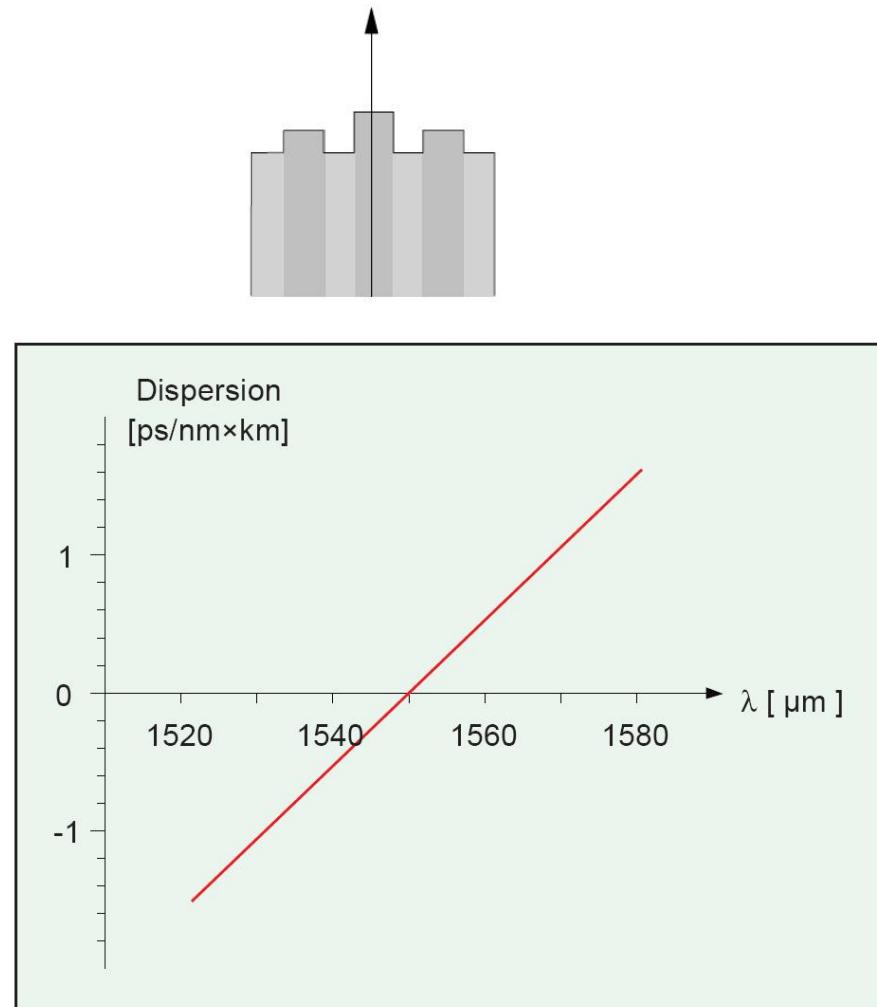
$$B_{opt} = \sqrt{2}B_{el}$$

- ▶ Viteză legăturii

$$V[Gb/s] \cong 2 \cdot B_{el}[GHz]$$

# Dispersion shifted fibers

- ▶ Atenuarea e mai mica la 1550 nm
- ▶ EDFA (Erbium doped fibre amplifiers) opereaza in banda aceasta
- ▶ Sistemele WDM (Wavelength division Multiplexing) necesita banda larga amplificata



# Catalog

## How to Order

Contact your sales representative, or call the Optical Fiber Customer Service Department  
 Ph: 607-248-2000 (U.S. and Canada)  
 +44-1244-287-437 (Europe)  
 Email: [opticalfiber@corning.com](mailto:opticalfiber@corning.com)  
 Please specify the fiber type, attenuation and quantity when ordering.

## Mechanical Specifications

### Proof Test

The entire fiber length is subjected to a tensile stress  $\leq 100$  kpsi (0.7 GPa)\*.  
 \*Higher proof test levels available.

### Length

Fiber lengths available up to 50.4\* km/spool.  
 \*Longer spliced lengths available.

## Performance Characterizations

Characterized parameters are typical values.

Core Diameter	8.2 $\mu\text{m}$
Numerical Aperture	0.14
	<i>N.A. is measured at the one percent power level of a one-dimensional point source at 1310 nm.</i>
Zero Dispersion Wavelength ( $\lambda_0$ )	1317 nm
Zero Dispersion Slope ( $S_0$ )	0.088 ps/(nm <sup>2</sup> ·km)
Effective Group Index (at 1310 nm)	1310 nm: 1.4670 1550 nm: 1.4750
Fatigue Resistance Parameter (N <sub>f</sub> )	20
Coating Strip Force	Dry: 0.6 lbs. (3N) Wet, 14-day room temperature: 0.6 lbs. (3N)
Rayleigh Backscatter Coefficient (for 1 ns Pulse Width)	1310 nm: -77 dB 1550 nm: -82 dB
Stimulated Brillouin Scattering Threshold	20 dBm <sup>0</sup>

Note:

(1) When characterized with a transmitter specifying 17 dBm SBS threshold over standard single-mode fiber. While absolute SBS threshold is a function of distance and signal format, NextCor fiber offers a 3 dB improvement over standard single-mode fiber independent of these variables.

## Formulas

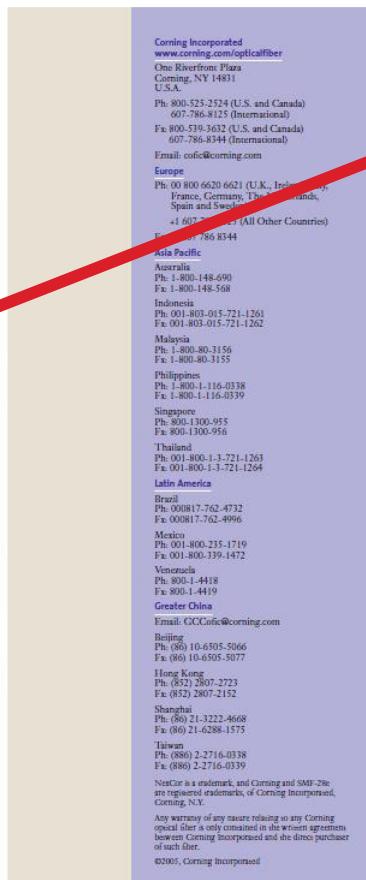
### Dispersion

$$\text{Dispersion } D(\lambda) = \frac{S_0}{4} \left[ \lambda - \frac{\lambda_0^2}{\lambda} \right] \text{ ps}/(\text{nm} \cdot \text{km}), \text{ for } 1200 \text{ nm} \leq \lambda \leq 1625 \text{ nm}$$

$\lambda$  = Operating Wavelength

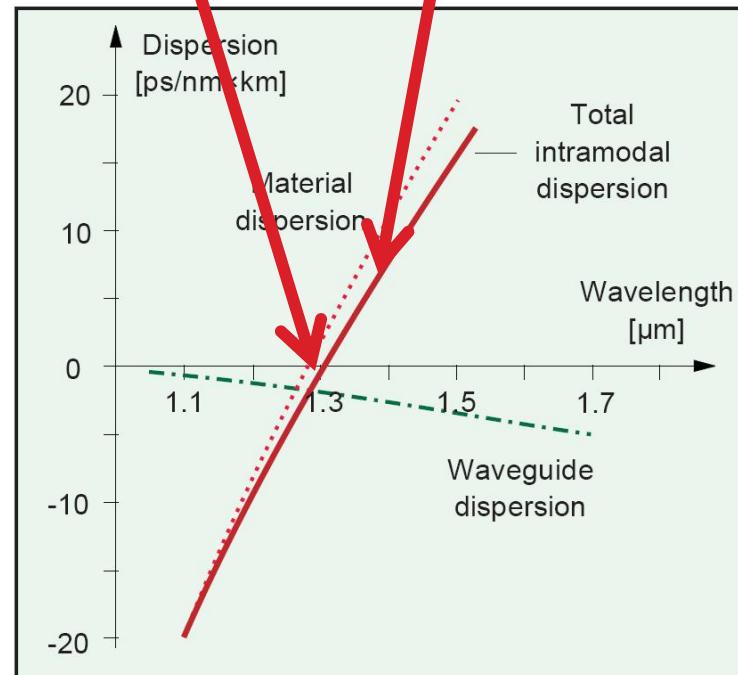
### Cladding Non-Circularity

$$\text{Cladding Non-Circularity} = \left[ \frac{\text{Min. Cladding Diameter}}{\text{Max. Cladding Diameter}} \right] \times 100$$

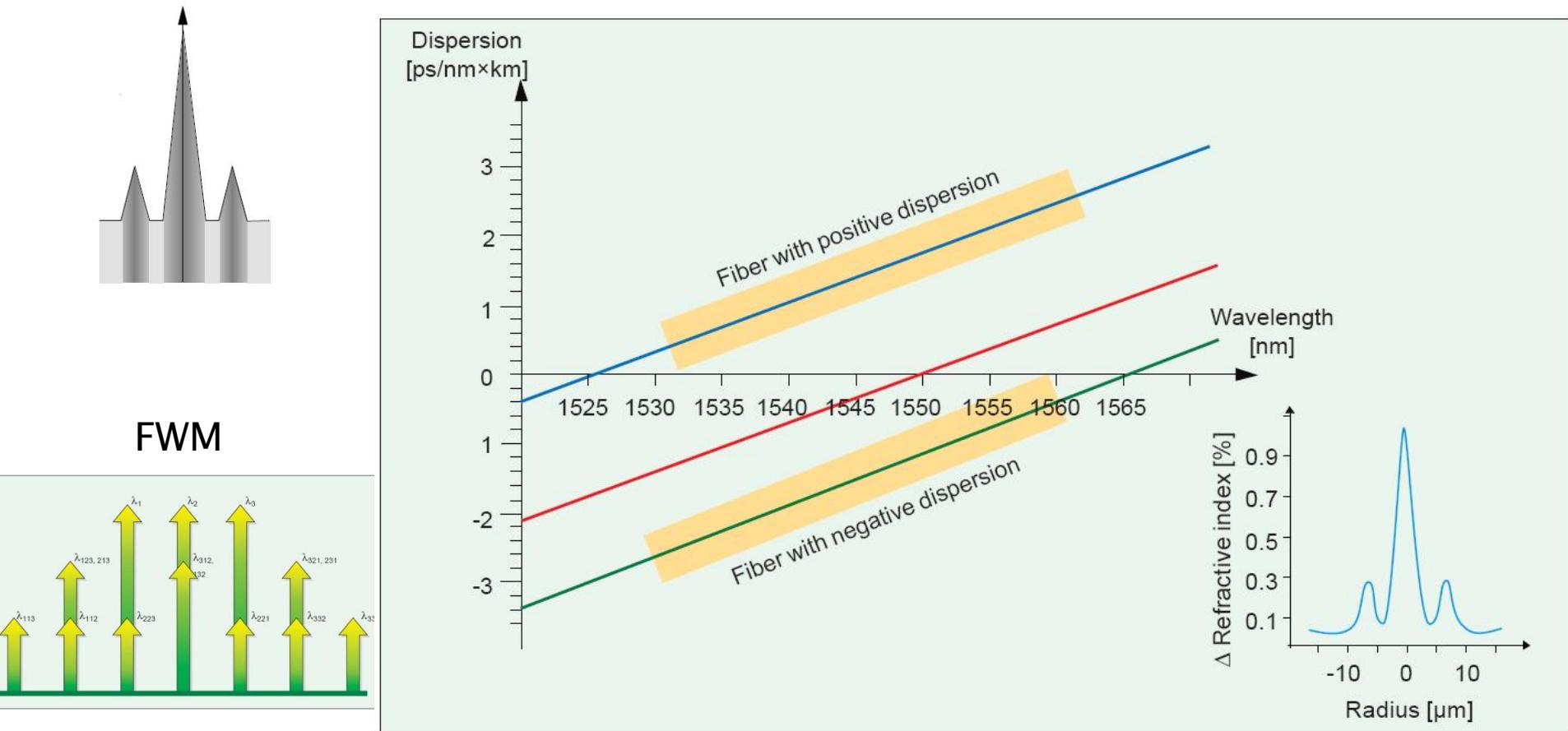


*far-field scan at 1510 nm*

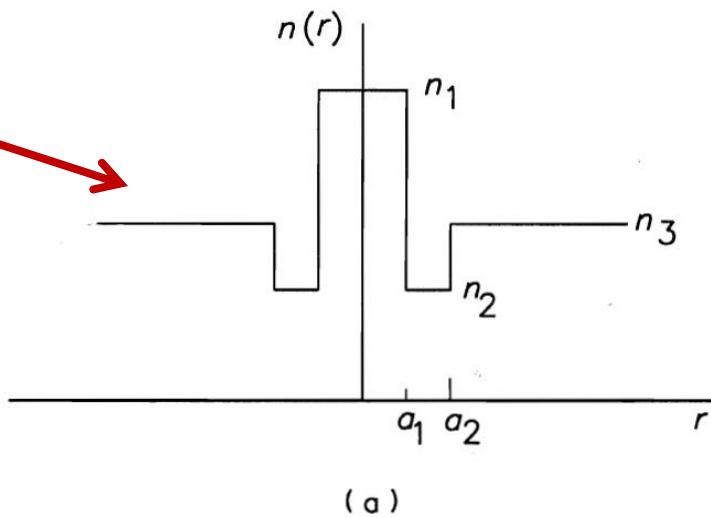
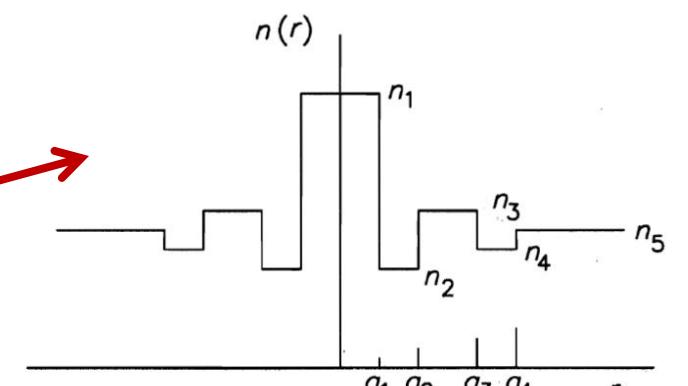
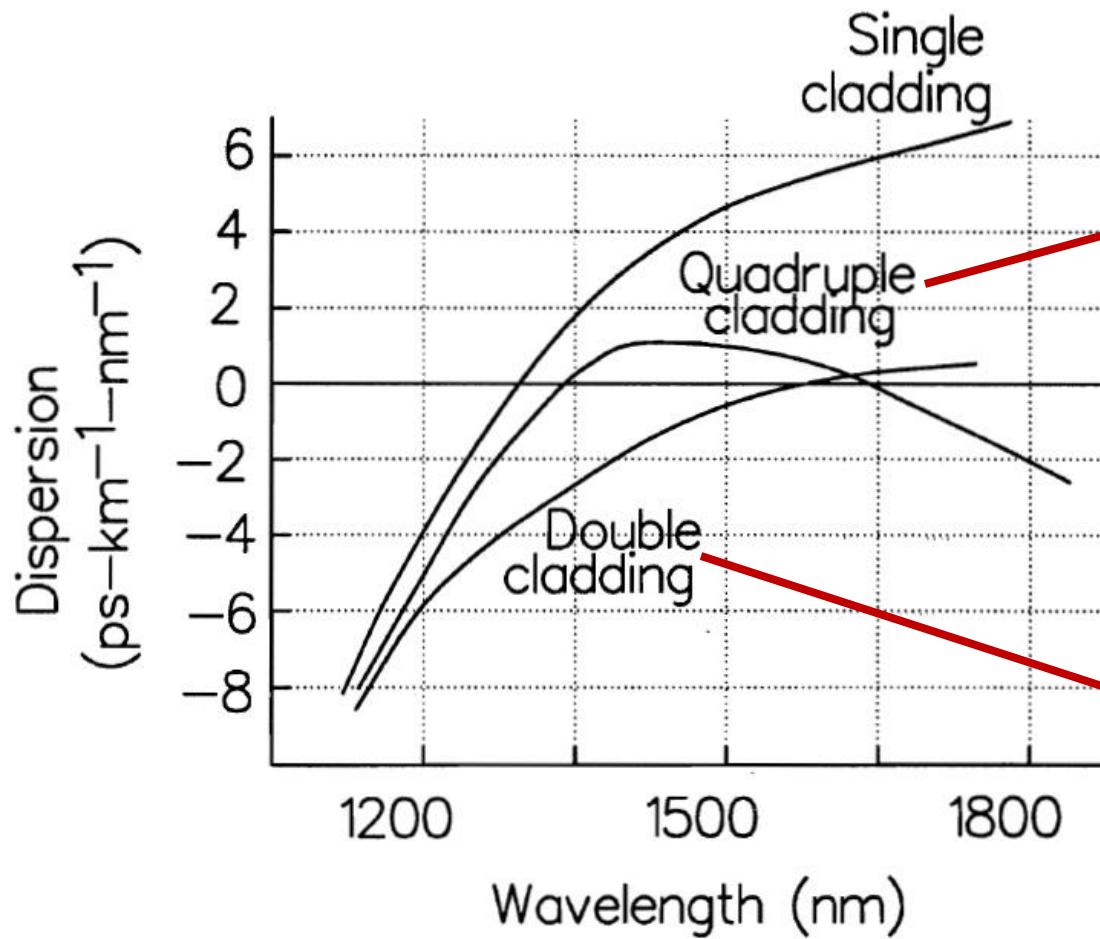
**Zero Dispersion Wavelength ( $\lambda_0$ )** 1317 nm  
**Zero Dispersion Slope ( $S_0$ )** 0.088 ps/(nm<sup>2</sup>·km)  
**Effective Group Index** 1310 nm: 1.4670



# Non-zero Dispersion shifted fibers



# Dispersion shifted fibers



# Contact

- ▶ Laboratorul de microunde si optoelectronica
- ▶ <http://rf-opto.eti.tuiasi.ro>
- ▶ [rdamian@etti.tuiasi.ro](mailto:rdamian@etti.tuiasi.ro)