

Optoelectronică, structuri și tehnologii

Curs 4

Fibra optică

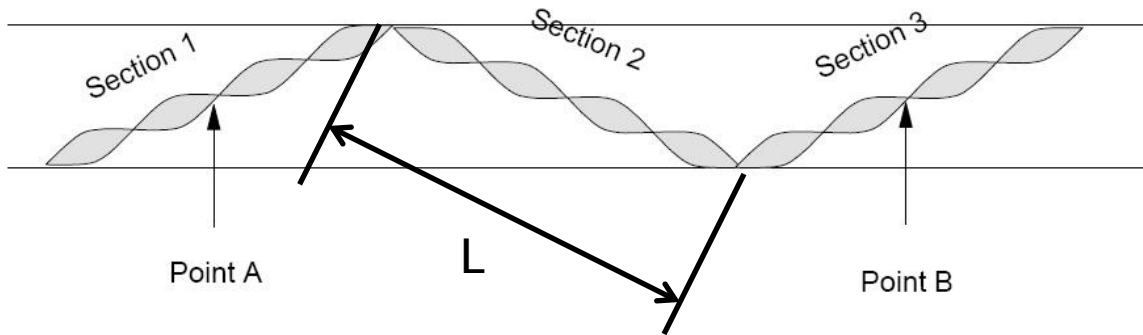
Capitolul 4

Frecventa normalizata

- ▶ Frecventa normalizata

$$V = 2\pi \frac{a}{\lambda} NA = k \cdot a \cdot NA \quad a - \text{raza miezului}$$

- ▶ Numar de moduri



$$L = k \cdot \lambda$$

$$N \approx \frac{V^2}{2} \cdot \frac{g}{g+2}$$

Frecventa normalizata

- ▶ Numar de moduri
 - Multimod cu salt de indice

$$g = 1 \Rightarrow N \approx \frac{V^2}{2}$$

- Multimod cu indice gradat

$$g = 2 \Rightarrow N \approx \frac{V^2}{4}$$

- Monomod

$V \leq V_c = 2.405$ exista un singur mod (solutii fc. Bessel)

$$\lambda \geq \lambda_c = \pi \frac{2a}{V_c} NA = \pi \frac{2a}{2.405} NA$$

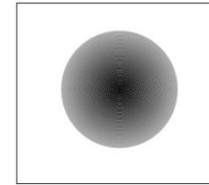
$$2a = 8.5 \mu\text{m}$$

$$NA = 0.11$$

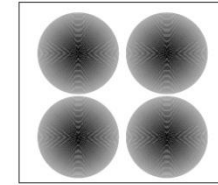
$$\lambda_c = \pi \frac{8.5}{2.405} 0.11 = 1210 \text{nm}$$

Moduri in fibra

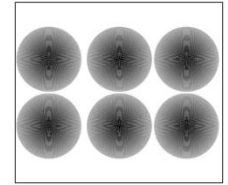
- ▶ Moduri in ghid rectangular



TEM₀₀

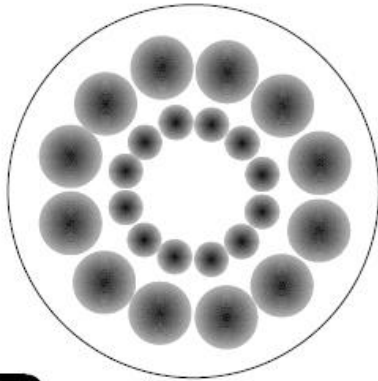


TEM₁₁

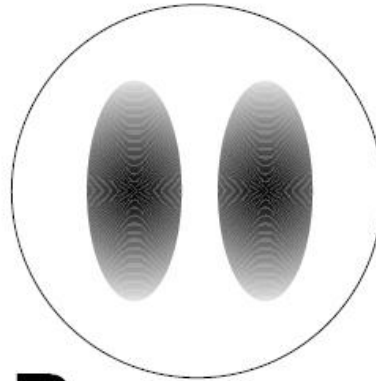


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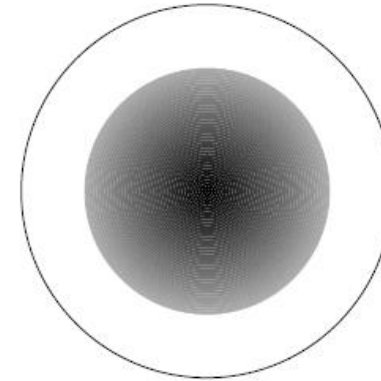
- ▶ Moduri linear polarizate in fibra



LP₆₂

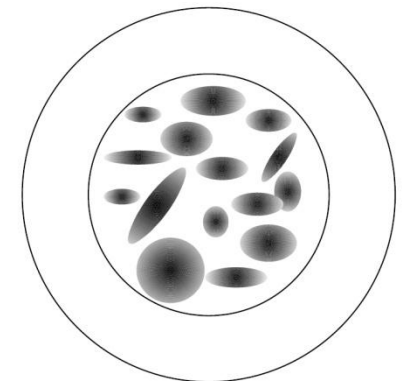


LP₁₁



LP₀₁

“Sparkle” pattern

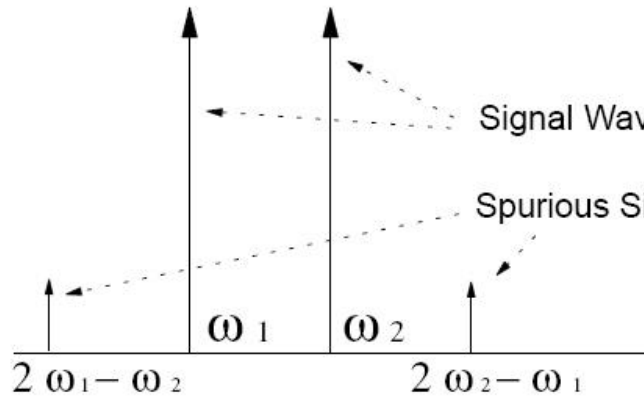


Efecte neliniare in fibra

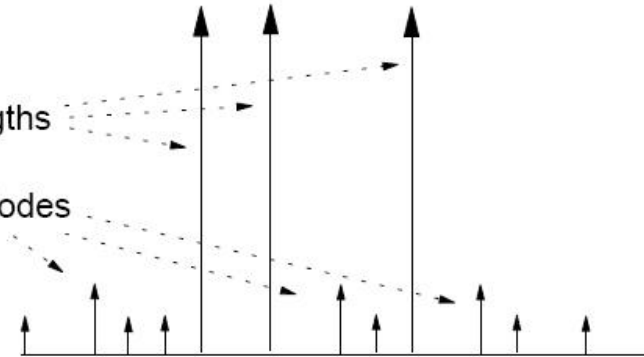
- ▶ **Stimulated Brillouin Scattering, SBC**
 - difractia luminii inspre emitator datorita undelor mecano-acustice generate in fibra
 - 6–10 dBm
- ▶ **Stimulated Raman Scattering, SRS**
 - interactiunea luminii cu vibratiile moleculare
 - 27 dBm (~1W)
- ▶ **Self Phase Modulation, SPM**
 - Frontiera impulsului implica indice de refractie variabil in timp moduland faza impulsului
 - 5 dBm
 - Cross Phase Modulation, CPM
- ▶ **Four-Wave Mixing, FWM**
 - 0 dBm

Four-Wave Mixing, FWM

Two Channels



Three Channels

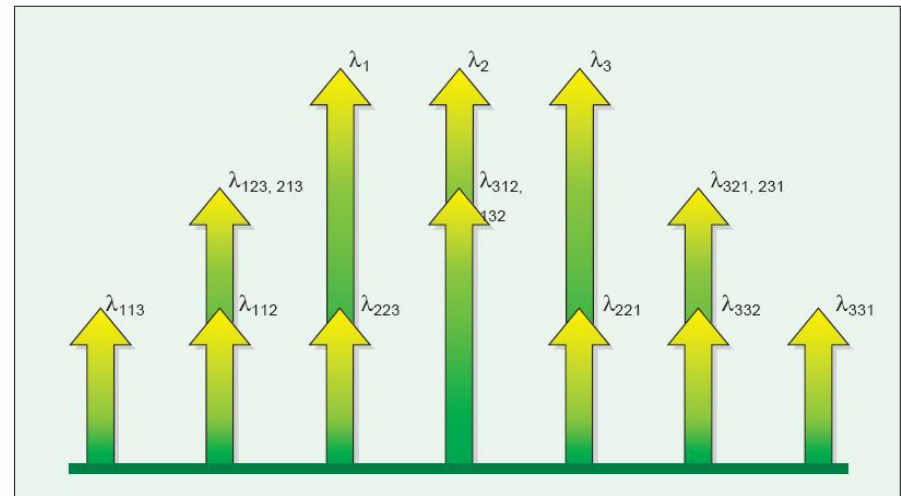


$$NL = \frac{1}{2}(N^3 - N^2)$$

$$N = 2, NL = 4$$

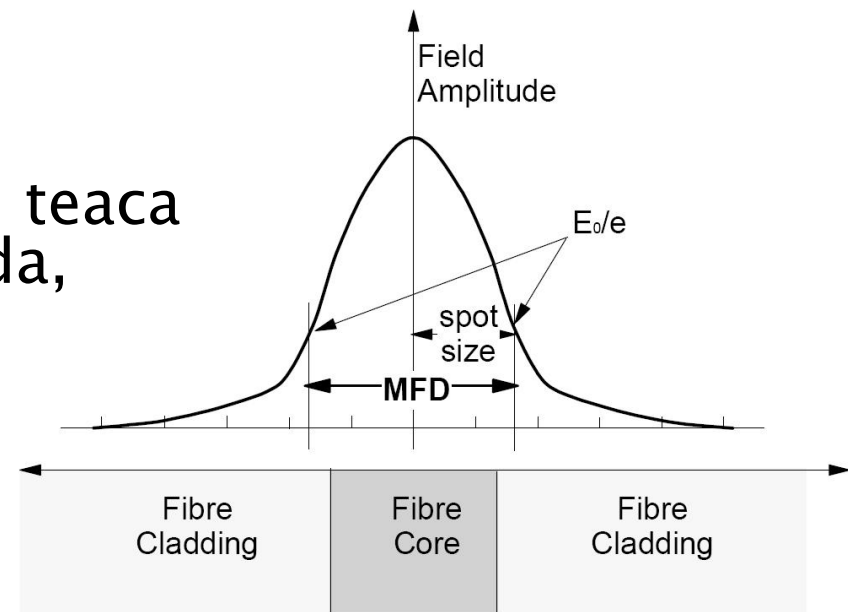
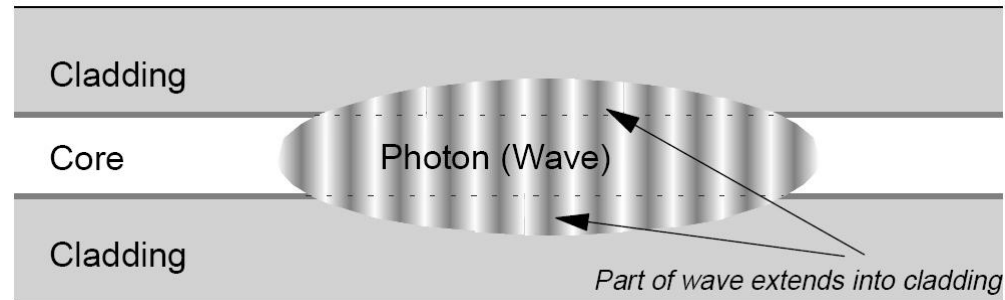
$$N = 3, NL = 9$$

$$N = 16, NL = 1920$$



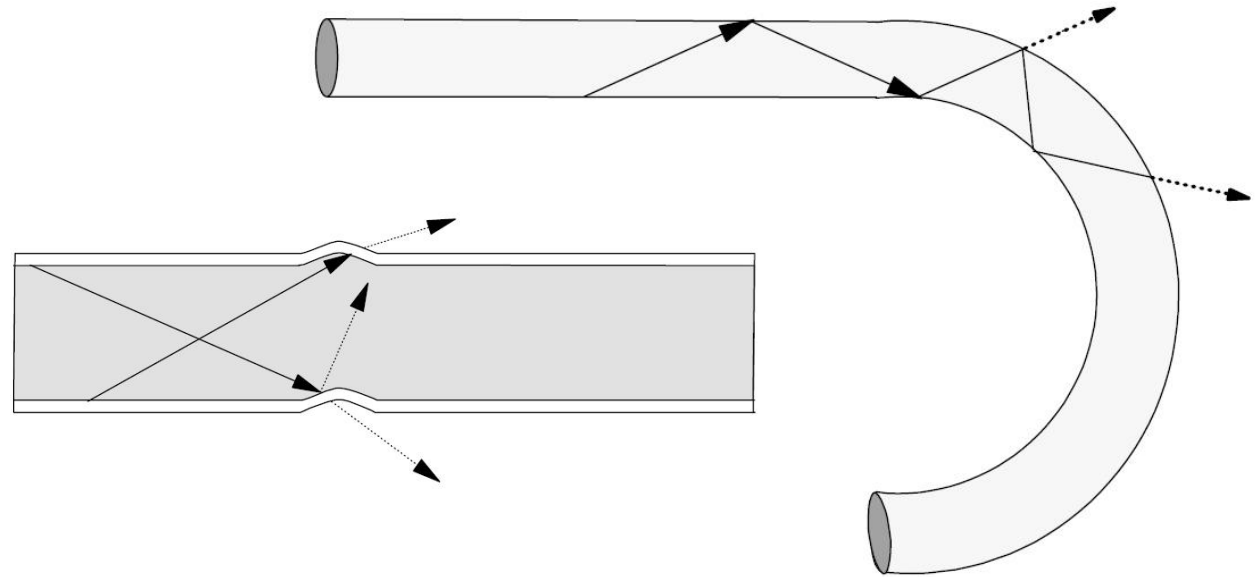
Propagarea in fibra monomod

- ▶ Propagarea luminii poate fi explicata doar prin teoria electromagnetica
- ▶ Energia campului se extinde in teaca (diametrul efectiv al spotului luminos – MFD, Mode Field Diameter)
- ▶ $MFD > 2a$
- ▶ Adancimea de patrundere in teaca depinde de lungimea de unda, generand dispersia de ghid



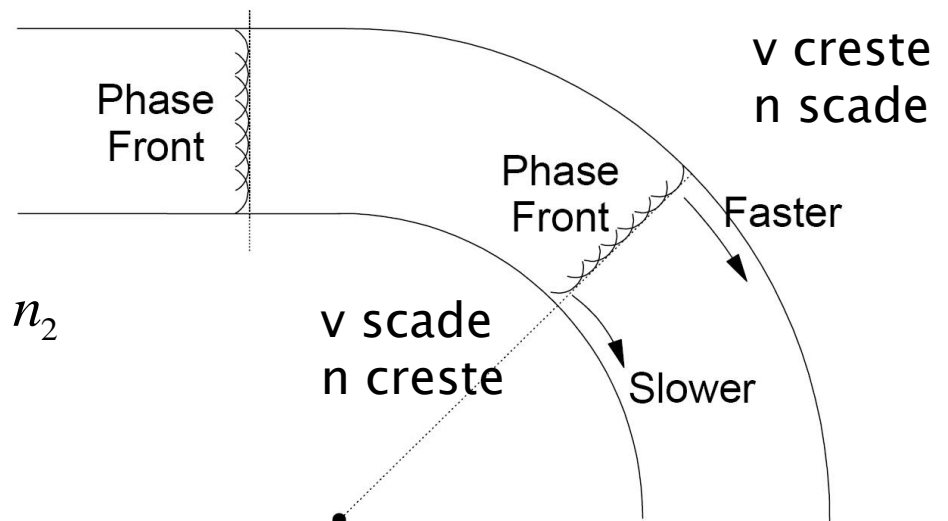
Efectul curburilor

▶ Multimod



▶ Monomod

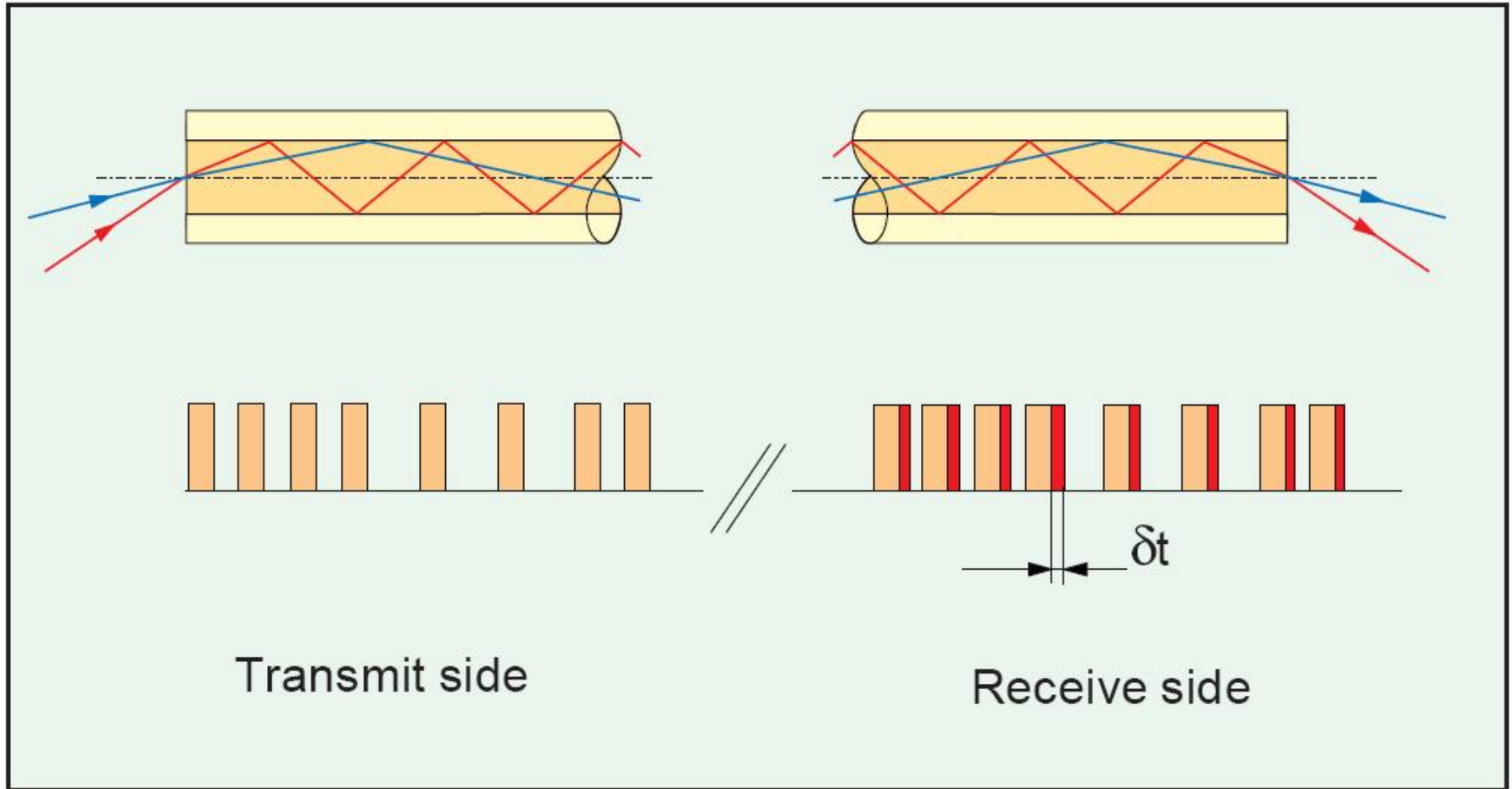
$$R > R_C \Rightarrow n_{1,ext} > n_2$$



Dispersia

- ▶ intermodala (modala – depinde de prezenta modurilor)
- ▶ intramodală (cromatică – depinde de lungimea de undă)
 - de material
 - de ghid

Dispersia modala



Dispersia modala

▶ salt de indice

$$dt = \frac{L \cdot n_2^2}{c \cdot n_1} \left(\frac{n_2 - n_1}{n_2} \right) \approx \frac{L \cdot NA^2}{2 \cdot c \cdot n_2} \quad \text{intarzierea intre moduri cand} \quad \Delta = \frac{n_2 - n_1}{n_1} \ll 1$$

$$\Delta \tau_{\text{mod}}^2 = \frac{1}{3} \left(\frac{dt}{2} \right)^2$$

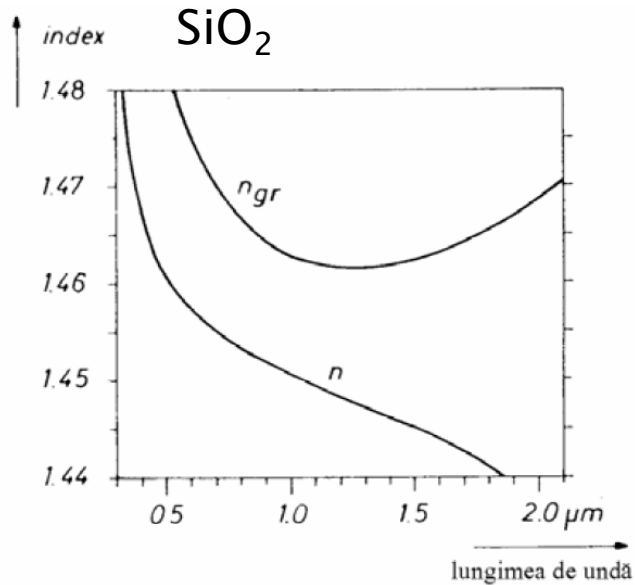
$$\Delta \tau_{\text{mod}} \cong \frac{L \cdot n_2 \cdot \Delta}{2\sqrt{3} \cdot c} \approx \frac{L \cdot NA^2}{4\sqrt{3} \cdot c \cdot n_2}$$

▶ indice gradat

$$dt = \frac{L \cdot n_2 \cdot \Delta^2}{2c} \approx \frac{L \cdot NA^4}{8 \cdot c \cdot n_2^3}$$

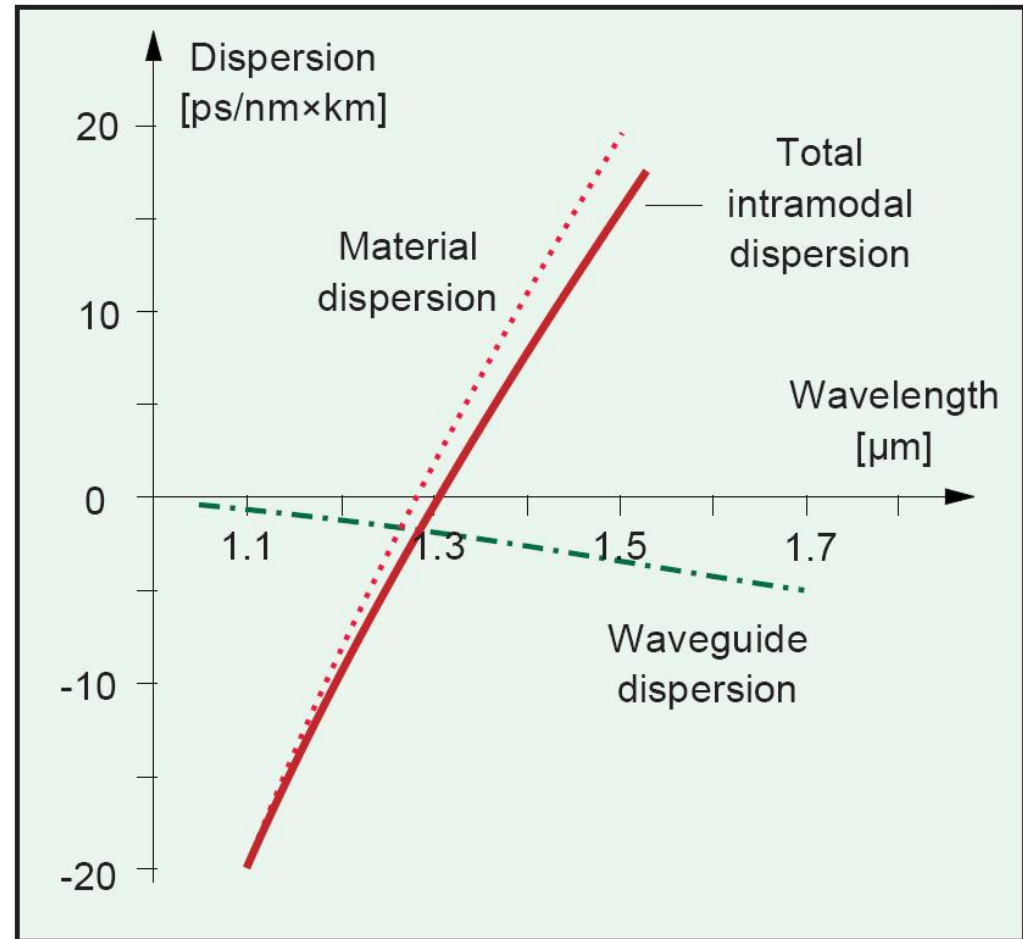
$$\Delta \tau_{\text{mod}} \cong \frac{L \cdot n_2 \cdot \Delta^2}{4\sqrt{3} \cdot c}$$

Dispersia de material



$$n_{gr} = n - \lambda \frac{dn}{d\lambda}$$

$$\Delta\tau_{mat} = \frac{L \cdot \lambda \cdot \Delta\lambda}{c} \cdot \frac{d^2n}{d\lambda^2}$$

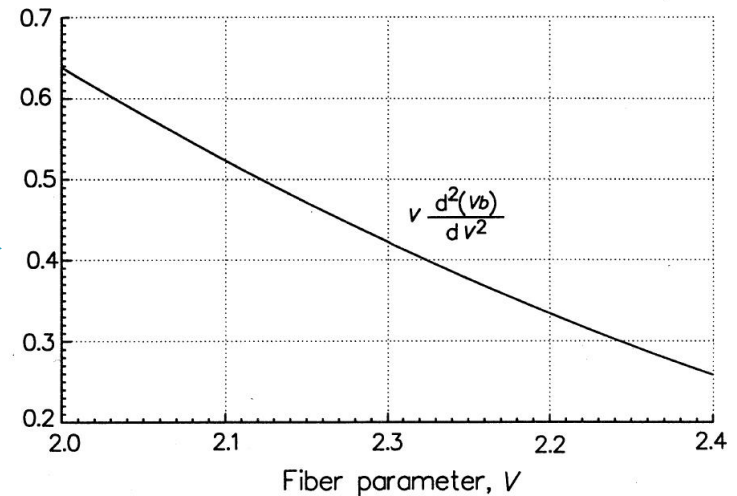
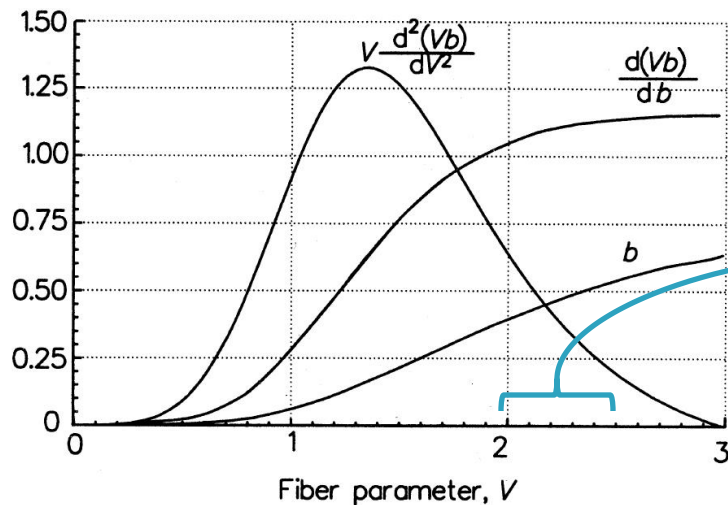


Dispersia de ghid

- ▶ Neglijabila in fibrele multimod fata de dispersia modala

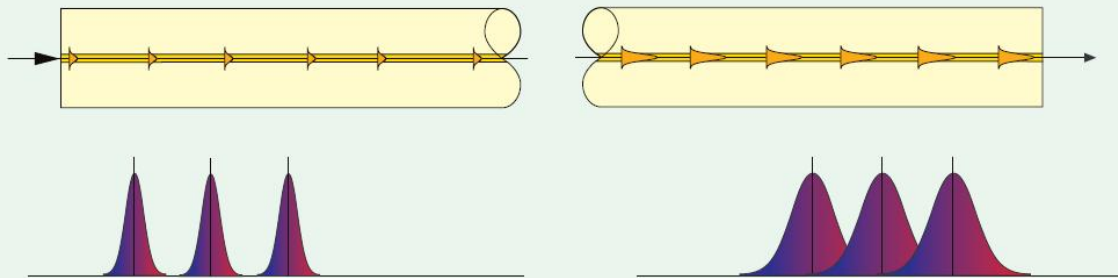
$$\Delta\tau_{mat} = \frac{n \cdot L \cdot \Delta}{c} \cdot \frac{\Delta\lambda}{\lambda} \cdot \left(V \frac{d^2(Vb)}{dV^2} \right)$$

b – constanta de propagare normalizata



Dispersia cromatica

> 50 km Single-mode step index
 < 10 km Multimode graded index
 < 1 km Multimode step index



Transmission:
 Well-defined pulses but not absolutely
 monochromatic.
 Typical spectral width < 0.8 nm

Reception:
 Pulse broadening caused by the laser's spectral width
 and the difference between the refractive indices of
 the red and blue ends of the light pulse.

$$\Delta\tau_{cr} = D(\lambda) \cdot \Delta\lambda \cdot L$$

- ▶ $D(\lambda) \approx 100 + 0.4 (850 - \lambda)$ [ps/nm/km]
pentru $800 < \lambda < 900$ nm
- ▶ $D(\lambda) \leq 3,5$ ps/nm/km
pentru $1285 < \lambda < 1330$ nm
- ▶ $D(\lambda) \leq 17$ ps/nm/km
pentru $1525 < \lambda < 1575$ nm

Banda

- ▶ Dispersia totala

$$\Delta\tau_{tot} = \sqrt{\Delta\tau_{cr}^2 + \Delta\tau_{mod}^2}$$

- ▶ Banda

$$B_{opt} = \frac{0.44}{\Delta\tau_{tot} [ns]} [GHz]$$

$$B_{opt} = \sqrt{2} B_{el}$$

- ▶ Banda optica la 3 dB corespunde unei benzi electrice la 6 dB

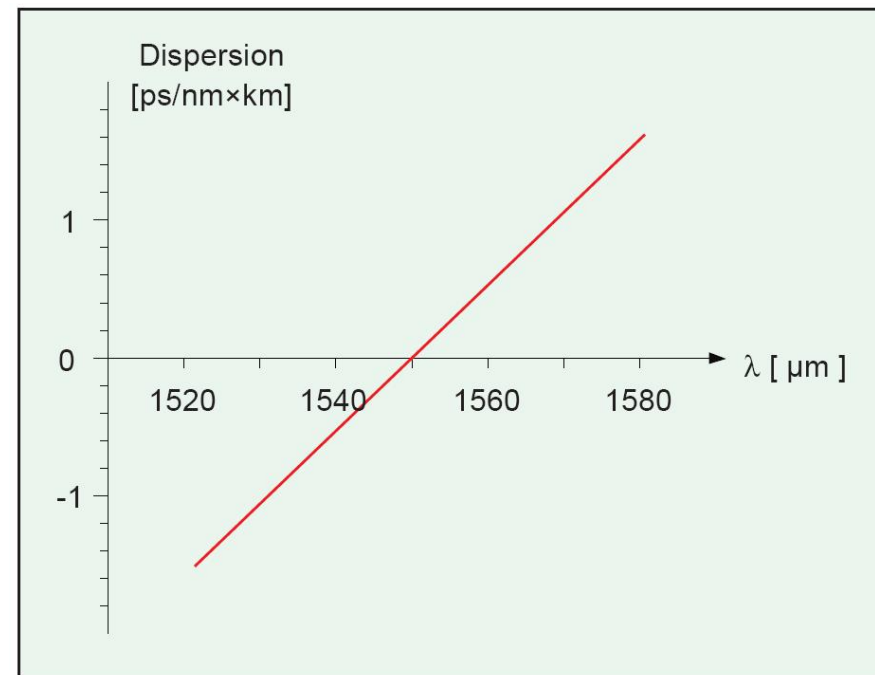
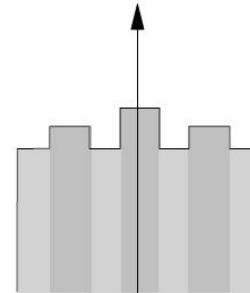
- $P_{opt} \sim I$; $P_{el} \sim I^2$

- ▶ Viteza legaturii

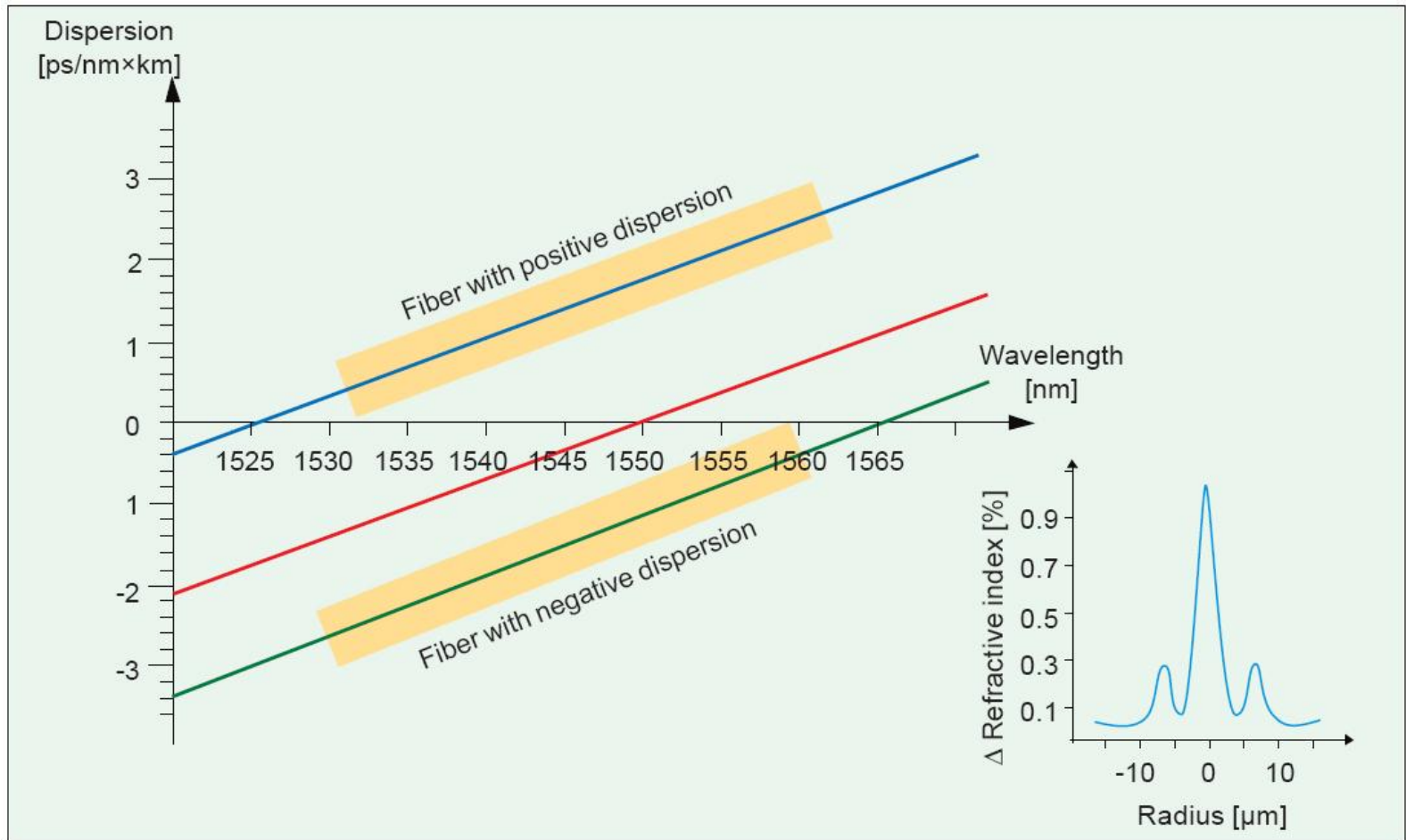
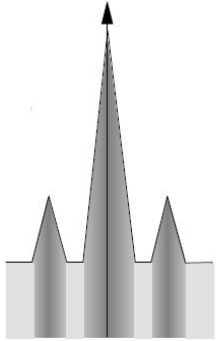
$$V [Gb/s] \cong \frac{1}{2} B_{el}$$

Dispersion shifted fibers

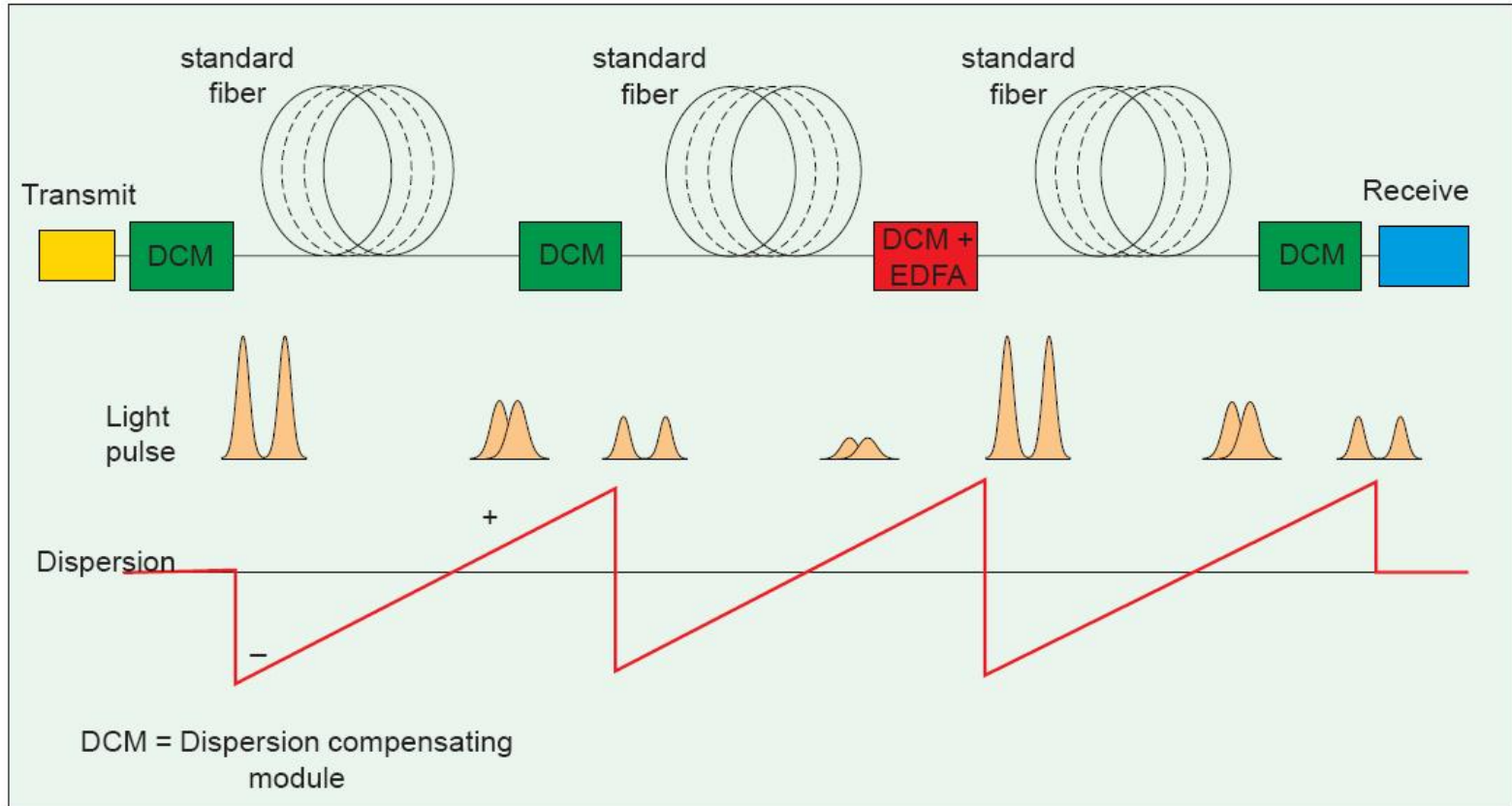
- ▶ Atenuarea e mai mica la 1550 nm
- ▶ EDFA (Erbium doped fibre amplifiers) opereaza in banda aceasta
- ▶ Sistemele WDM (Wavelength division Multiplexing) necesita banda larga amplificata



Non-zero Dispersion shifted fibers



Fibra pentru compensarea dispersiei



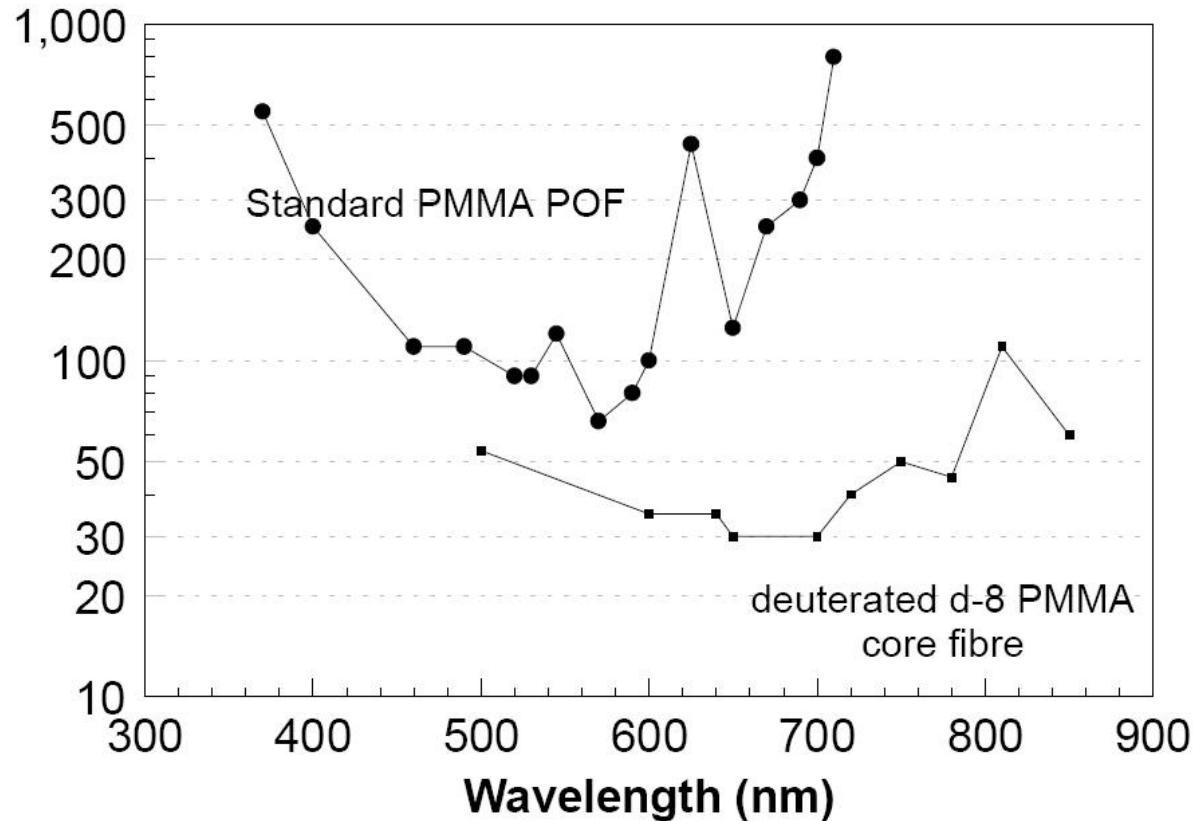
- ▶ Dispersie -100 ps/nm/km
- ▶ Atenuare 0.5 dB/km

Fibra standard ITU G.652

- ▶ Diametru teaca = 125 μm
- ▶ MFD = 9÷10 μm la 1300 nm
- ▶ $\lambda_c = 1100\div 1280$ nm
- ▶ Pierderi de curbura (la 1550 nm) mai mici de 1 dB pentru 100 spire de fibra rulata pe un mosor cu 7.5 cm diametru
- ▶ Dispersia in banda 1300 nm (1285–1330 nm) mai mica de 3.5 ps/nm/km. La 1550 nm dispersia trebuie sa fie mai mica de 20 ps/nm/km
- ▶ Viteza de variatie a dispersiei (panta dispersiei) mai mica de 0.095 ps/nm²/km

Fibra optica din plastic (POF)

Attenuation dB/Km



- ▶ Atenuare 180 dB/km
- ▶ NA = 0.3
- ▶ Diametru 1 mm
- ▶ Banda 125MHz (100m)