

Optoelectronică

Curs 5

2023/2024

Disciplina 2023/2024

- ▶ 2C/1L Optoelectronică **OPTO**
- ▶ **Minim 7 prezente curs + laborator**
- ▶ Curs – conf. **Radu Damian**
 - an IV μ E
 - Marti 14(**:10**)-16:00, P8
 - E – 70% din nota (50%+20%)
 - **20% test (VP) la curs**, saptamana 4-6?
 - probleme + (2p prez. curs)
 - toate materialele permise
- ▶ Laborator – **drd. Stefan Stoica**
 - an IV μ E
 - Marti 16-20 par
 - Max. 7 prezente
 - L – 30% din nota (+Caiet de laborator)

Cuprins

- ▶ **Lumina ca undă electromagnetică*** (ecuațiile lui Maxwell, ecuația undelor, parametri de propagare)
- ▶ **Elemente de fotometrie și radiometrie*** (mărimi energetice/luminoase)
- ▶ **Fibra optică** (realizare, principiu de funcționare, atenuare, dispersie, banda de frecvență)
- ▶ **Cabluri optice** (tehnologie, conectori, lipire – splice)
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- ▶ **Dispozitive de captare a energiei solare** (principiu de funcționare, utilizare, proiectare)

* – VP

Documentatie



English | Romana |

[Main](#) [Courses](#) [Master](#) [Staff](#) [Research](#) [Students](#)

Microwave and Optoelectronics Laboratory

We are enlisted in the Telecommunications Department of the Electronics, Telecommunication and Information Technology Faculty (ETIT) from the "Gh. Asachi" Technical University (TUIASI) in Iasi, Romania

We currently cover inside ETIT the fields related to:

- Microwave Circuits and Devices
- Optoelectronics
- Information Technology

Courses

Nr.	Course	Shortcut	Code	Type	Semester	Credits	Weekly	Examination	Link
1	Microwave Devices and Circuits for Radiocommunications	DCMR	DOS412T	DOS	7	4	0P,1L,0S,2C	Exam	details
2	Monolithic Microwave Integrated Circuits	CIMM	RD.IA.207	DOMS	11	6	1.5L,0S,2C,0P	Exam	details
3	Advanced Techniques in the Design of the Radio-communications Systems	TAPSR	RD.IA.103	DIMS	9	6	1.5P,0L,0S,2C	Exam	details
4	Optical Communications	CO	DOS409T	DOS	7	5	0P,1L,0S,3C	Colloquium	details
5	Optical Communications	OC	EDOS409T	DOS	7	5	0P,1L,0S,3C	Exam	details
6	Satellite Communications	CS	RC.IA.104	DIMS	9	6	0L,0S,2C,1.5P	Exam	details
7	Applied Informatics 1	IA1	DOF135	DOF	1	4	0P,1L,0S,2C	Verification	details
8	Applied Informatics 1	AI1	EDOF135	DOF	1	4	0P,1L,0S,2C	Verification	details
9	Databases, Web Programming and Interfacing	DWPI	ITT.IA.601	DIS	11	5	1P,1L,0.25S,1C	Verification	details
10	Web Applications Design	PAW	RC.IA.108	DIMS	10	5	1L,0S,1.5C,1P	Exam	details
11	Optoelectronics	OPTO	DID405M	DID	8	4	0P,1L,0S,2C	Colloquium	details
12	Microwave Devices and Circuits for Radiocommunications (English)	MDCR	EDOS412T	DOS	8	4	0P,1L,0S,2C	Exam	details



Documentatie

- ▶ RF-OPTO
 - <http://rf-opto.etti.tuiasi.ro>
- ▶ Fotografie
 - “examen” online
 - necesara la laborator/curs

Bonus (~0.5–4.15)

Disciplina: Optoelectronica, structuri, tehnologii, circuite
An: 2015/2016

Bonus-uri care se aplica la nota de la teza obtinute prin:

- prezenta la curs (0.5p / 3pr)
- 3 miniteste aplicate la curs (max. 3 X 1.5p)
- contributie la site rf-opto (foto <C5=1p, >C5=0.5p)

Nr.	Student	Grupa	Prezente curs	Bonus prezenta	Bonus foto	Bonus T1	Bonus T2	Bonus T3	Total Bonus	Obs.
1	CIOLPAN OCTAVIAN	5306	3	0.5					0.5	-
2	NITA COSTEL-CATALIN	5307	4	0.5	1				1.5	-
3	BARON BOGDAN-IONUT	5405	12	2	1	0.5		0.75	4.25	-

Prezenta

[Curs](#)
[Laborator](#)

Liste

[Studenti care nu pot intra in examen](#)
[Bonus-uri acumulate](#)

- ▶ **Minim** 7 prezente
- ▶ 0.5p/3prez
- ▶ 3 teste
- ▶ foto <C7 / <C9

Lumina ca undă electromagnetică

Capitolul 2

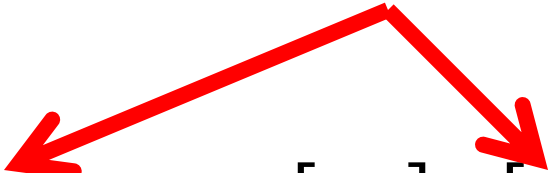
Cuprins

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Calculul atenuarii

$$\text{Pierderi} = \frac{P_{out}}{P_{in}} < 1$$

$$\text{Pierderi[dB]} = 10 \cdot \log_{10} \left(\frac{P_{out}}{P_{in}} \right) < 0$$


$$\text{Pierderi/Atenuare[dB]} = [-] 10 \cdot \log_{10} \left(\frac{P_{out}}{P_{in}} \right)$$

$$\text{Castig} = \frac{P_{out}}{P_{in}} > 1$$

$$\text{Castig[dB]} = 10 \cdot \log_{10} \left(\frac{P_{out}}{P_{in}} \right) > 0$$

$$\text{Atenuare[dB/km]} = \frac{\text{Pierderi[dB]}}{\text{lungime[km]}}$$

Calculul atenuarii

Pierderi/Atenuare $\rightarrow P_{out} < P_{in} \rightarrow P_{out} [\text{dBm}] < P_{in} [\text{dBm}]$

$$P_{out} [\text{dBm}] = P_{in} [\text{dBm}] - \text{Pierderi/Atenuare} [\text{dB}]$$



Castig/Amplificare $\rightarrow P_{out} > P_{in} \rightarrow P_{out} [\text{dBm}] > P_{in} [\text{dBm}]$

$$P_{out} [\text{dBm}] = P_{in} [\text{dBm}] + \text{Castig/Amplificare} [\text{dB}]$$



Reprezentare logaritmică

$$\text{dB} = 10 \cdot \log_{10} (P_2 / P_1)$$

$$\text{dBm} = 10 \cdot \log_{10} (P / 1 \text{ mW})$$

$$0 \text{ dB} = 1$$

$$+ 0.1 \text{ dB} = 1.023 (+2.3\%)$$

$$+ 3 \text{ dB} = 2$$

$$+ 5 \text{ dB} = 3$$

$$+ 10 \text{ dB} = 10$$

$$-3 \text{ dB} = 0.5$$

$$-10 \text{ dB} = 0.1$$

$$-20 \text{ dB} = 0.01$$

$$-30 \text{ dB} = 0.001$$

$$0 \text{ dBm} = 1 \text{ mW}$$

$$3 \text{ dBm} = 2 \text{ mW}$$

$$5 \text{ dBm} = 3 \text{ mW}$$

$$10 \text{ dBm} = 10 \text{ mW}$$

$$20 \text{ dBm} = 100 \text{ mW}$$

$$-3 \text{ dBm} = 0.5 \text{ mW}$$

$$-10 \text{ dBm} = 100 \mu\text{W}$$

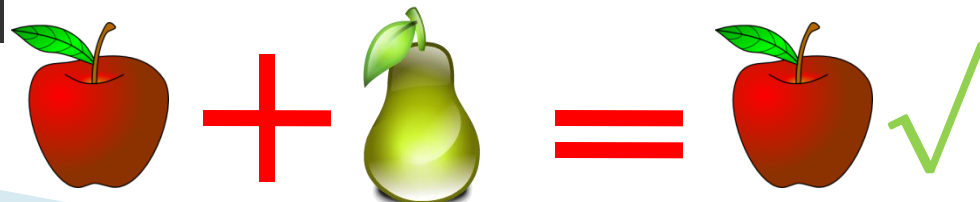
$$-30 \text{ dBm} = 1 \mu\text{W}$$

$$-60 \text{ dBm} = 1 \text{ nW}$$

$$[\text{dBm}] + [\text{dB}] = [\text{dBm}]$$

$$[\text{dBm/Hz}] + [\text{dB}] = [\text{dBm/Hz}]$$

$$[x] + [\text{dB}] = [x]$$



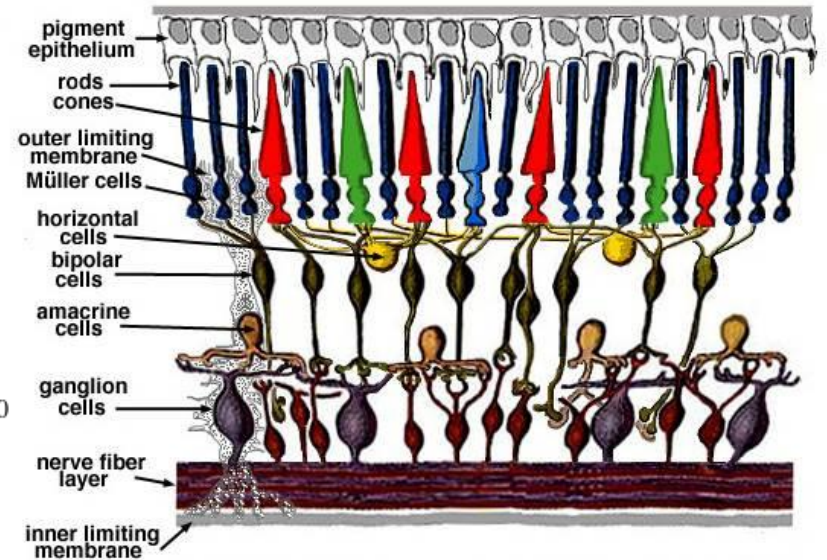
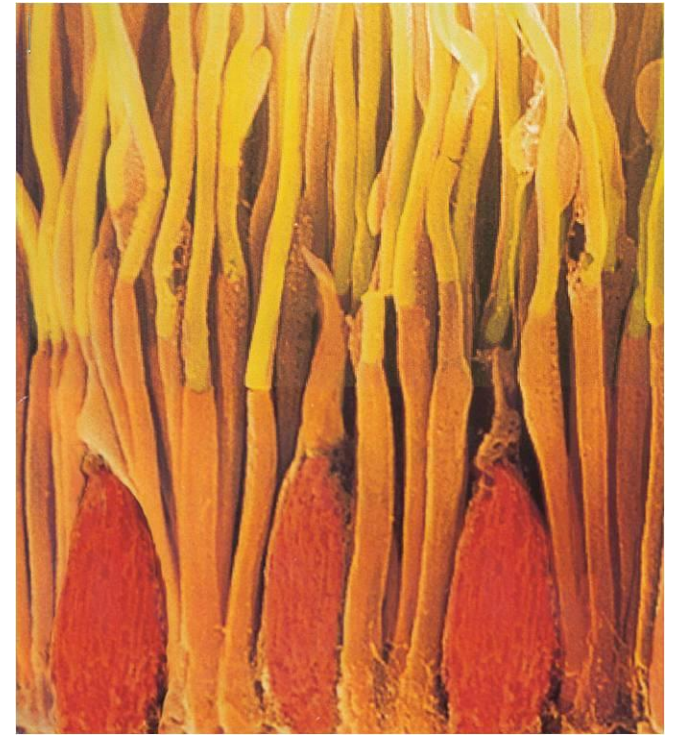
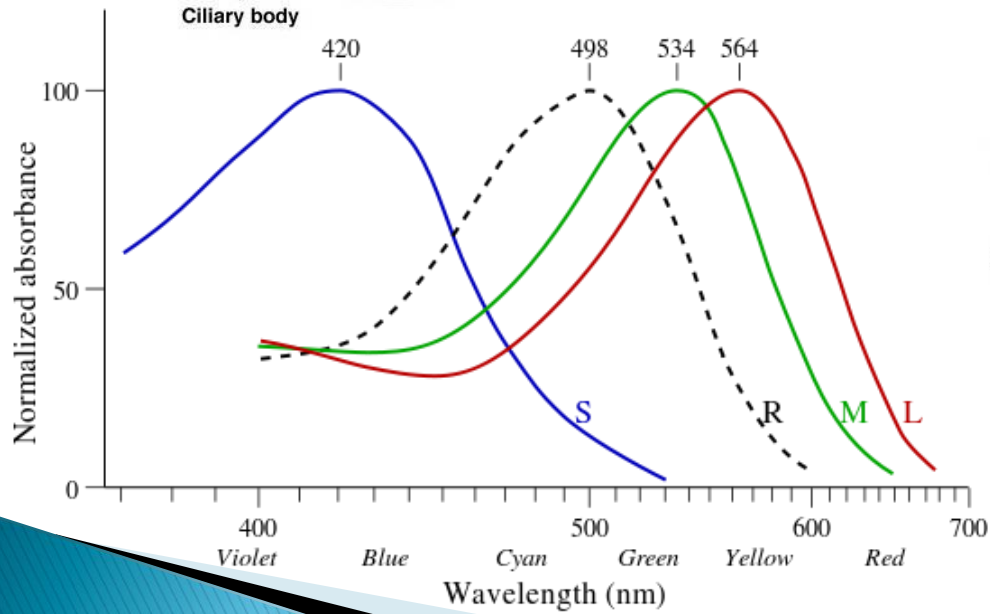
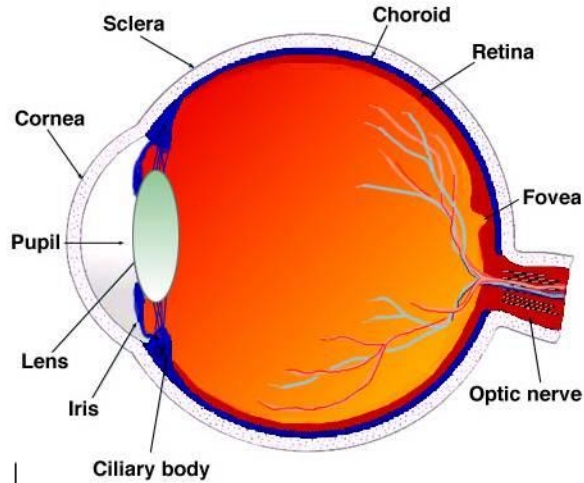
Fotometrie și radiometrie

Capitolul 3

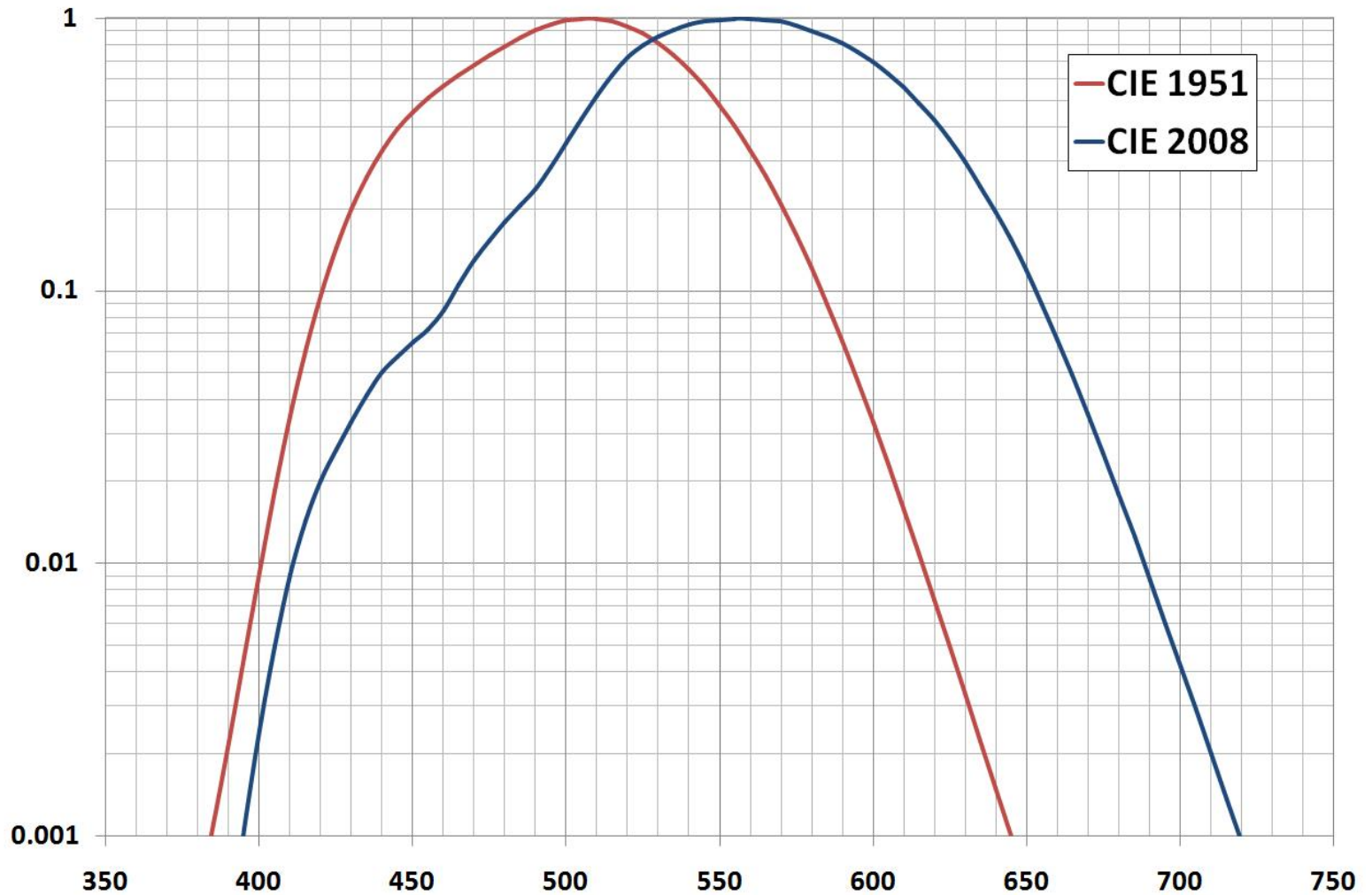
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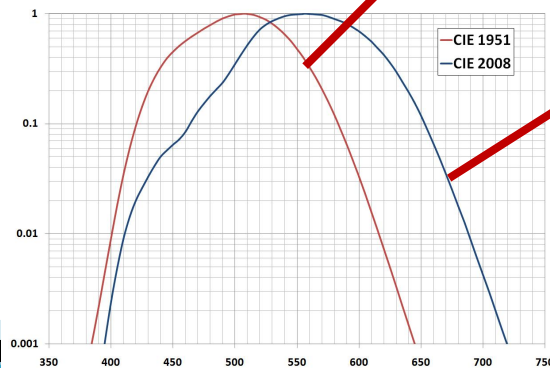
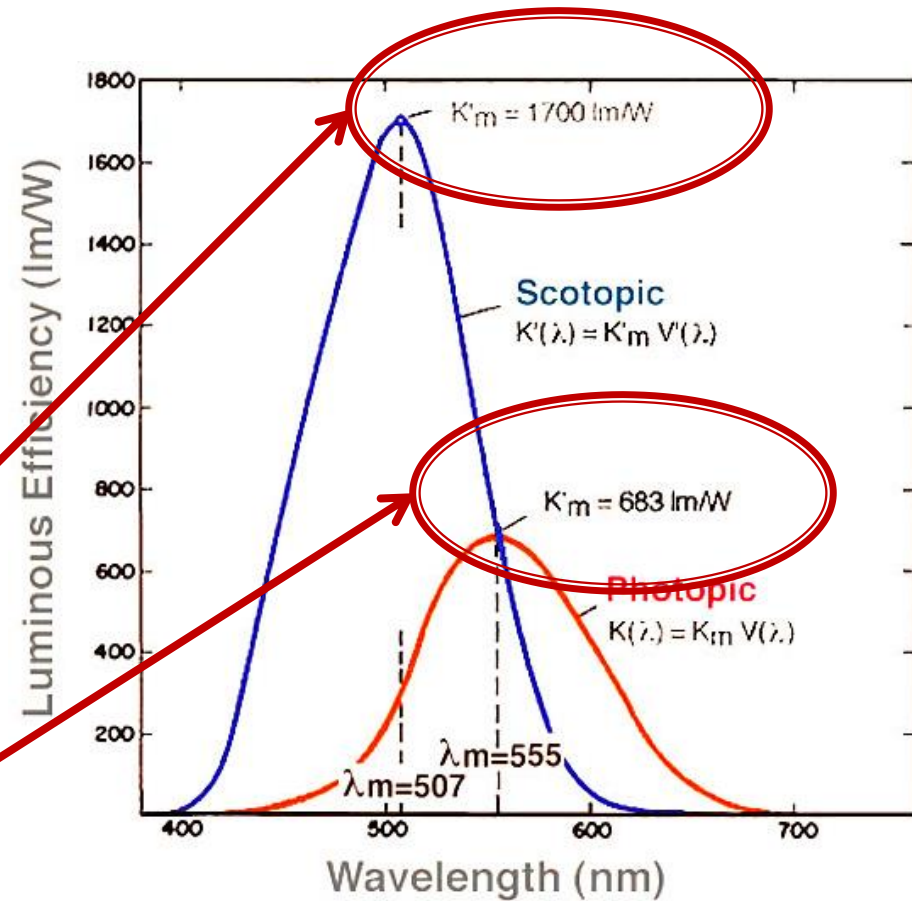
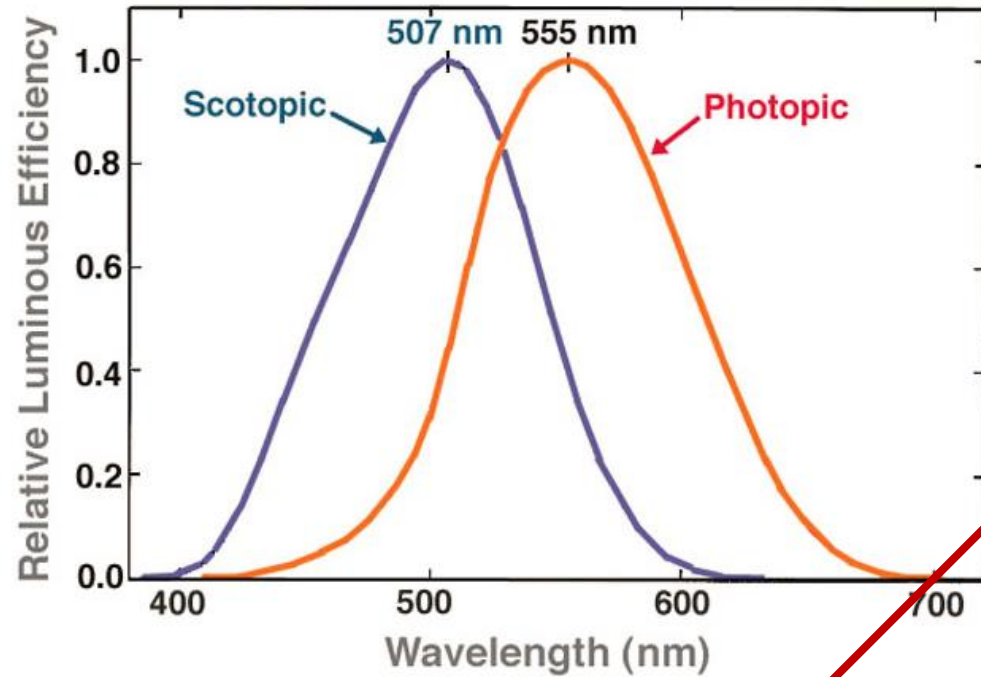
Ochiul uman



CIE $V(\lambda)$ fopic / scotopic

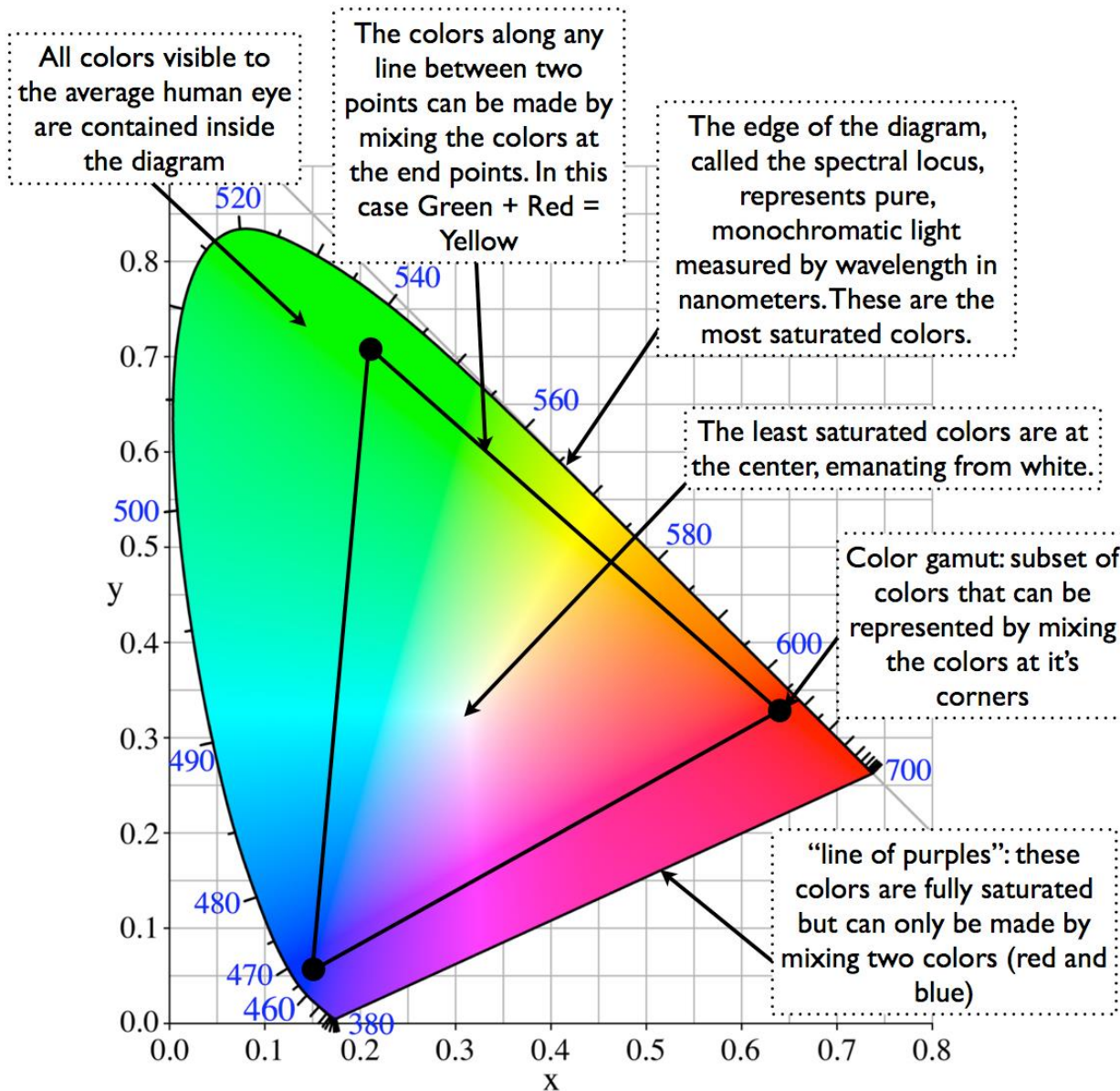


Relatie radiometrie/fotometrie



CIE xy 1931

► utilizzare



Fibra optică

Capitolul 4

Aplicatii majore

▶ Comunicatii

- Infrarosu (InGaAsP)

▶ Vizibil

- Spectru vizibil (GaAlAs)

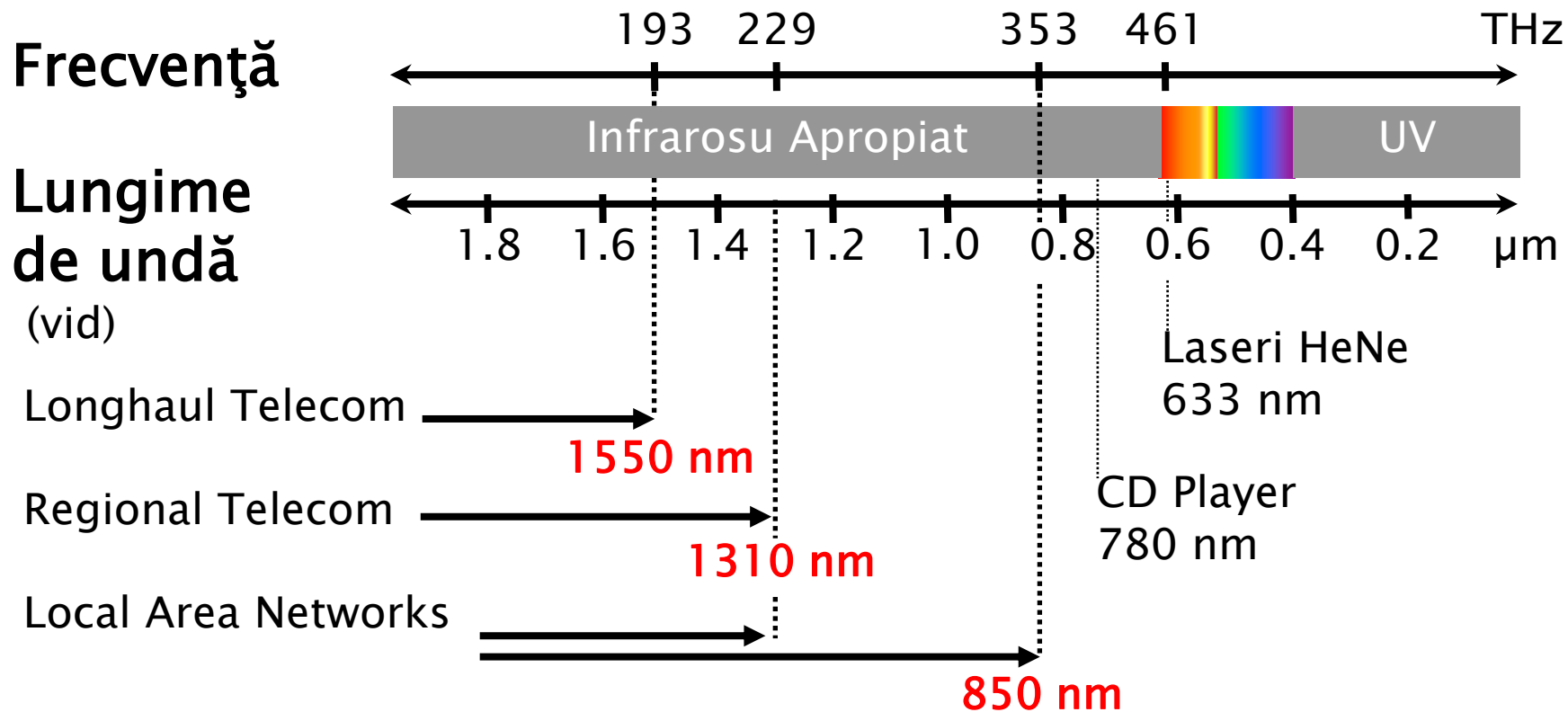
▶ Iluminare

- Putere ridicata, lumina alba (GaInN)

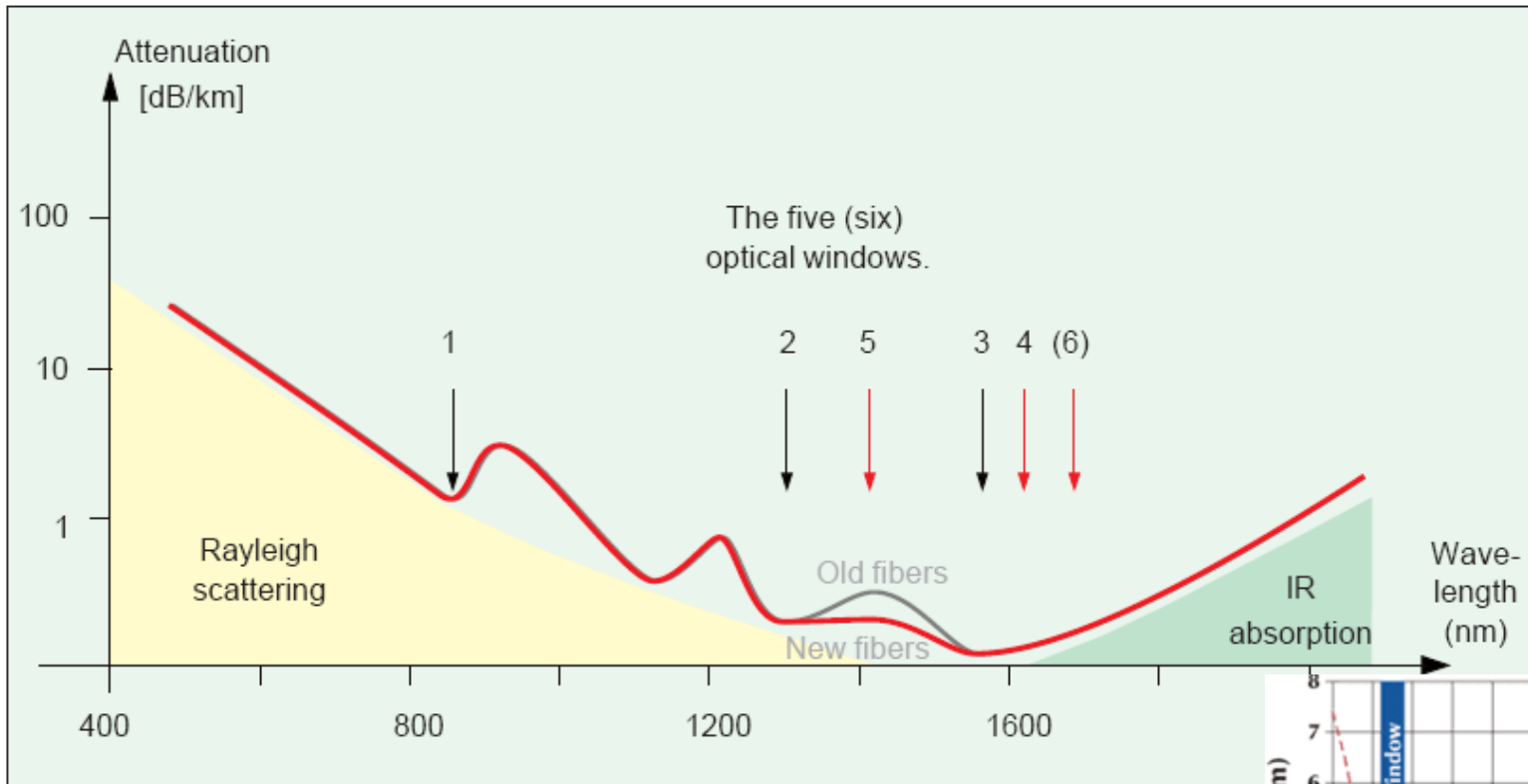
▶ Energie solara

- Efect fotovoltaic (Si)

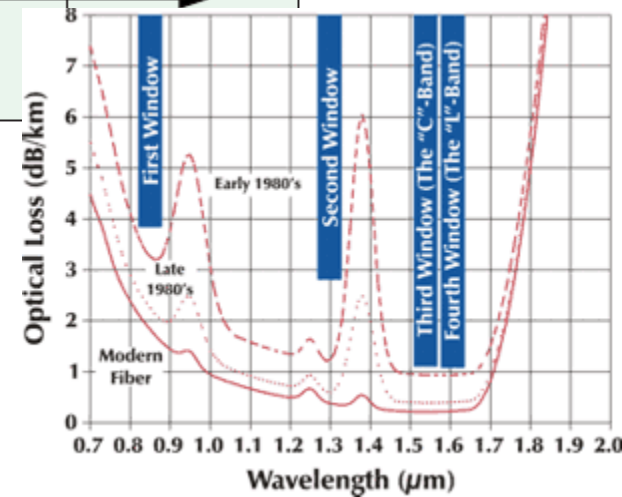
Benzi de lucru in comunicațiile optice



Atenuarea în fibra optică (SiO₂)



850nm, 1310nm, 1550nm

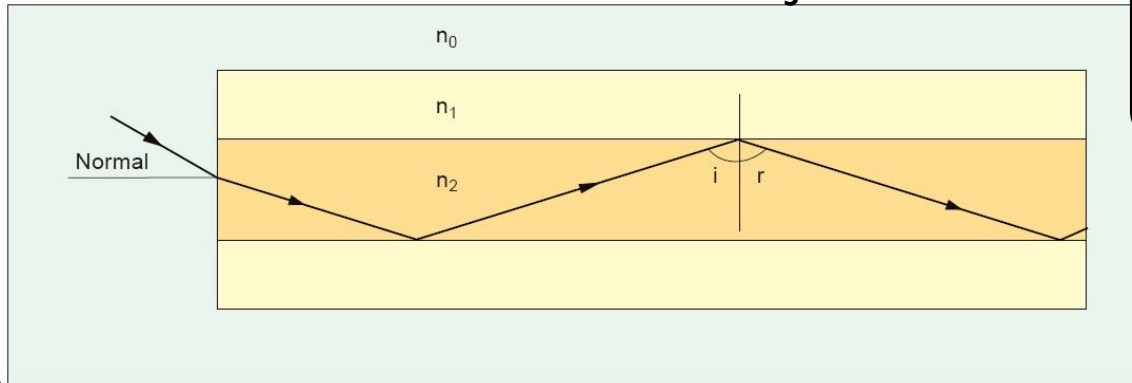
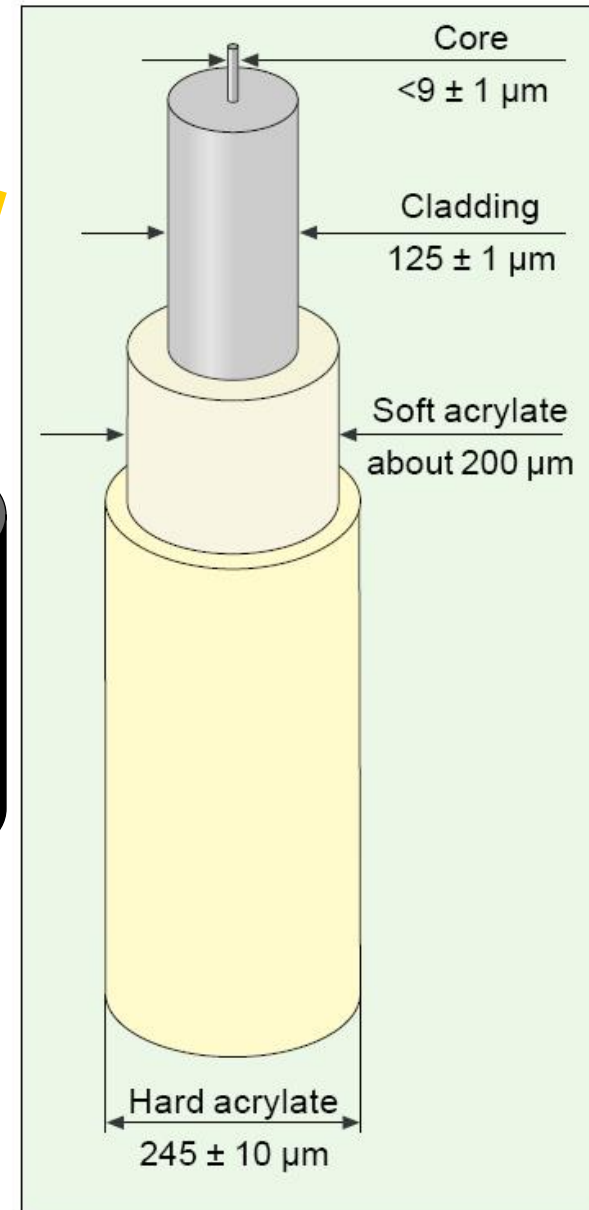
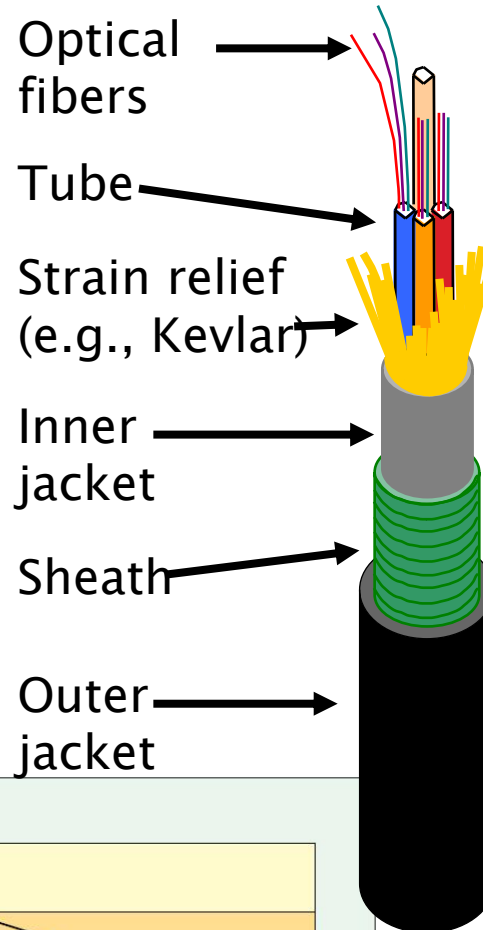


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Fibra optica

- ▶ un ghid de unda dielectric
 - miez
 - teaca



Unghi de acceptanta, apertura numerica

▶ Unghi de acceptanta

$$n_0 \cdot \sin \theta_{ACC} = n_2 \cdot \sin \phi_2$$

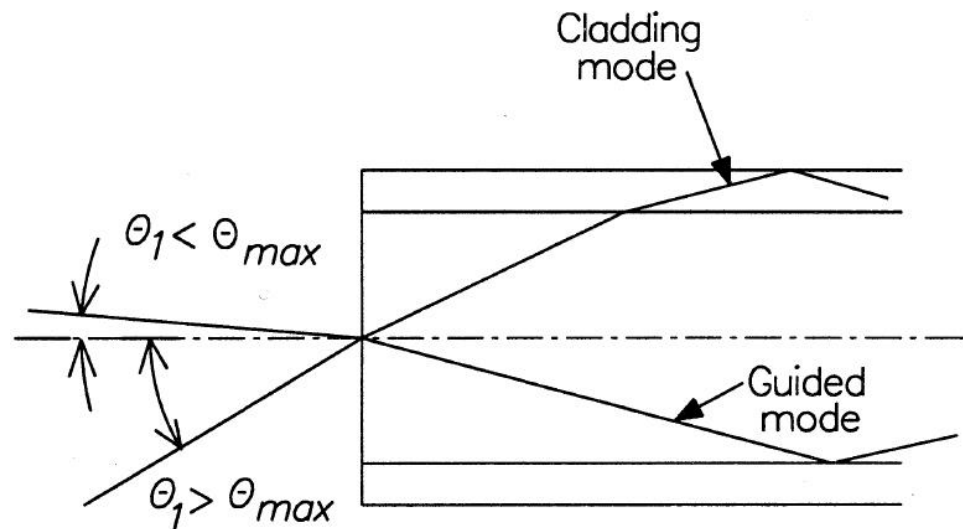
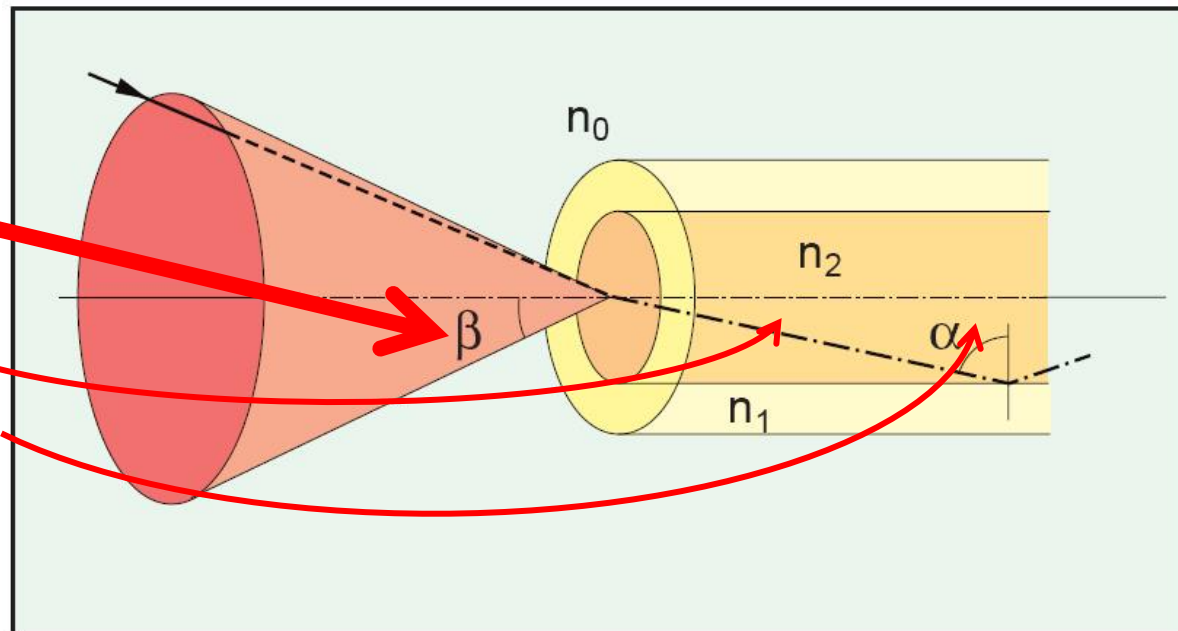
$$n_0 \cdot \sin \theta_{ACC} = n_2 \cdot \cos \phi_c$$

▶ Apertura numerica

$$NA = n_0 \cdot \sin \theta_{ACC}$$

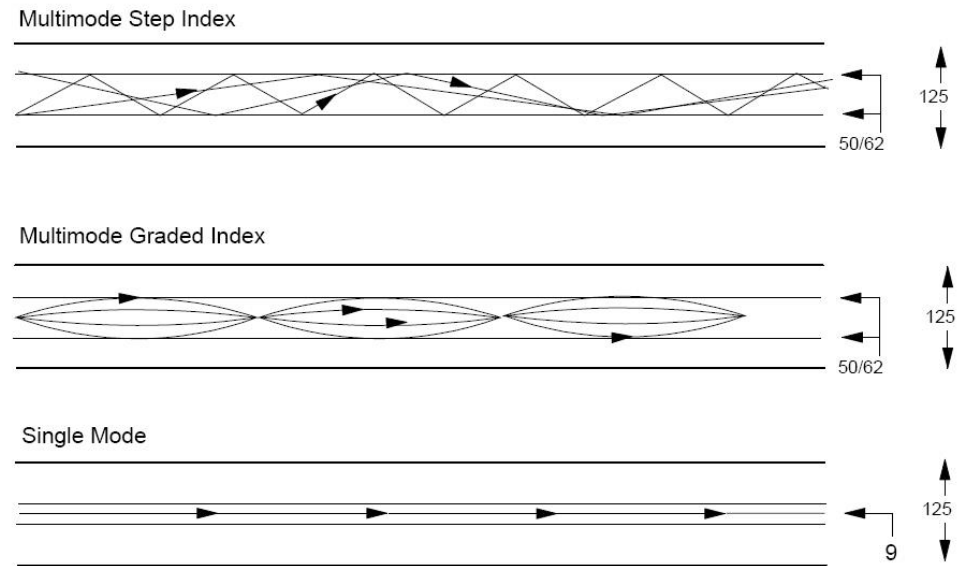
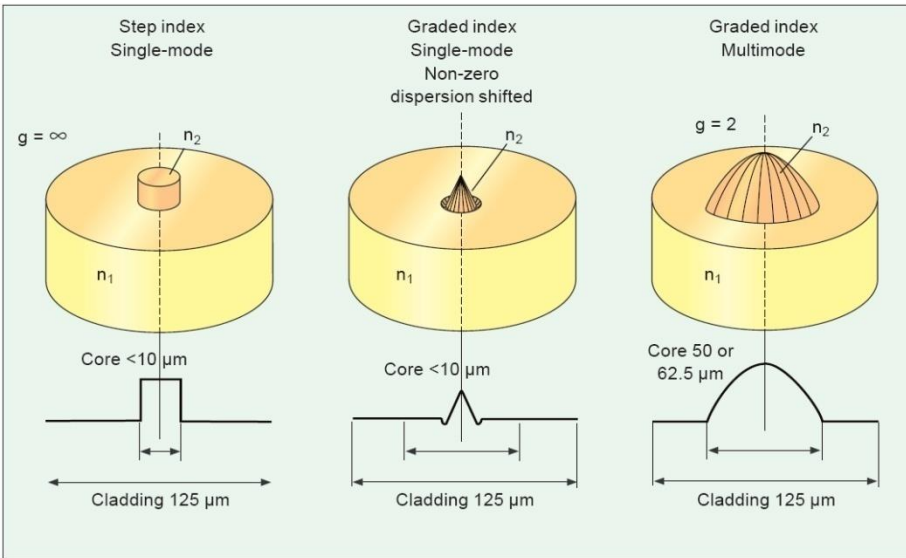
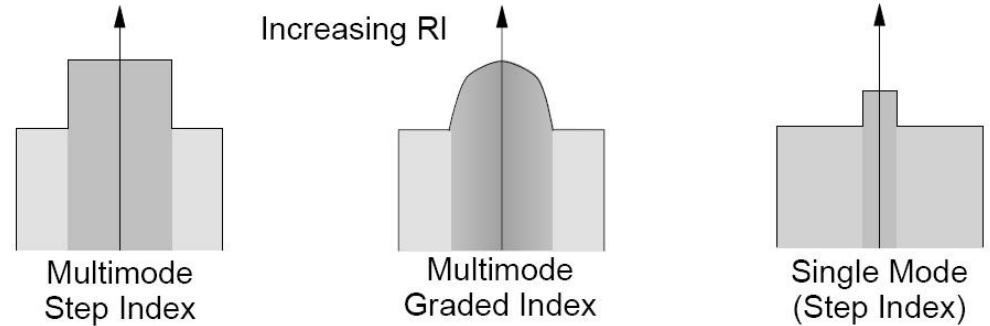
$$NA = n_2 \sqrt{\frac{n_2^2 - n_1^2}{n_2^2}} = \sqrt{n_2^2 - n_1^2}$$

n_2 - miez
 n_1 - teaca
 $n_2 > n_1$!!

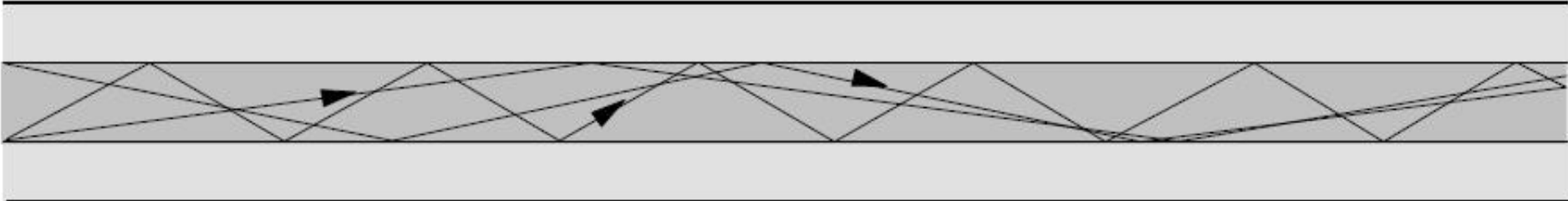


Tipuri de fibra

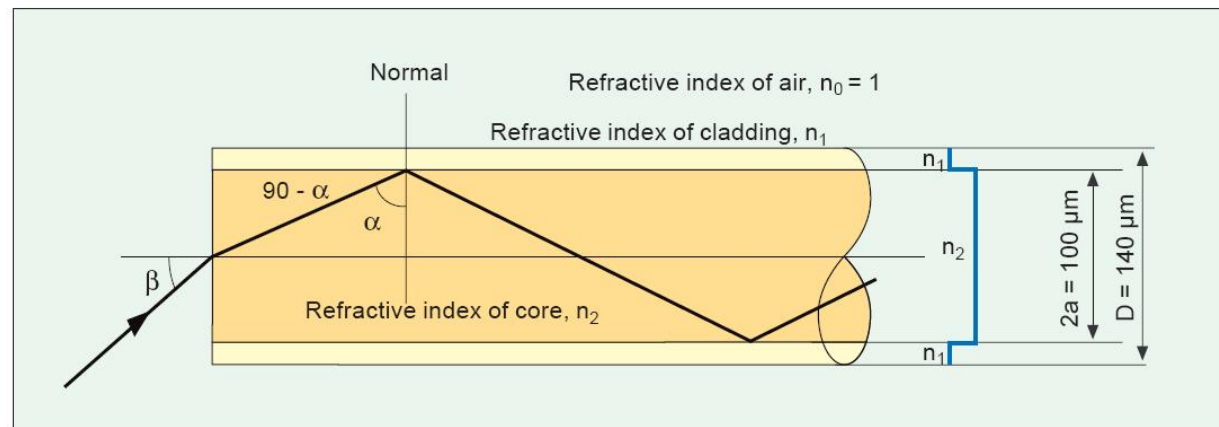
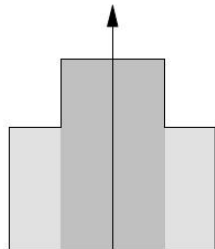
- ▶ Monomod
- ▶ Multimod
 - cu salt de indice
 - cu indice gradat



Fibre multimod cu salt de indice

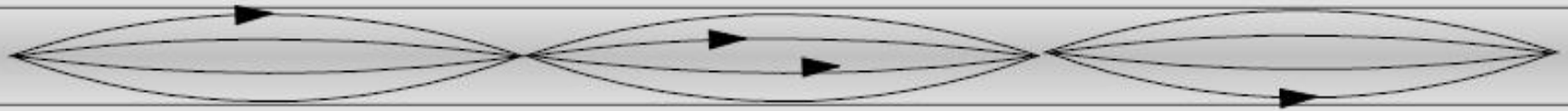


- ▶ 50/125 sau 62.5/125 (μm)
- ▶ 15–50 MHz · km

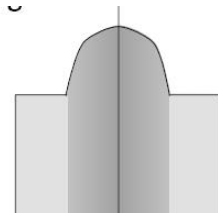
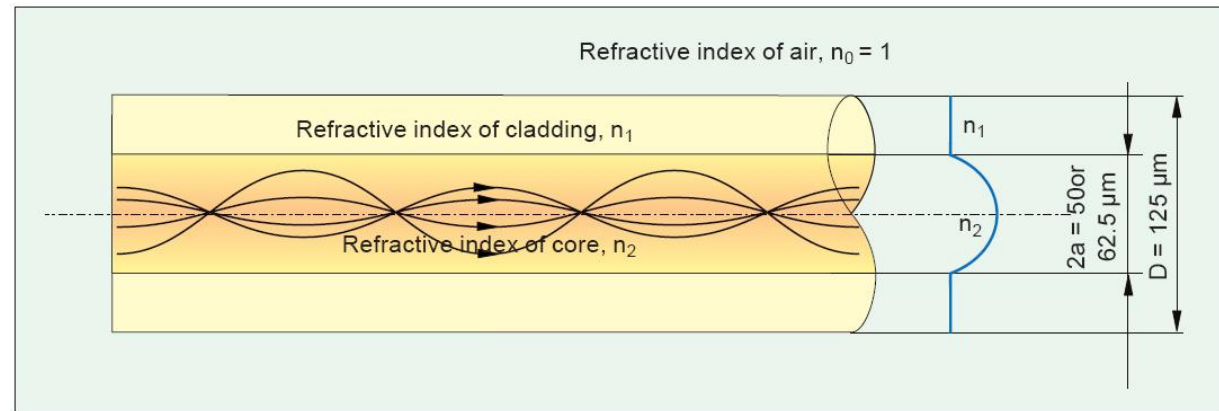


	glass	plastic
core diameter $2a$	62.5 100 μm	980 μm
cladding diameter D	125 140 μm	1000 μm
core refractive index n_2	1.48	
cladding refractive index n_1	1.45	

Fibre multimod cu indice gradat

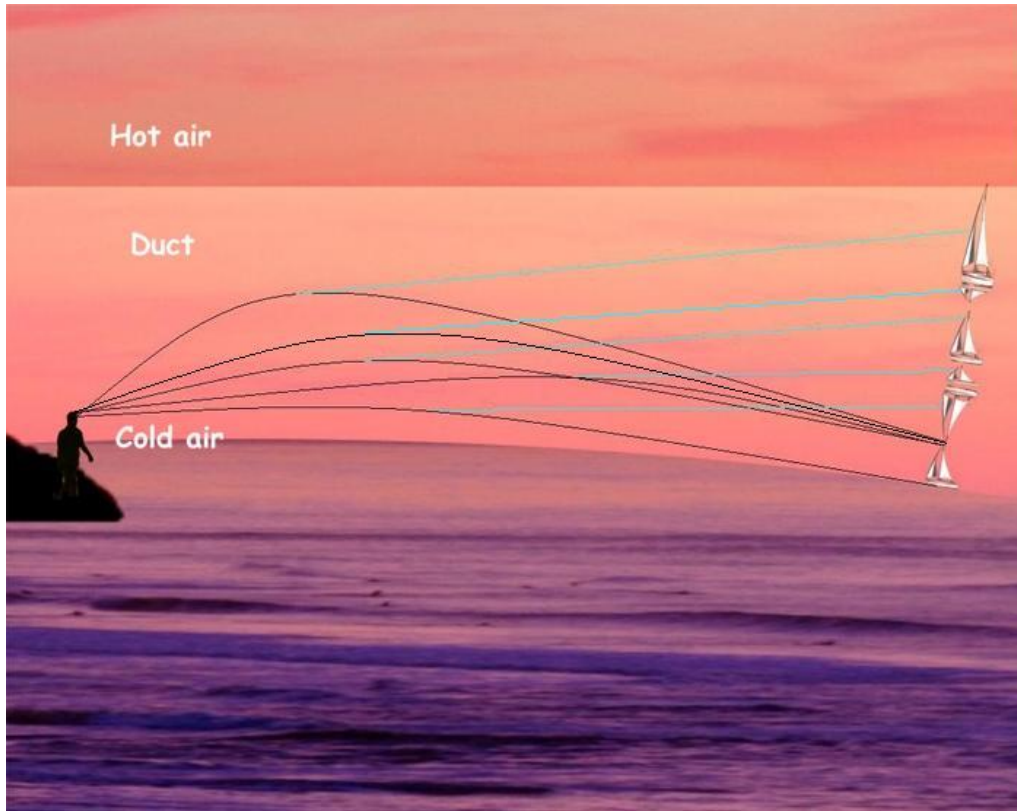


- ▶ 50/125 sau 62.5/125 (μm)
- ▶ 700–1200 MHz · km



Core diameter $2a$	50 or 62.5 μm
Cladding diameter D	125 μm
Maximum refractive index, core	1.46
Relative differential refractive index	0.010

Fata Morgana



Fibre multimod cu indice gradat

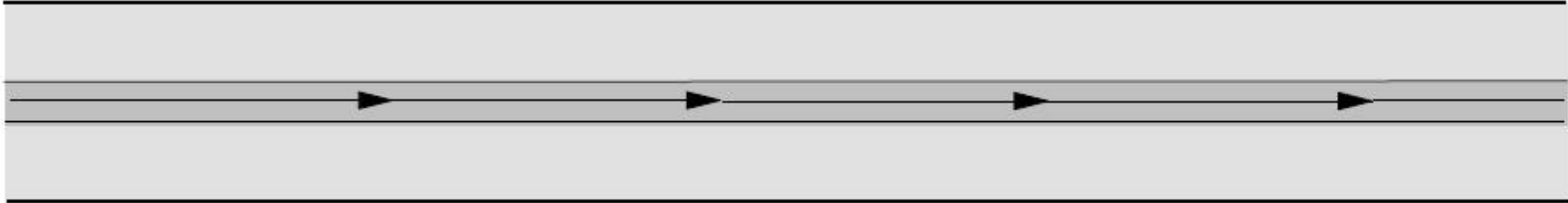


$$n(r) = n_2 \left[1 - \Delta \left(\frac{r}{a} \right)^g \right]$$

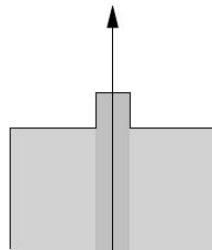
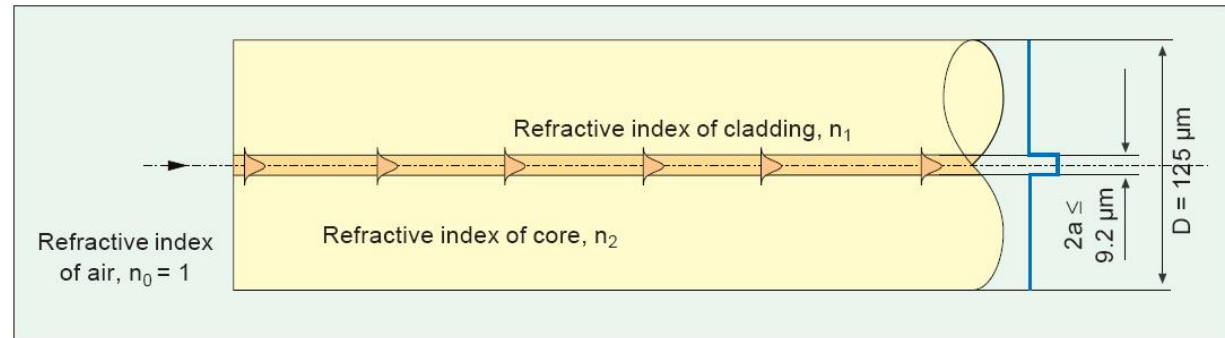
$$\Delta = \frac{NA^2}{2n_2^2} = \frac{n_2^2 - n_1^2}{2n_2^2} \approx \frac{n_2 - n_1}{n_2} \approx \frac{\Delta n}{n} \quad \text{for } \Delta \ll 1$$

- ▶ $g = 1$ - indice gradat triunghiular
- ▶ $g = 2$ - indice gradat parabolic
- ▶ $g = \infty$ - salt de indice

Fibre monomod



- ▶ 6–8/125 (μm)
- ▶ MHz · km
nerelevant
- ▶ MFD – Mode
Field Diameter



Cladding diameter D	125 μm
Core refractive index n_2	1.4485
Cladding refractive index n_1	1.4440
Refractive index differential	0.003 = 0.3%

Ghid cilindric dielectric

► Ecuatiile lui Maxwell in coordonate cilindrice

$$\frac{\partial^2 U}{\partial r^2} + \frac{1}{r} \frac{\partial U}{\partial r} + \frac{1}{r^2} \frac{\partial^2 U}{\partial \phi^2} + \frac{\partial^2 U}{\partial z^2} + n^2 k_o^2 U = 0$$

a – raza miezului
U – E(r) sau H(r)

$$U(r, \phi, z) = u(r) e^{-jl\phi} e^{-j\beta z}, \quad l = 0, \pm 1, \pm 2, \dots$$

$$\frac{d^2 u}{dr^2} + \frac{1}{r} \frac{du}{dr} + \left(n^2(r) k_o^2 - \beta^2 - \frac{l^2}{r^2} \right) u = 0$$

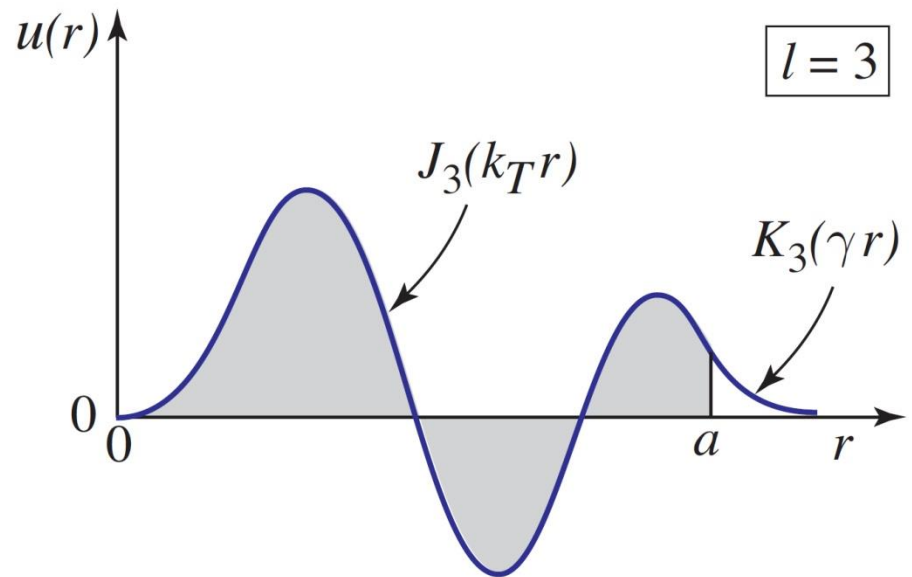
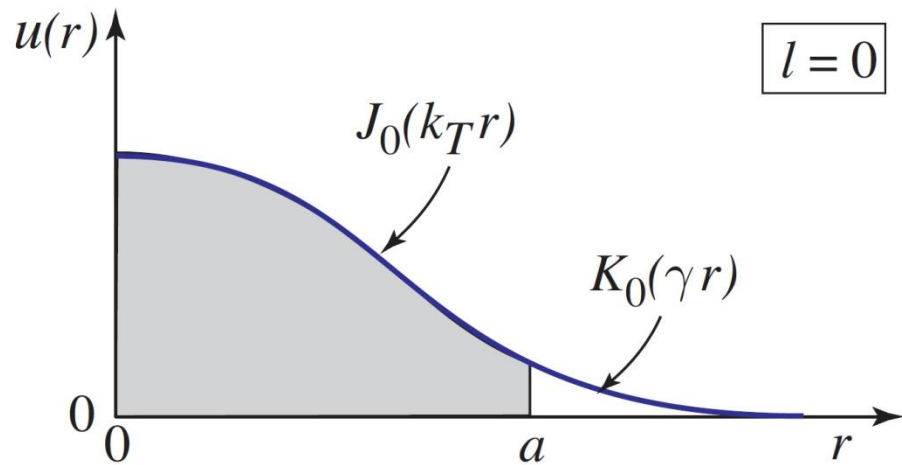
$$\frac{d^2 u}{dr^2} + \frac{1}{r} \frac{du}{dr} + \left(k_T^2 - \frac{l^2}{r^2} \right) u = 0, \quad r < a$$

$$\frac{d^2 u}{dr^2} + \frac{1}{r} \frac{du}{dr} - \left(\gamma^2 + \frac{l^2}{r^2} \right) u = 0, \quad r > a$$

Ghid cilindric dielectric

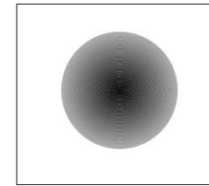
- ▶ solutii proportionale cu functii Bessel

$$u(r) \propto \begin{cases} J_l(k_T r), & r < a \quad (\text{core}) \\ K_l(\gamma r), & r > a \quad (\text{cladding}) \end{cases}$$

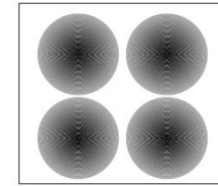


Moduri in fibra

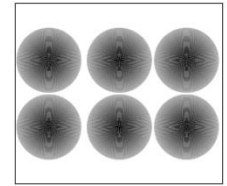
- ▶ Moduri in ghid rectangular



TEM₀₀

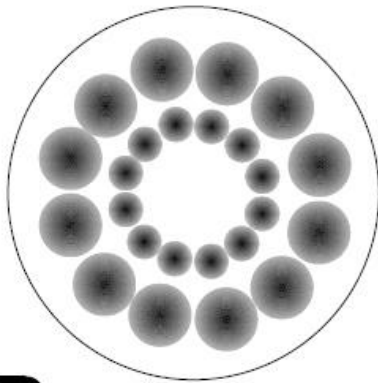


TEM₁₁

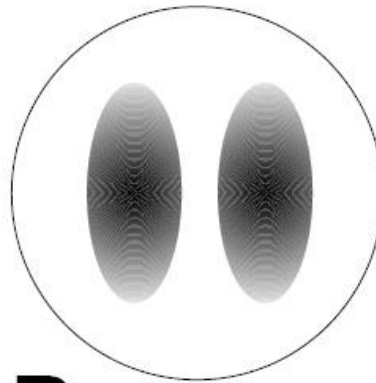


TEM₂₁

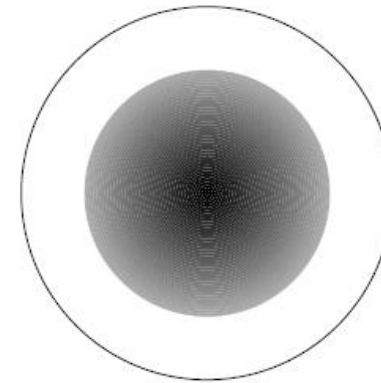
- ▶ Moduri linear polarizate in fibra



LP₆₂

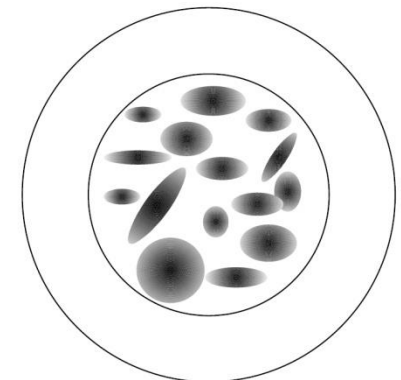


LP₁₁



LP₀₁

“Sparkle” pattern



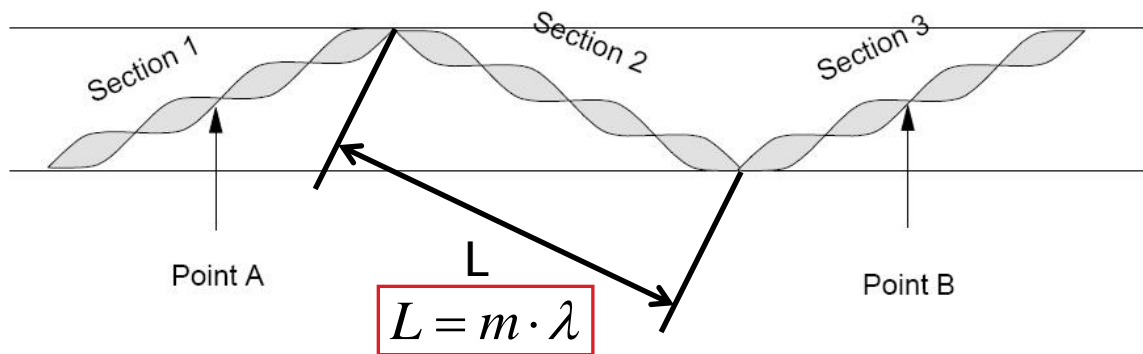
Frecventa normalizata

► Frecventa normalizata

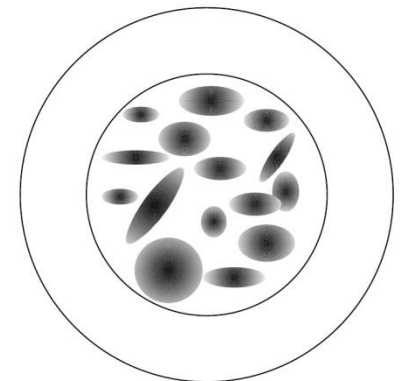
$$V = 2\pi \frac{a}{\lambda} NA = k \cdot a \cdot NA \quad a - \text{raza miezului}$$

$$k = \frac{2\pi}{\lambda}$$

► Numar de moduri

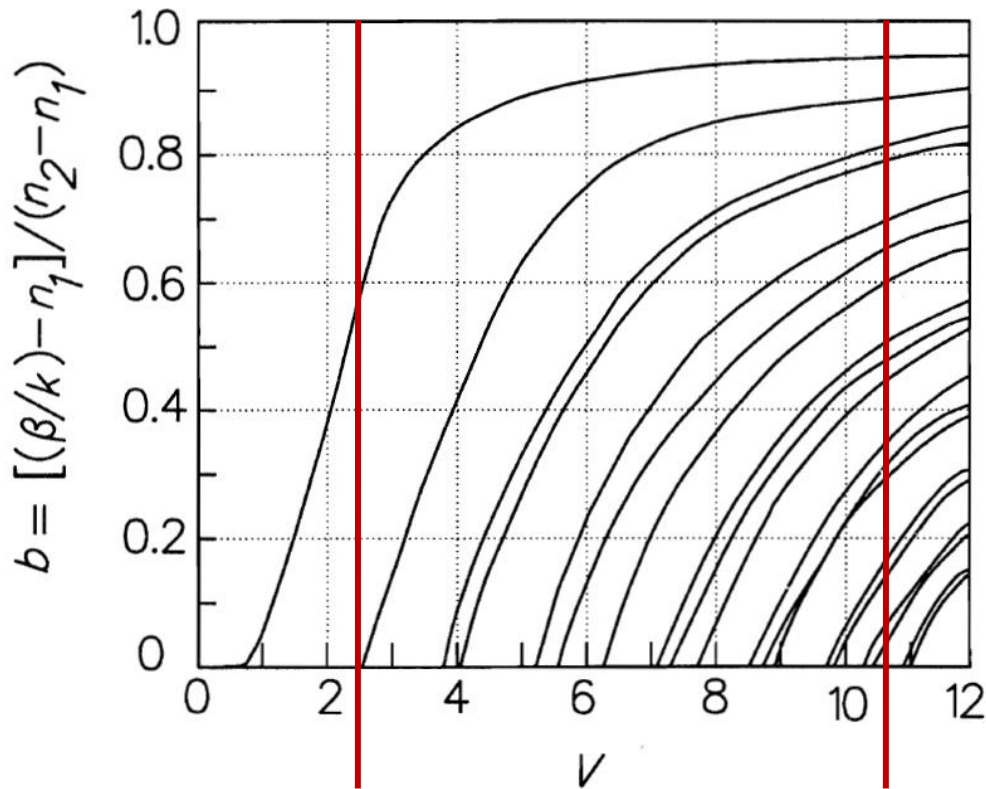


$$N \approx \frac{V^2}{2} \cdot \frac{g}{g+2}$$



Frecventa normalizata – monomod

► Fibre monomod



b – coeficient de propagare modal relativ

$$V \leq V_c = 2.405$$

exista un **singur** mod (solutii fc. Bessel)

$$\lambda \geq \lambda_c = \pi \frac{2a}{V_c} NA = \pi \frac{2a}{2.405} NA$$

Exemplu:

$$2a = 8.5 \mu\text{m}$$

$$NA = 0.11$$

$$\lambda_c = \pi \frac{8.5}{2.405} 0.11 = 1210 \text{nm}$$

Frecventa normalizata

- ▶ Numar de moduri
 - Multimod cu salt de indice

$$g = \infty \Rightarrow N \approx \frac{V^2}{2}$$

- Multimod cu indice gradat

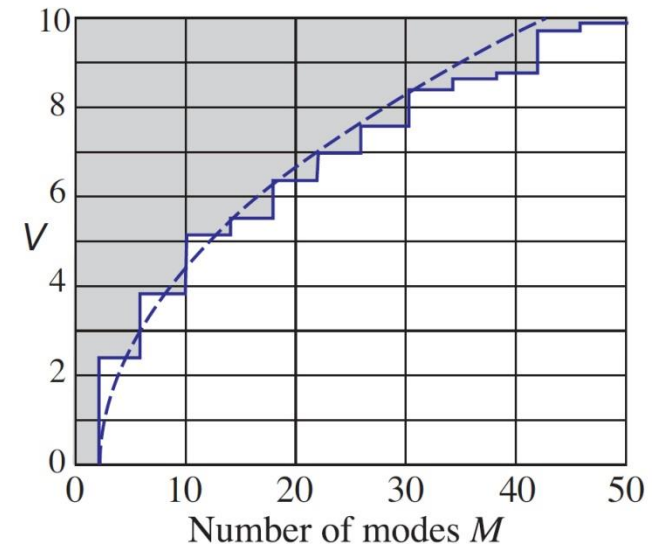
$$g = 2 \Rightarrow N \approx \frac{V^2}{4}$$

- Monomod

$$V \leq V_c = 2.405$$

exista un singur mod (solutii fc. Bessel)

$$N \approx \frac{V^2}{2} \cdot \frac{g}{g+2}$$

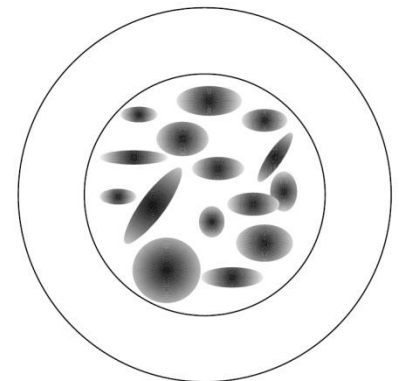


Exemplu

- ▶ fibra tipica multimod
 - $g=2$
 - $2a = 50\mu\text{m} \rightarrow a = 25\mu\text{m}$
 - $NA = 0.2$ la $\lambda = 1\mu\text{m}$

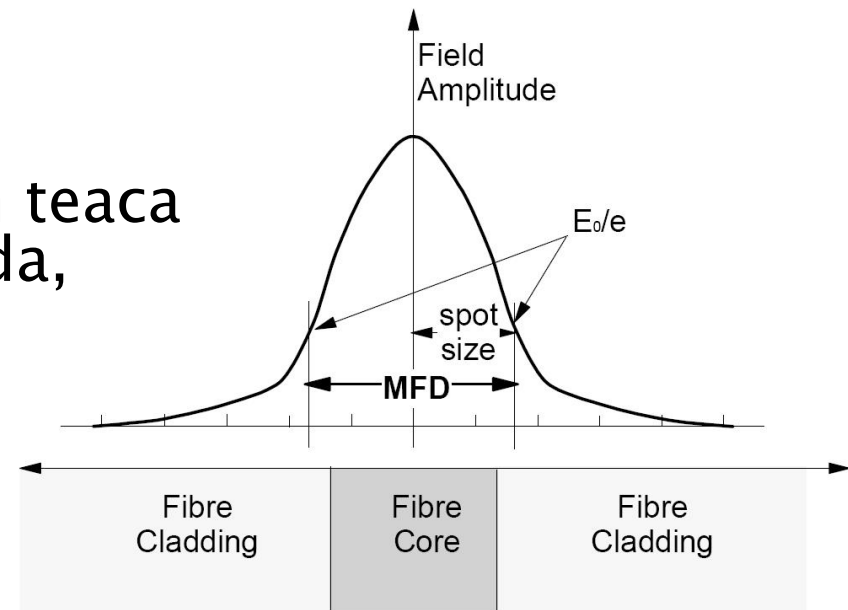
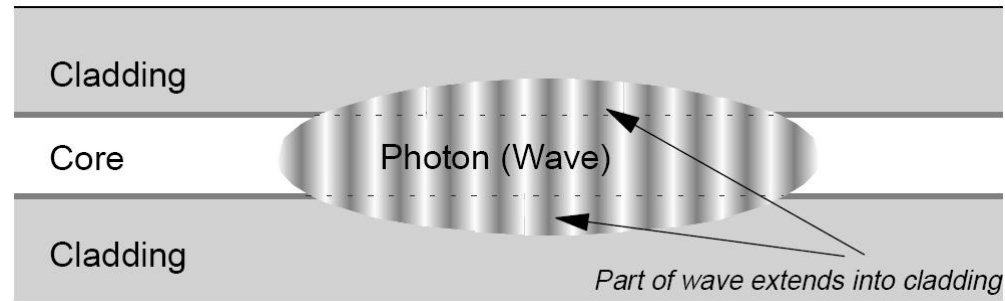
$$V = 2\pi \frac{a}{\lambda} NA = 2\pi \frac{25}{1} 0.2 = 2 \cdot \pi \cdot 5 \approx 31.4$$

$$g = 2 \Rightarrow N = \frac{V^2}{4} = \frac{31.4^2}{4} = 247$$

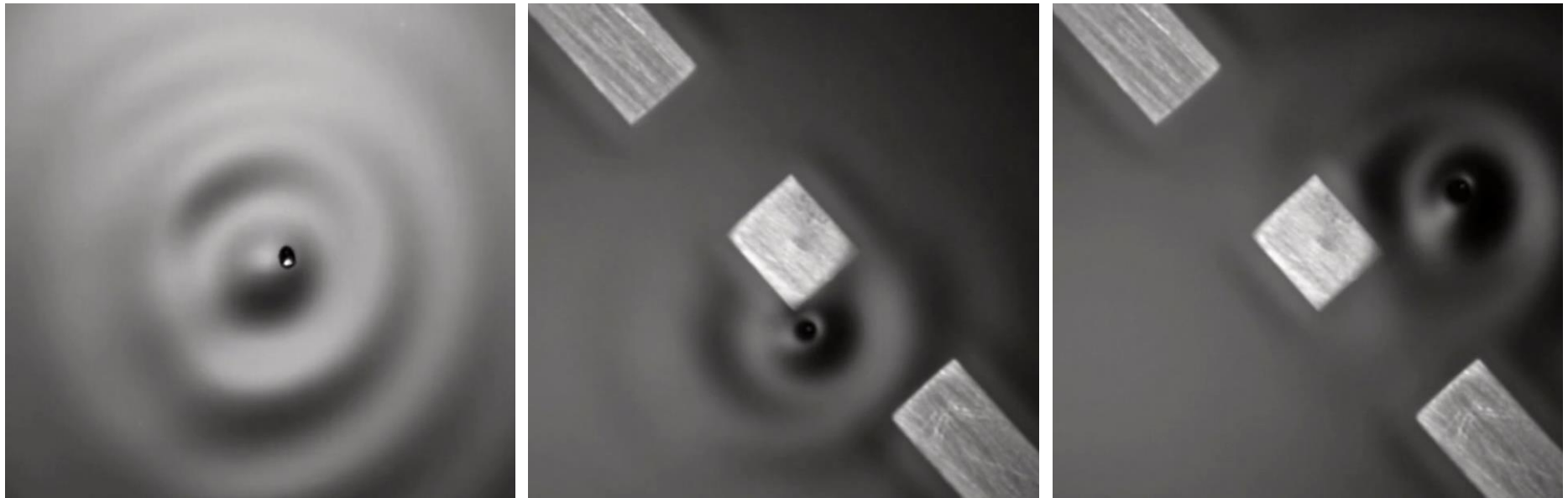


Propagarea in fibra monomod

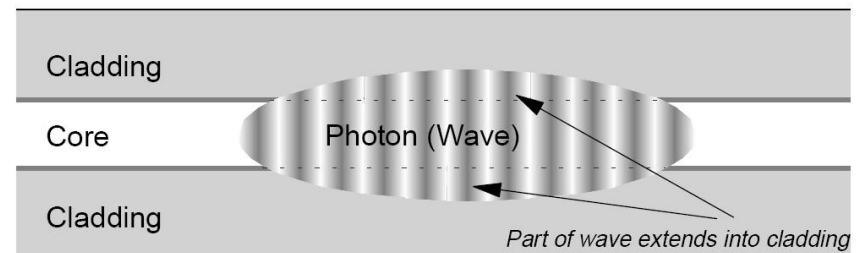
- ▶ Propagarea luminii poate fi explicata doar prin teoria electromagnetica
- ▶ Energia campului se extinde in teaca (diametrul efectiv al spotului luminos – MFD, Mode Field Diameter)
- ▶ $MFD > 2a$
- ▶ Adancimea de patrundere in teaca depinde de lungimea de unda, generand dispersia de ghid



Modelare



Through the Wormhole
S02E07 How Does the Universe Work



Fenomene de interes

- ▶ Cat de departe pot transmite semnalul luminos pe fibra
 - **atenuare**
- ▶ Cat de rapid pot transmite informația
 - dispersie

Reprezentare logaritmică

$$\text{Pierderi [dB]} = 10 \cdot \log_{10} \left(\frac{P_{out}}{P_{in}} \right)$$

$$P[\text{dBm}] = 10 \cdot \log_{10} \left(\frac{P}{P_0} \right) = 10 \cdot \log_{10} \left(\frac{P}{1 \text{ mW}} \right)$$

$$\text{dB} = 10 \cdot \log_{10} (P_2 / P_1)$$

$$\text{dBm} = 10 \cdot \log_{10} (P / 1 \text{ mW})$$

$$0 \text{ dB} = 1$$

$$0 \text{ dBm} = 1 \text{ mW}$$

$$+ 0.1 \text{ dB} = 1.023 (+2.3\%)$$

$$3 \text{ dBm} = 2 \text{ mW}$$

$$+ 3 \text{ dB} = 2$$

$$5 \text{ dBm} = 3 \text{ mW}$$

$$+ 5 \text{ dB} = 3$$

$$10 \text{ dBm} = 10 \text{ mW}$$

$$+ 10 \text{ dB} = 10$$

$$20 \text{ dBm} = 100 \text{ mW}$$

$$-3 \text{ dB} = 0.5$$

$$-3 \text{ dBm} = 0.5 \text{ mW}$$

$$-10 \text{ dB} = 0.1$$

$$-10 \text{ dBm} = 100 \mu\text{W}$$

$$-20 \text{ dB} = 0.01$$

$$-30 \text{ dBm} = 1 \mu\text{W}$$

$$-30 \text{ dB} = 0.001$$

$$-60 \text{ dBm} = 1 \text{ nW}$$

$$[\text{dBm}] + [\text{dB}] = [\text{dBm}]$$

$$[\text{dBm/Hz}] + [\text{dB}] = [\text{dBm/Hz}]$$

$$[x] + [\text{dB}] = [x]$$

Calculul atenuarii

$$\text{Pierderi} = \frac{P_{out}}{P_{in}}$$

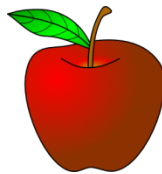
$$\text{Pierderi[dB]} = [-] 10 \cdot \log_{10} \left(\frac{P_{out}}{P_{in}} \right)$$

$$\text{Pierderi[dB]} = [-] 10 \cdot \log_{10} \left(\frac{P_{out}}{P_0} \cdot \frac{P_0}{P_{in}} \right) = [-] 10 \cdot \left[\log_{10} \left(\frac{P_{out}}{P_0} \right) - \log_{10} \left(\frac{P_{in}}{P_0} \right) \right]$$

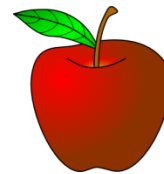
$$\text{Pierderi[dB]} = [-] (P_{out} [\text{dBm}] - P_{in} [\text{dBm}])$$



=



-

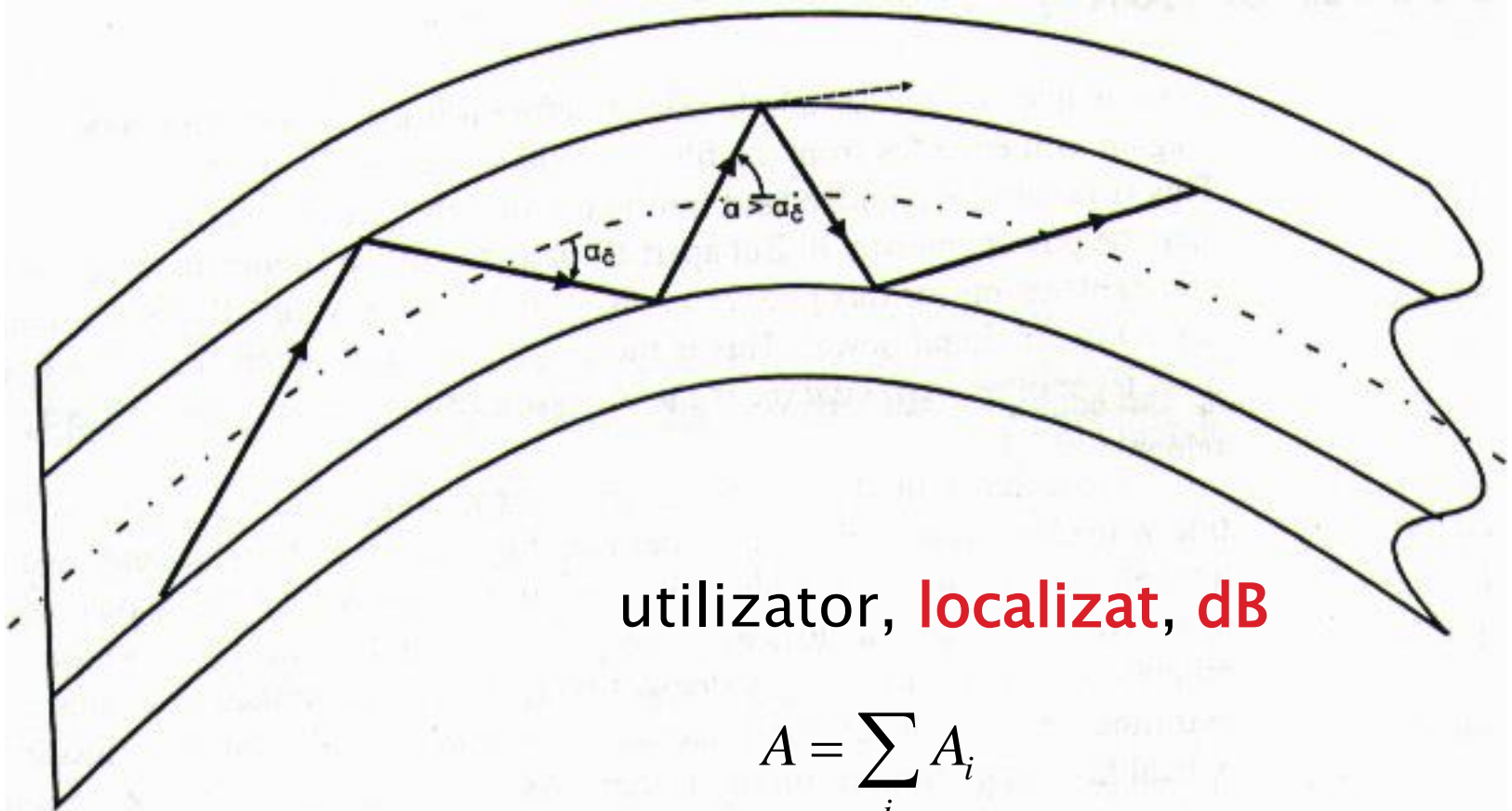


$$\text{Atenuare[dB/km]} = \frac{\text{Pierderi[dB]}}{\text{lungime[km]}}$$

Atenuare

- ▶ Macrocurburi
 - utilizator, **localizat**, dB
- ▶ Discontinuitate in fibra
 - utilizator, **localizat**, dB
- ▶ Microcurburi
 - **distribuit**, tehnologie, dB/km
- ▶ Imprastiere
 - **distribuit**, tehnologie, dB/km
- ▶ Absorbție
 - **distribuit**, material, dB/km

Macrocurburi



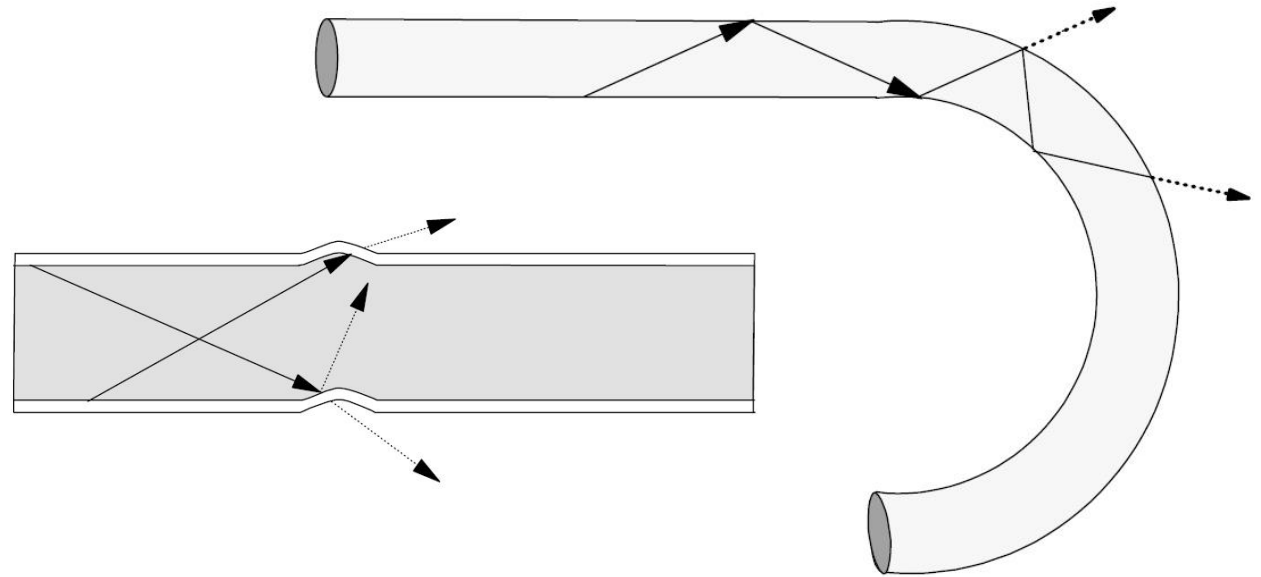
utilizator, **localizat**, dB

$$A = \sum_i A_i$$

$$A = N \cdot A_i$$

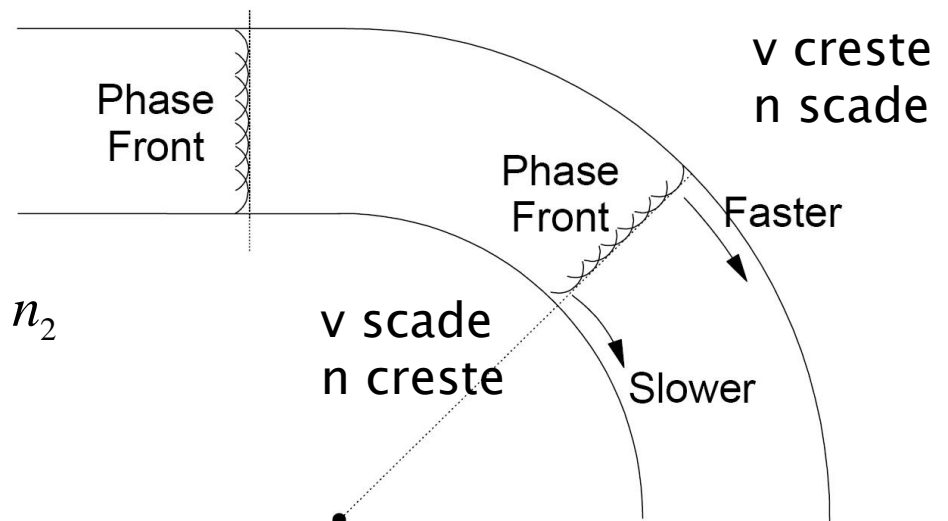
Efectul curburilor

▶ Multimod



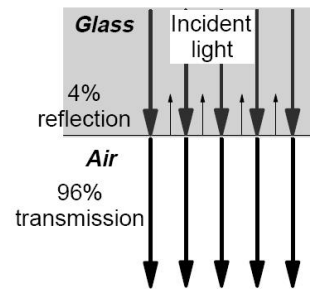
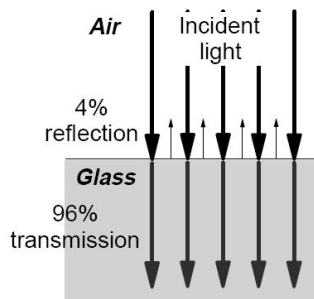
▶ Monomod

$$R > R_C \Rightarrow n_{1,ext} > n_2$$



Discontinuitate in fibra

- ▶ Apare cand nu putem considera fibra un singur ghid dielectric
 - defectiuni
 - conectori

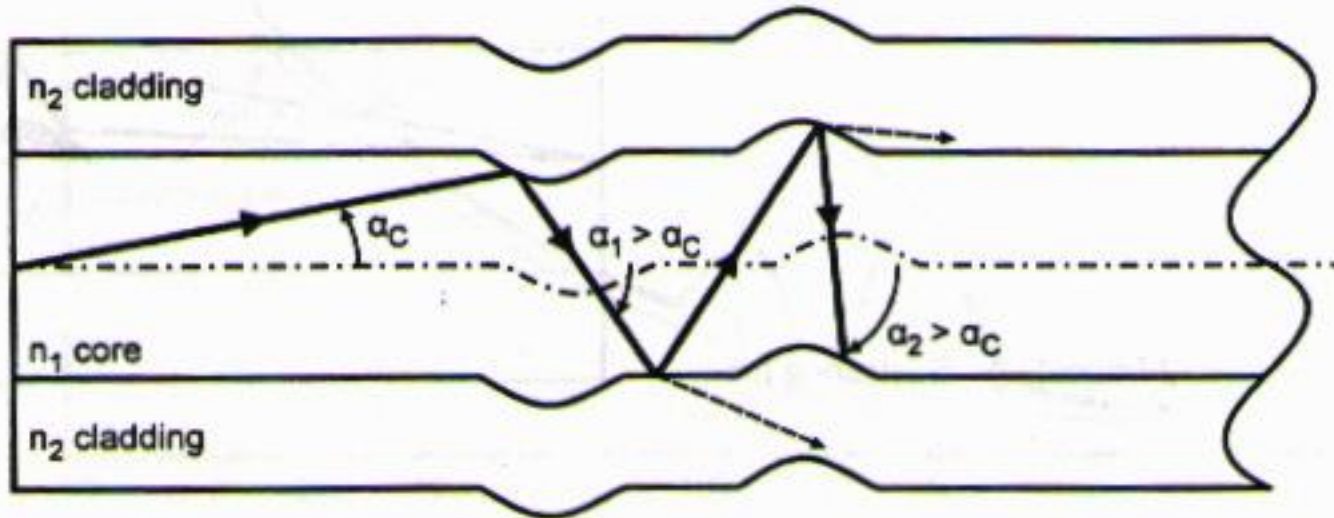


utilizator, **localizat**, dB

$$A = \sum_i A_i$$

$$A = N \cdot A_i$$

Microcurburi

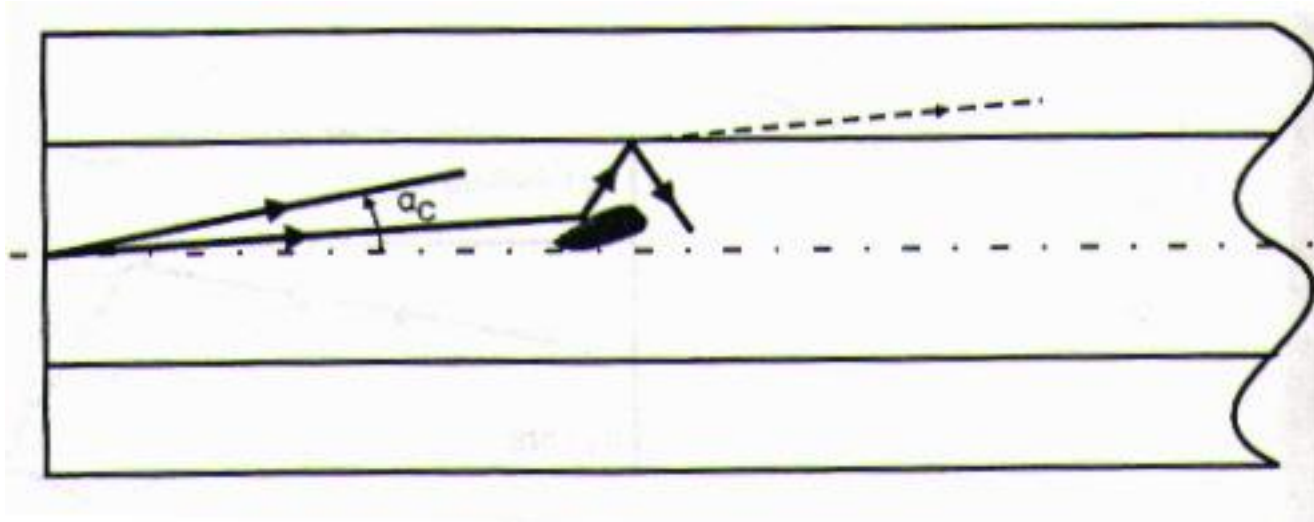


distribuit, tehnologie, **dB/km**

$$A = A_i \cdot L$$

$$A[dB] = A_i[dB / km] \cdot L[km]$$

Imprastiere

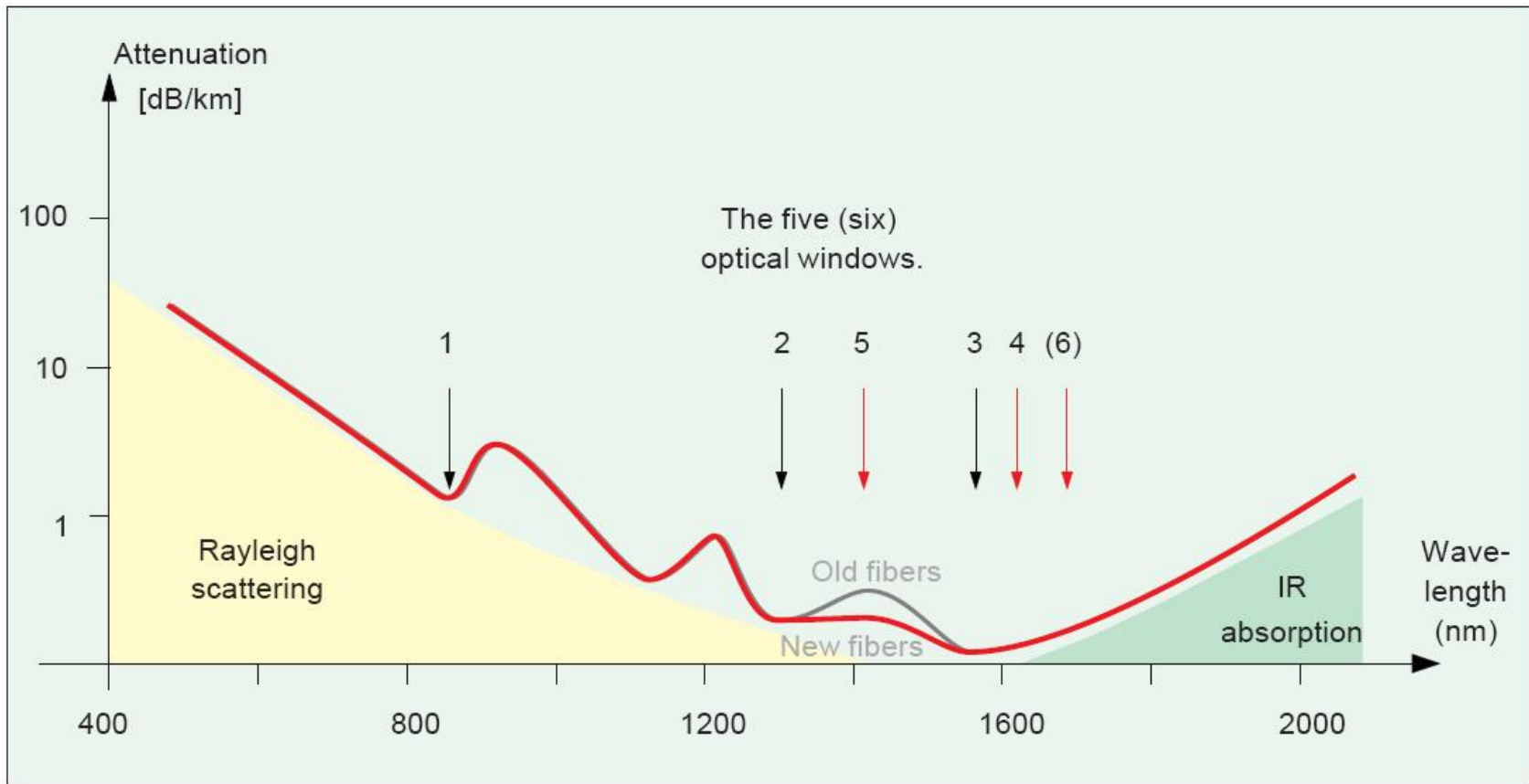


distribuit, tehnologie, **dB/km**

$$A = A_i \cdot L$$

$$A[dB] = A_i[dB/km] \cdot L[km]$$

Absorbtie

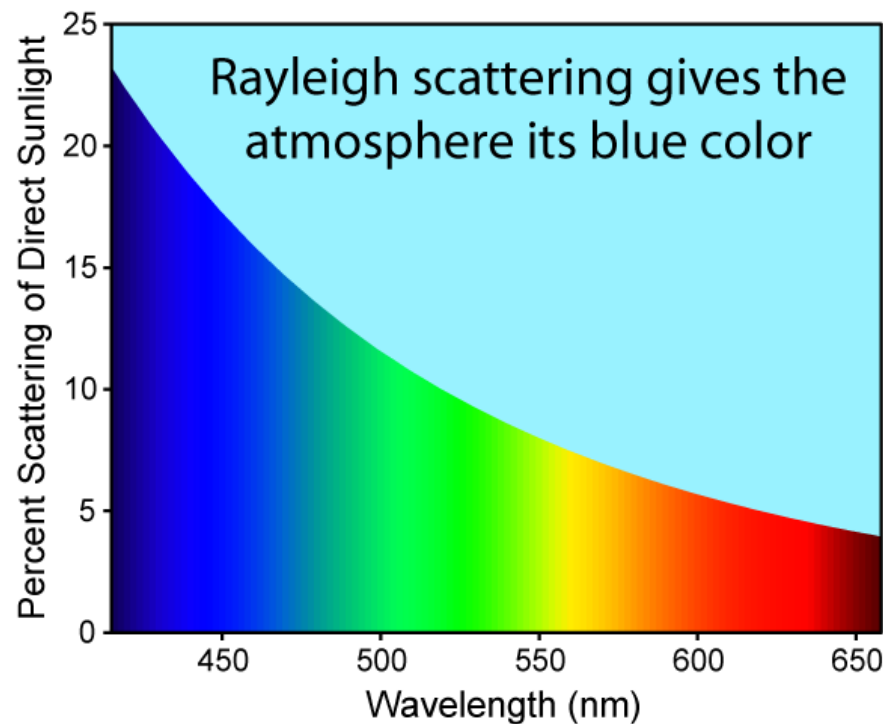


distribuit, material, dB/km

$$A[dB] = A_i[dB/km] \cdot L[km]$$

Difractie Rayleighgh

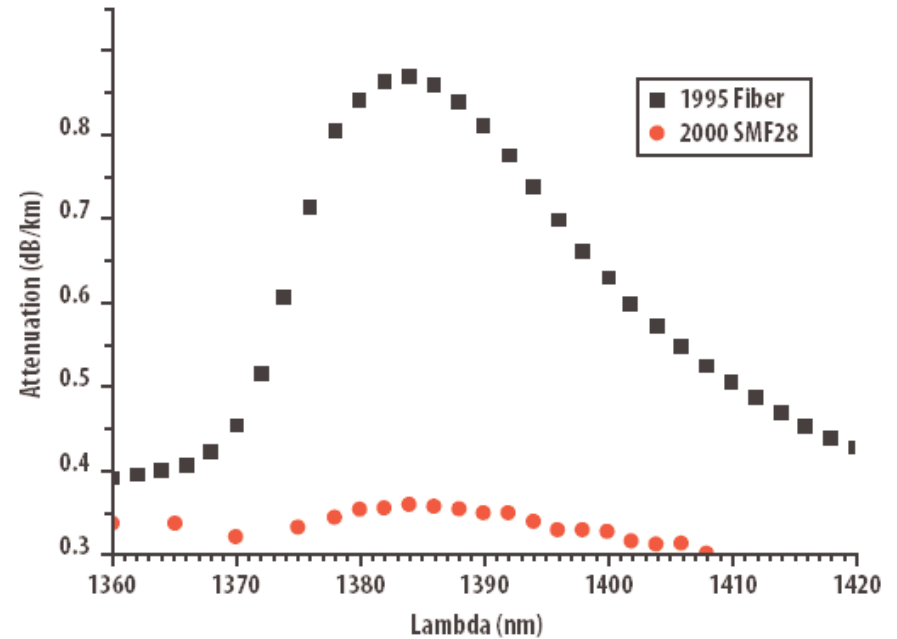
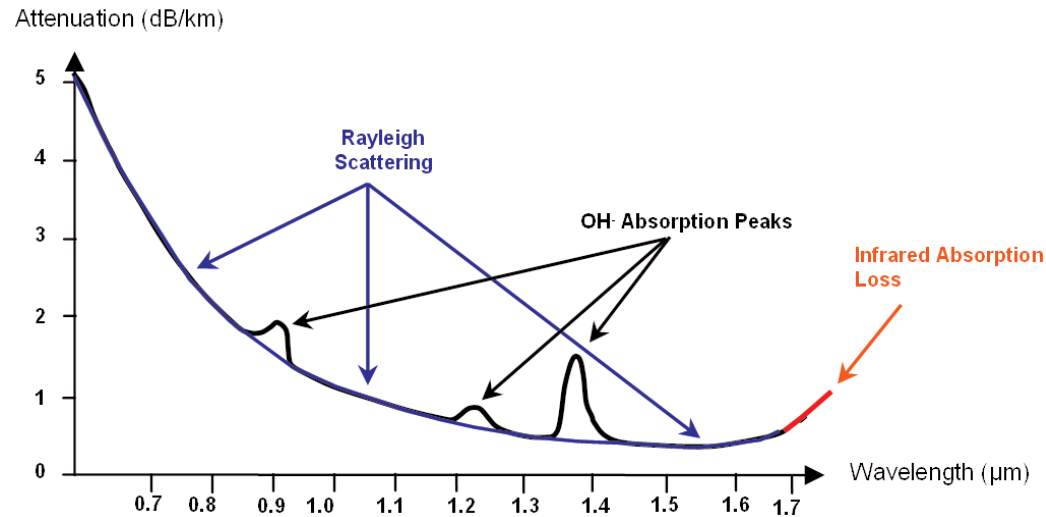
- ▶ imprastierea luminii (si a altor radiatii electromagnetice) de particule (molecule) mult mai mici decat lungimea de unda



$$A \sim \frac{1}{\lambda^4}$$

Absorbentie OH

- ▶ Absorbentie
 - 950nm
 - 1244nm
 - 1383nm
- ▶ Apa!



Fiber Attenuation Comparison

Atenuare

$$E_y(z_1) = Ct \cdot e^{-\alpha \cdot z_1} \cdot e^{j(\omega t - \beta \cdot z_1)}$$

$$E_y(z_2) = Ct \cdot e^{-\alpha \cdot z_2} \cdot e^{j(\omega t - \beta \cdot z_2)}$$

$$W, P \sim \int E^2$$

$$A = \frac{P_2}{P_1} = \frac{Ct^2 \cdot e^{-2\alpha \cdot z_2}}{Ct^2 \cdot e^{-2\alpha \cdot z_1}} = e^{-2\alpha \cdot (z_2 - z_1)}$$

$$A[dB] = 10 \log_{10} \frac{P_2}{P_1} = 10 \log_{10} \left[e^{-2\alpha \cdot (z_2 - z_1)} \right]$$

$$A[dB] = -20 \cdot \alpha \cdot (z_2 - z_1) \log_{10} e = -8.686 \cdot \alpha \cdot (z_2 - z_1)$$

$$A / L [dB / km] = -8.686 \cdot \alpha < 0$$

- ▶ Atenuarea se exprima de obicei in **dB/km**
 - ▶ de obicei valori pozitive
 - ▶ semnul = **implicit**

Calculul atenuarii

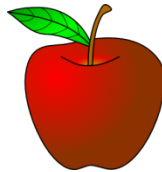
$$\text{Pierderi} = \frac{P_{out}}{P_{in}}$$

$$\text{Pierderi[dB]} = [-] 10 \cdot \log_{10} \left(\frac{P_{out}}{P_{in}} \right)$$

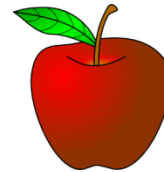
$$\text{Pierderi[dB]} = [-] (P_{out} [\text{dBm}] - P_{in} [\text{dBm}])$$



=



-



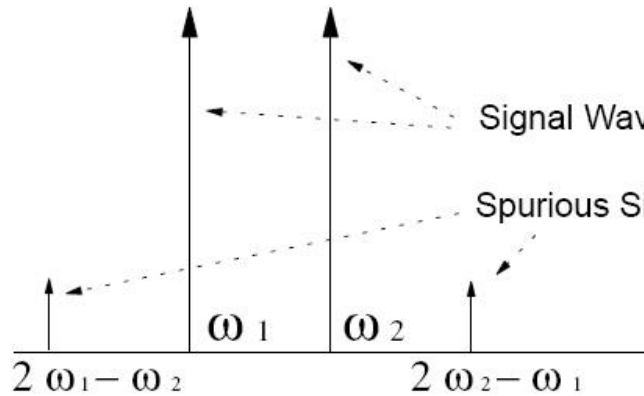
$$\text{Atenuare[dB/km]} = \frac{\text{Pierderi[dB]}}{\text{lungime[km]}}$$

Efecte neliniare in fibra

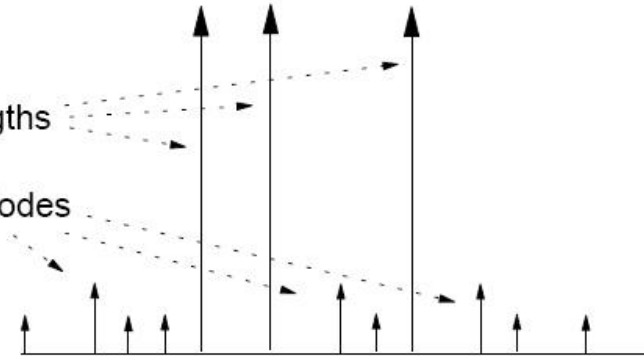
- ▶ **Stimulated Brillouin Scattering, SBC**
 - difractia luminii inspre emitator datorita undelor mecano-acustice generate in fibra
 - 6–10 dBm
- ▶ **Stimulated Raman Scattering, SRS**
 - interactiunea luminii cu vibratiile moleculare
 - 27 dBm (~1W)
- ▶ **Self Phase Modulation, SPM**
 - Frontiera impulsului implica indice de refractie variabil in timp moduland faza impulsului
 - 5 dBm
 - Cross Phase Modulation, CPM
- ▶ **Four-Wave Mixing, FWM**
 - 0 dBm

Four-Wave Mixing, FWM

Two Channels



Three Channels

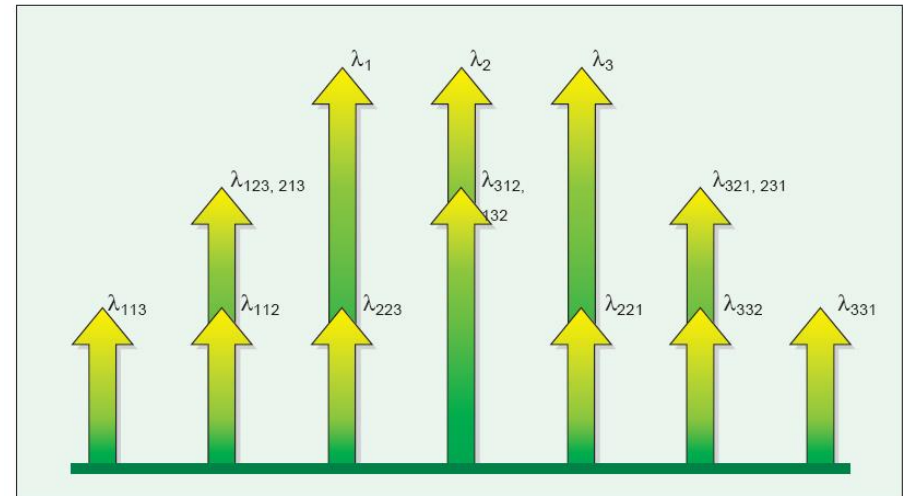


$$NL = \frac{1}{2}(N^3 - N^2)$$

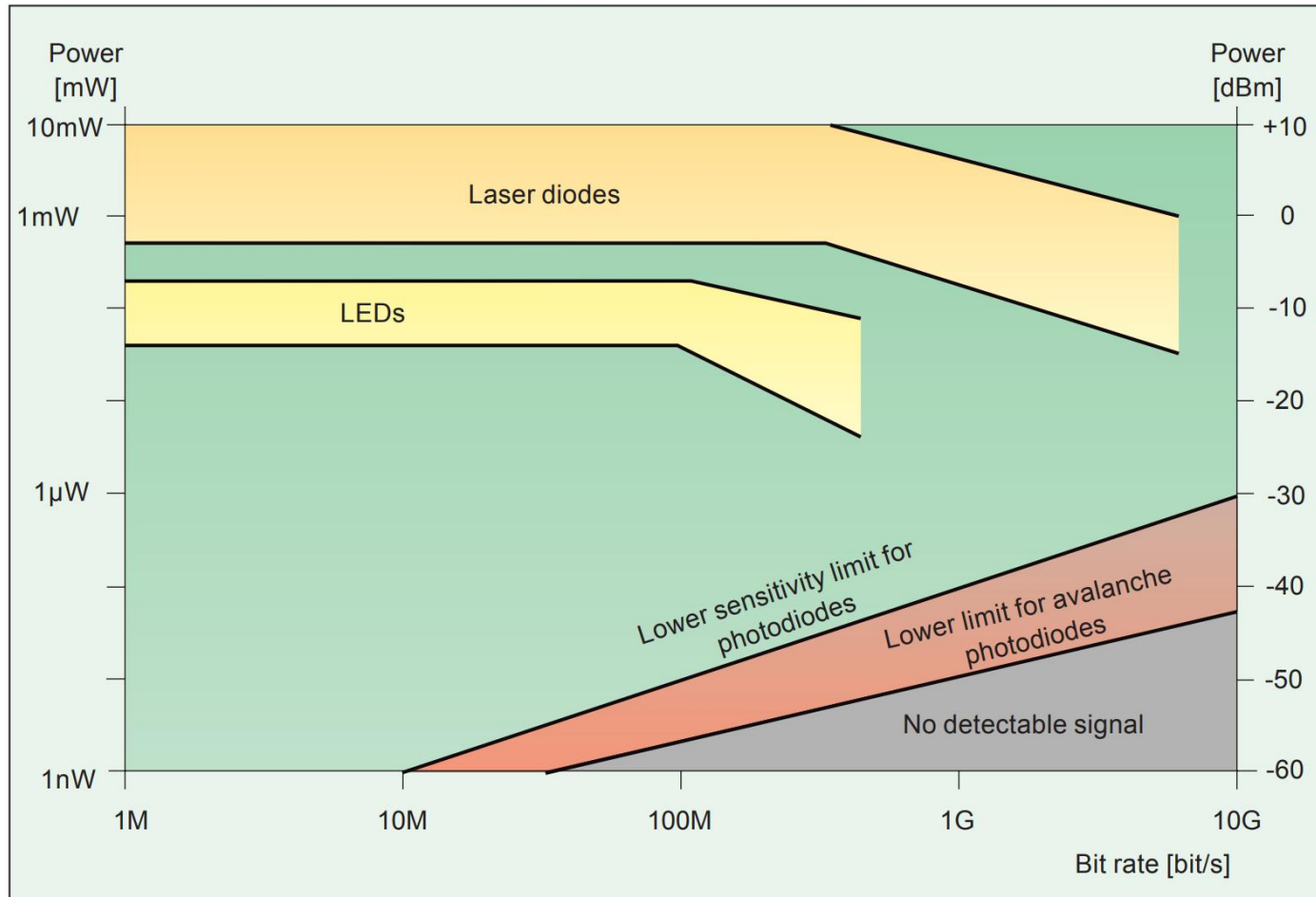
$$N = 2, NL = 4$$

$$N = 3, NL = 9$$

$$N = 16, NL = 1920$$



Limite putere/bandă a dispozitivelor optoelectronice



Contact

- ▶ Laboratorul de microunde si optoelectronica
- ▶ <http://rf-opto.etti.tuiasi.ro>
- ▶ rdamian@etti.tuiasi.ro