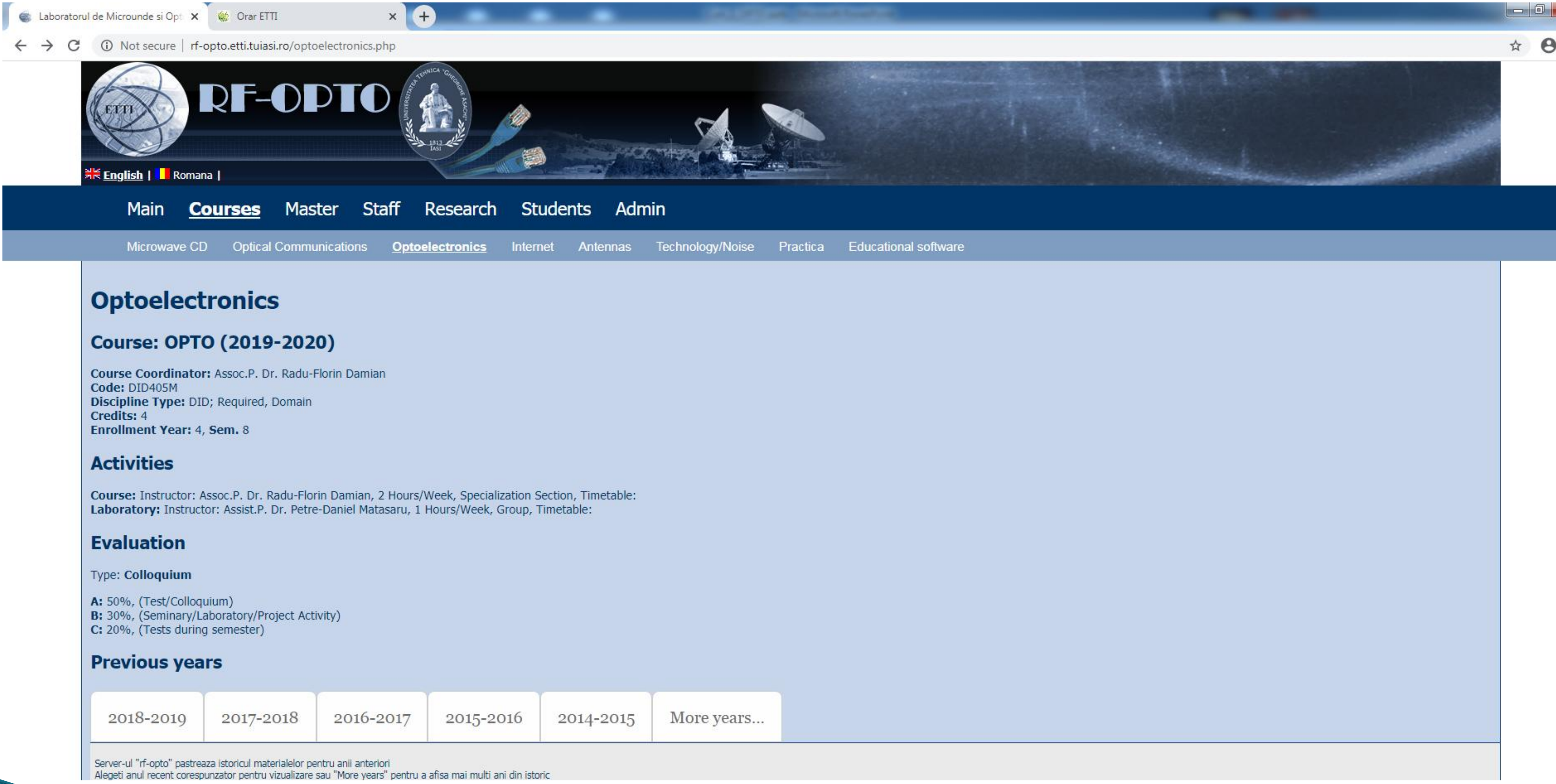
Optoelectronică

Curs 4
2019/2020

Disciplina 2019/2020

- 2C/1L Optoelectronică OPTO
- Minim 7 prezente curs + laborator
- Curs – conf. Radu Damian
  - an IV μE
  - Vineri 8-11, P5
  - E – 70% din nota
    - **20% test la curs**, saptamana 4-5?
  - probleme + (? 1 subiect teorie) + (2p prez. curs)
  - toate materialele permise
- Laborator – sl. Daniel Matasaru
  - an IV μE
    - Joi 8-14 impar
  - L – 30% din nota (+Caiet de laborator)

Documentatie



Laboratorul de Microunde si Opt | Orar ETTI

Not secure | rf-opto.etti.tuiasi.ro/optoelectronics.php

RF-OPTO

English | Romana |

Main | Courses | Master | Staff | Research | Students | Admin

Microwave CD | Optical Communications | Optoelectronics | Internet | Antennas | Technology/Noise | Practica | Educational software

Optoelectronics

Course: OPTO (2019-2020)

Course Coordinator: Assoc.P. Dr. Radu-Florin Damian
Code: DID405M
Discipline Type: DID; Required, Domain
Credits: 4
Enrollment Year: 4, **Sem.** 8

Activities

Course: Instructor: Assoc.P. Dr. Radu-Florin Damian, 2 Hours/Week, Specialization Section, Timetable:
Laboratory: Instructor: Assist.P. Dr. Petre-Daniel Matasaru, 1 Hours/Week, Group, Timetable:

Evaluation

Type: **Colloquium**

A: 50%, (Test/Colloquium)
B: 30%, (Seminary/Laboratory/Project Activity)
C: 20%, (Tests during semester)

Previous years

2018-2019 | 2017-2018 | 2016-2017 | 2015-2016 | 2014-2015 | More years...

Server-ul "rf-opto" pastreaza istoricul materialelor pentru anii anteriori
Alegeti anul recent corespunzator pentru vizualizare sau "More years" pentru a afisa mai multi ani din istoric

Istoric

Optoelectronics

Course: OPTO (2019-2020)

Course Coordinator: Assoc.P. Dr. Radu-Florin Damian
Code: DID405M
Discipline Type: DID; Required, Domain
Credits: 4
Enrollment Year: 4, **Sem.** 8

Activities

Course: Instructor: Assoc.P. Dr. Radu-Florin Damian, 2 Hours/Week, Specialization Section, Timetable:
Laboratory: Instructor: Assist.P. Dr. Petre-Daniel Matasaru, 1 Hours/Week, Group, Timetable:

Evaluation

Type: **Colloquium**

A: 50%, (Test/Colloquium)
B: 30%, (Seminary/Laboratory/Project Activity)
C: 20%, (Tests during semester)

Previous years

2018-2019 | 2017-2018 | 2016-2017 | 2015-2016 | 2014-2015 | More years...

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Alegeti anul recent corespunzator pentru vizualizare sau "More years" pentru a afisa mai multi ani din istoric

Istoric 2004-2019

Previous years

2018-2019 | 2017-2018 | 2016-2017 | 2015-2016 | 2014-2015 | More years...

Optoelectronics

Course: OPTO (2018-2019)

Course Coordinator: Assoc.P. Dr. Radu-Florin Damian
Code: DIS405M
Discipline Type: DID; Required, Domain
Credits: 3
Enrollment Year: 4, **Sem.** 8

Activities

Course: Instructor: Assoc.P. Dr. Radu-Florin Damian, 2 Hours/Week, Specialization Se
Laboratory: Instructor: Assist.P. Dr. Petre-Daniel Matasaru, 1 Hours/Week, Group, Ti

Evaluation

Type: **Colloquium**

A: 50%, (Test/Colloquium)
B: 30%, (Seminary/Laboratory/Project Activity)
C: 20%, (Tests during semester)

Grades

Aggregate Results

Attendance

Previous years

2018-2019 | 2017-2018 | 2016-2017 | 2015-2016 | 2014-2015 | 2013-2014 | 2012-201

Optoelectronics, Structures, Technologies, Circuits

Course: OSTC (2013-2014)

Course Coordinator: Assoc.P. Dr. Radu-Florin Damian
Code: DIS405M
Discipline Type: DIS; Required, Specialty
Credits: 4
Enrollment Year: 4, **Sem.** 7

Activities

Course: Instructor: Assoc.P. Dr. Radu-Florin Damian, 2 Hours/Week, Specialization Section, Timetable:
Laboratory: Instructor: Assist.P. Dr. Petre-Daniel Matasaru, 1 Hours/Week, Half Group, Timetable:

Evaluation

Type: **Colloquium**

A: 66%, (Test/Colloquium)
B: 17%, (Seminary/Laboratory/Project Activity)
D: 17%, (Homework/Specialty papers)

Grades

Aggregate Results

Materials

Documentatie

- RF-OPTO
  - http://rf-opto.etti.tuiasi.ro
- Fotografie
  - de trimis prin email: rdamian@etti.tuiasi.ro
  - necesara la laborator/curs

Examen

- subiecte **individuale**

Reprezentare logaritmică

$dB = 10 \cdot \log_{10}(P_2 / P_1)$

$dBm = 10 \cdot \log_{10}(P / 1\ mW)$

0 dB	= 1
+ 0.1 dB	= 1.023 (+2.3%)
+ 3 dB	= 2
+ 5 dB	= 3
+ 10 dB	= 10
–3 dB	= 0.5
–10 dB	= 0.1
–20 dB	= 0.01
–30 dB	= 0.001

0 dBm	= 1 mW
3 dBm	= 2 mW
5 dBm	= 3 mW
10 dBm	= 10 mW
20 dBm	= 100 mW
–3 dBm	= 0.5 mW
–10 dBm	= 100 μW
–30 dBm	= 1 μW
–60 dBm	= 1 nW

[dBm] + [dB] = [dBm]

[dBm/Hz] + [dB] = [dBm/Hz]

[x] + [dB] = [x]

Recapitulare

Ultima (online)

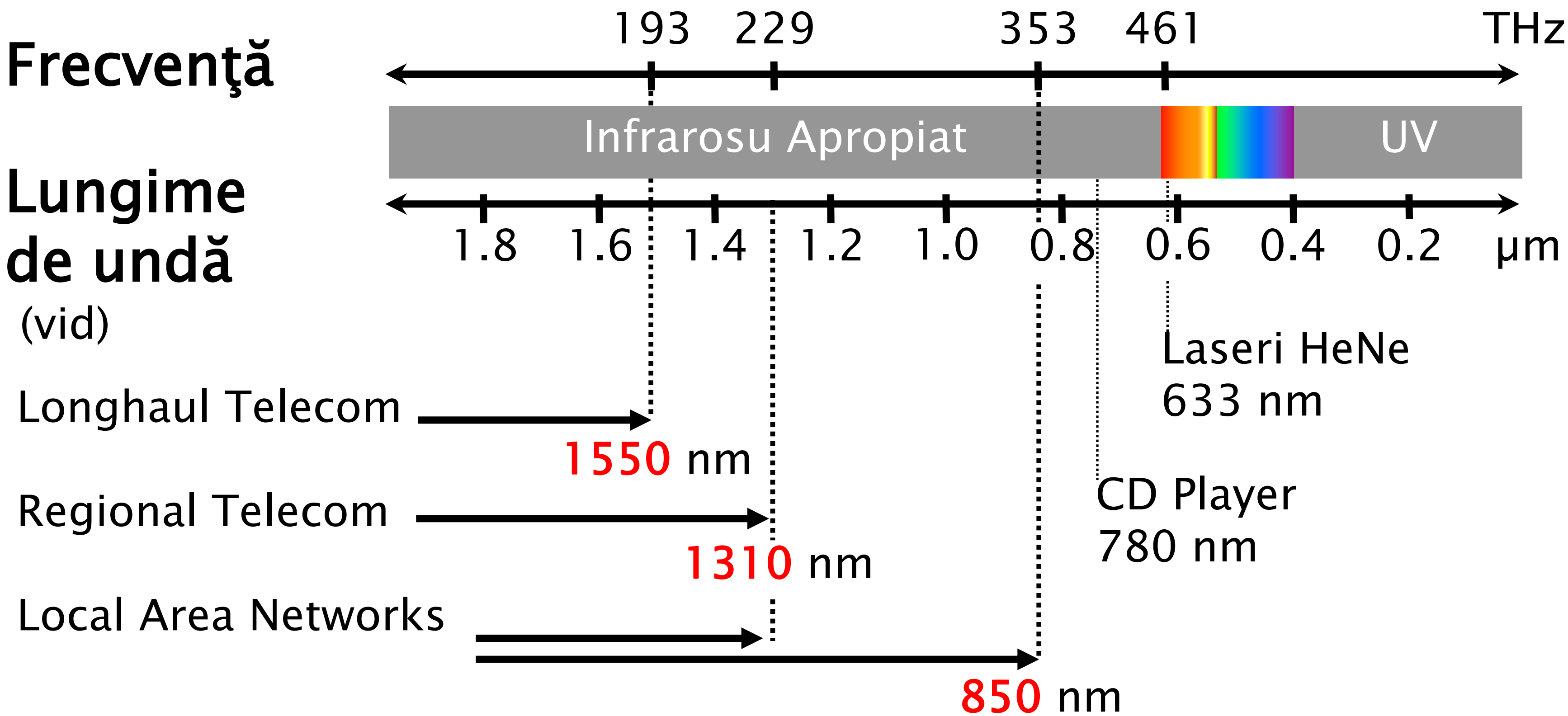
Introducere

Capitolul 1

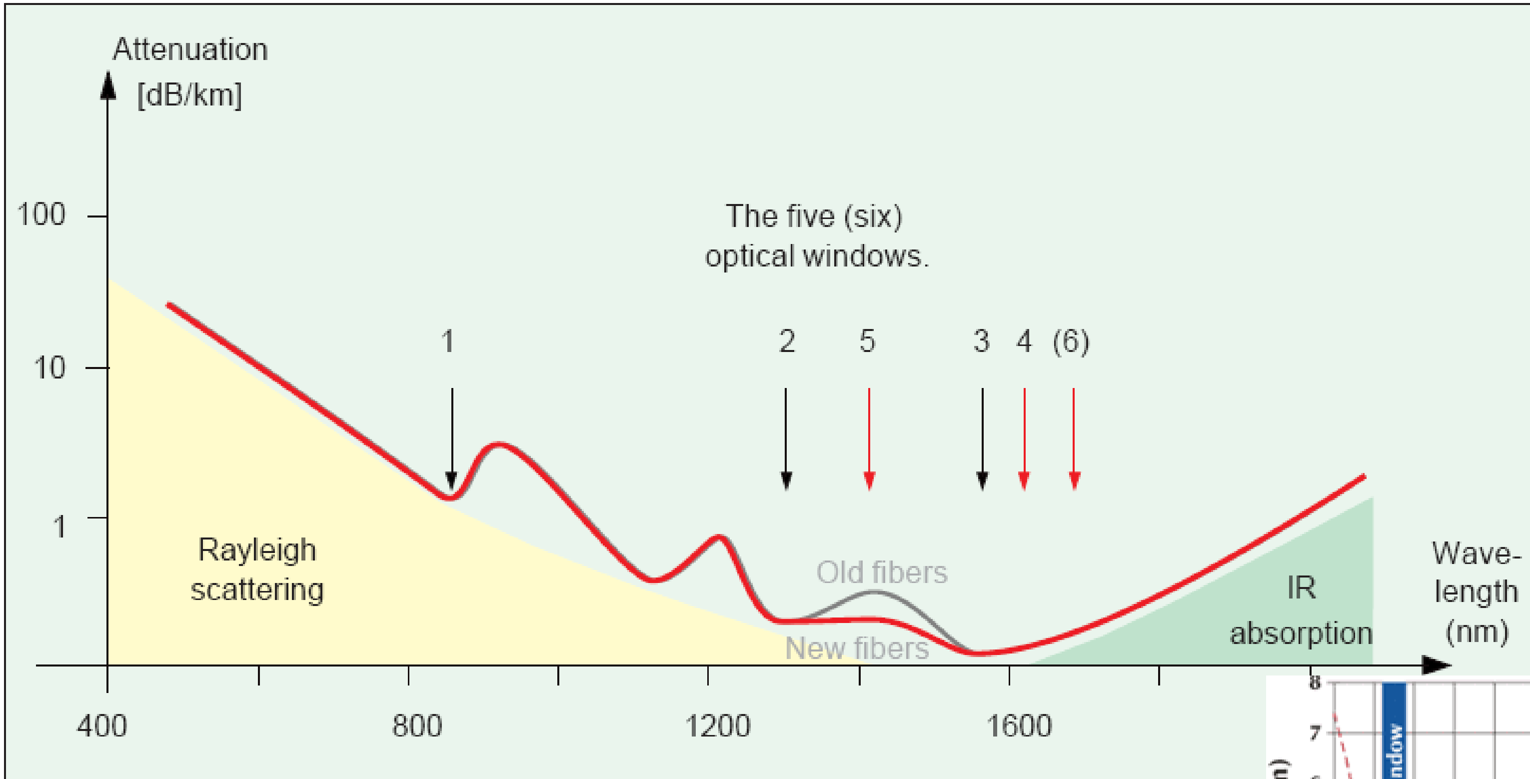
Aplicatii majore

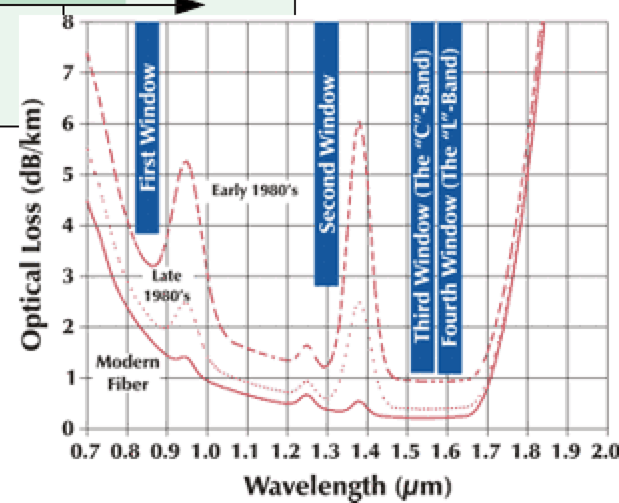
- Comunicatii
  - Infrarosu (InGaAsP)
- Vizibil
  - Spectru vizibil (GaAlAs)
- Iluminare
  - Putere ridicata, lumina alba (GaInN)

Benzi de lucru in comunicaţiile optice



Atenuarea în fibra optică (SiO_2)





850nm, 1310nm, 1550nm

Aplicatii majore

- Comunicatii
  - Infrarosu (InGaAsP)
- Vizibil
  - Spectru vizibil (GaAlAs)
- Iluminare
  - Putere ridicata, lumina alba (GaInN)

Aplicatii majore

- Comunicatii
  - Infrarosu (InGaAsP)
- Vizibil
  - Spectru vizibil (GaAlAs)
- Iluminare
  - Putere ridicata, lumina alba (GaInN)

Lumina ca undă electromagnetică

Capitolul 2

Parametri, dependenta de mediu

$$\eta_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}} = 377\Omega$$

$$c_0 = \frac{1}{\sqrt{\varepsilon_0 \cdot \mu_0}} = 2{,}99790 \cdot 10^8 \ m/s$$

$n = 1$

$$T = \frac{2\pi}{\omega} = \frac{1}{f}$$

$$\lambda_0 = \frac{2\pi}{\beta} = \frac{c_0}{f}$$

$$\eta = \frac{\eta_0}{n}$$

$$c = \frac{c_0}{n}$$

$n = \sqrt{\varepsilon_r}$

$$T = \frac{2\pi}{\omega} = \frac{1}{f}$$

$$\lambda = \frac{c_0}{n \cdot f} = \frac{\lambda_0}{n}$$

$$\lambda = \lambda(n)$$
$$f = \text{indep.}$$

ITU G.692

"the allowed channel frequencies are based on a 50 GHz grid with the reference frequency at 193.10 THz"

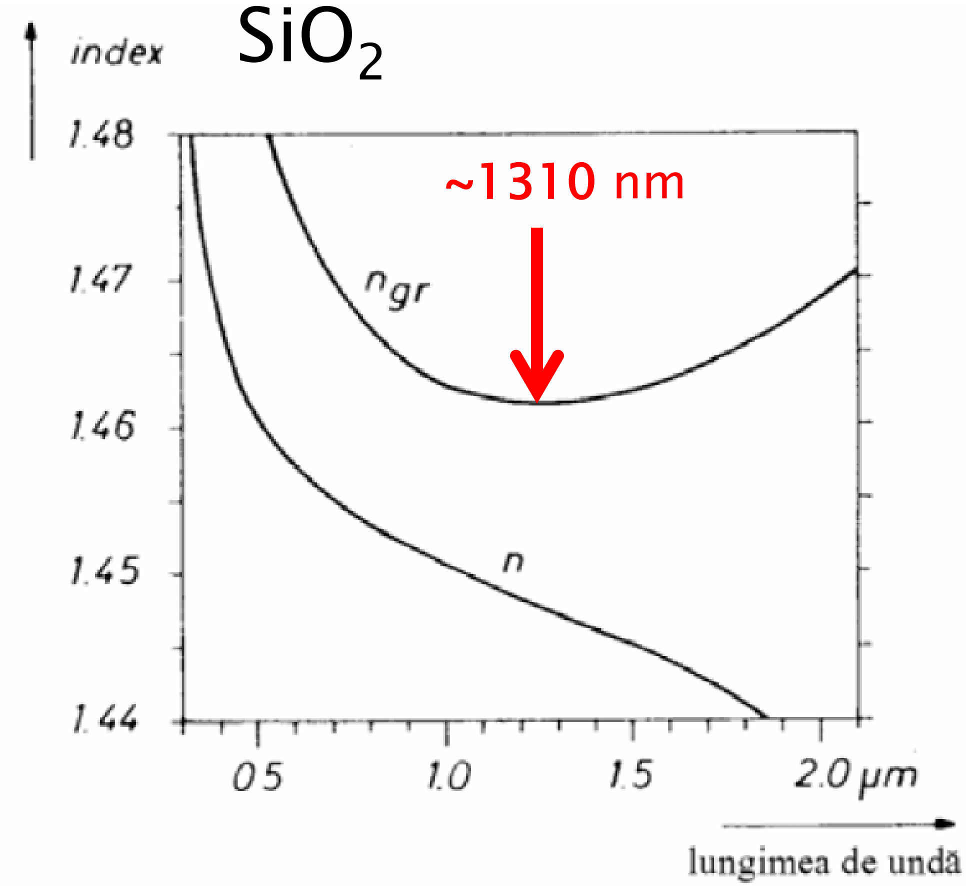
SI

"a source that emits monochromatic radiation of frequency $540 \cdot 10^{12}$ Hz"

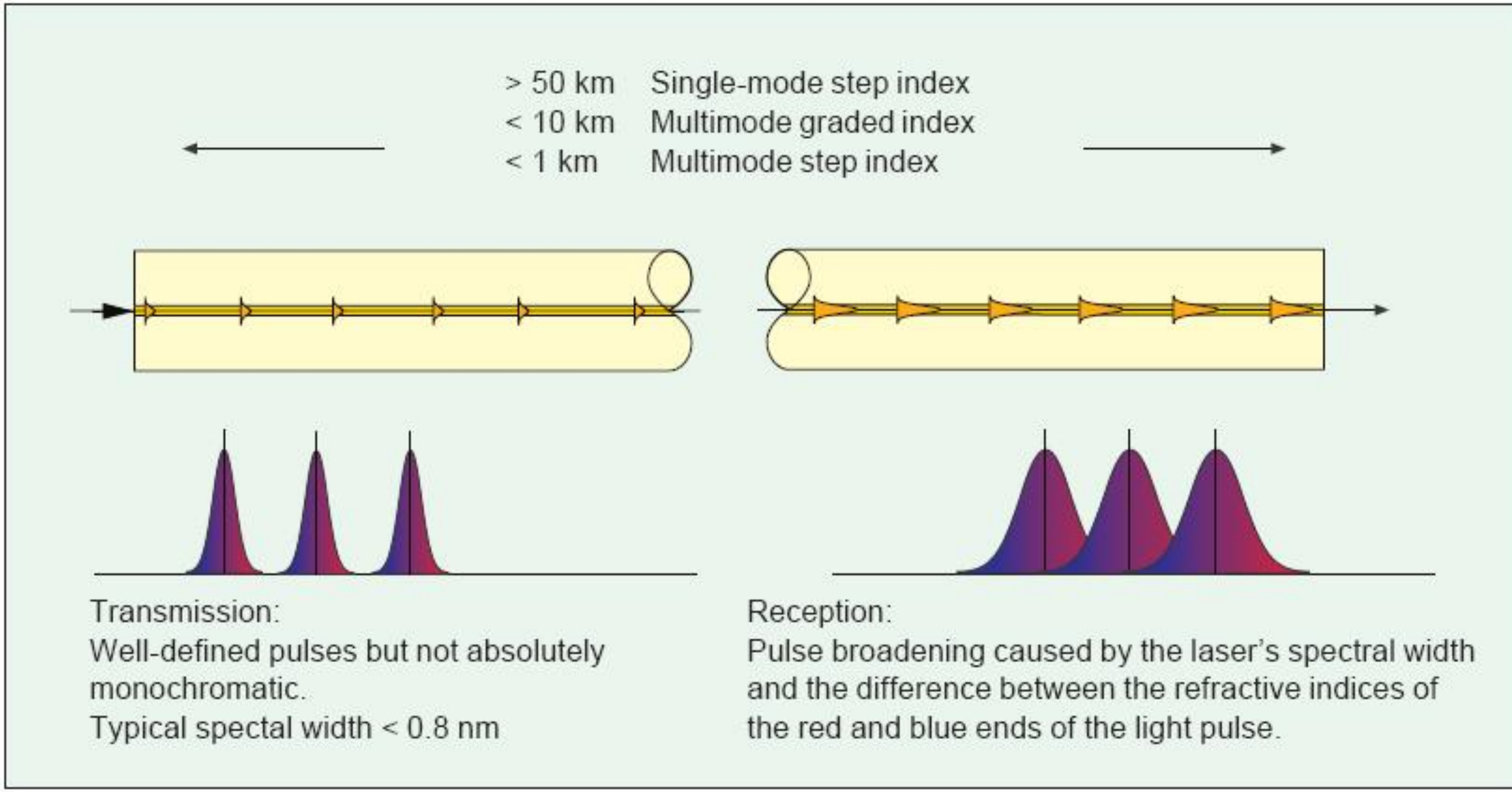
Dispersie normala

$$n_{gr} = n - \lambda \frac{dn}{d\lambda}$$

$$D = \frac{d\tau}{d\lambda} = \frac{1}{c} \cdot \frac{d n_{gr}}{d\lambda}$$



Dispersie


> 50 km Single-mode step index
< 10 km Multimode graded index
< 1 km Multimode step index
Transmission:
Well-defined pulses but not absolutely monochromatic.
Typical spectal width < 0.8 nm
Reception:
Pulse broadening caused by the laser's spectral width and the difference between the refractive indices of the red and blue ends of the light pulse.

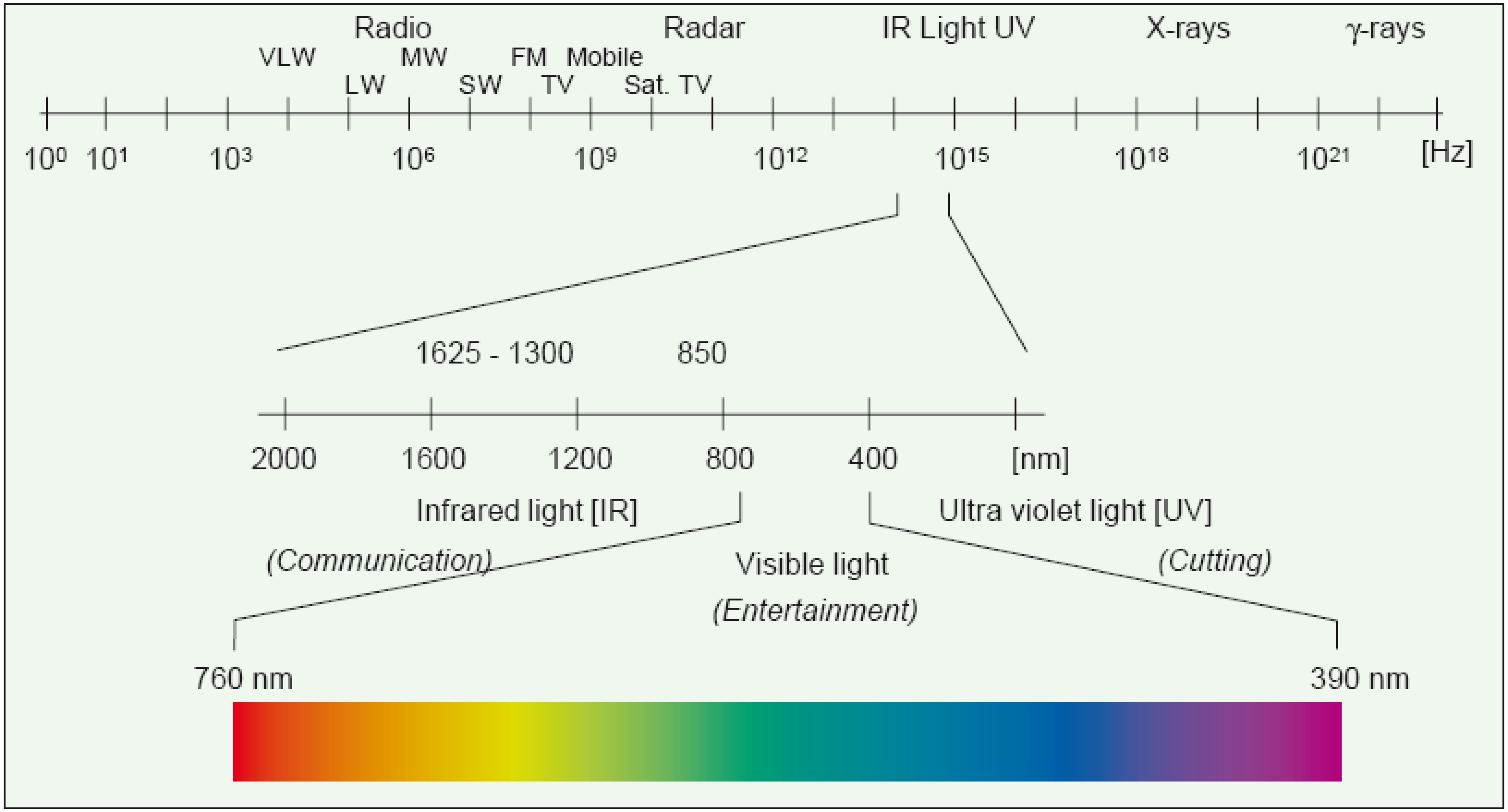
Fotometrie şi radiometrie

Capitolul 3

Aplicatii majore

- Comunicatii
  - Infrarosu (InGaAsP)
- Vizibil
  - Spectru vizibil (GaAlAs)
- Iluminare
  - Putere ridicata, lumina alba (GaInN)

Spectrul electromagnetic



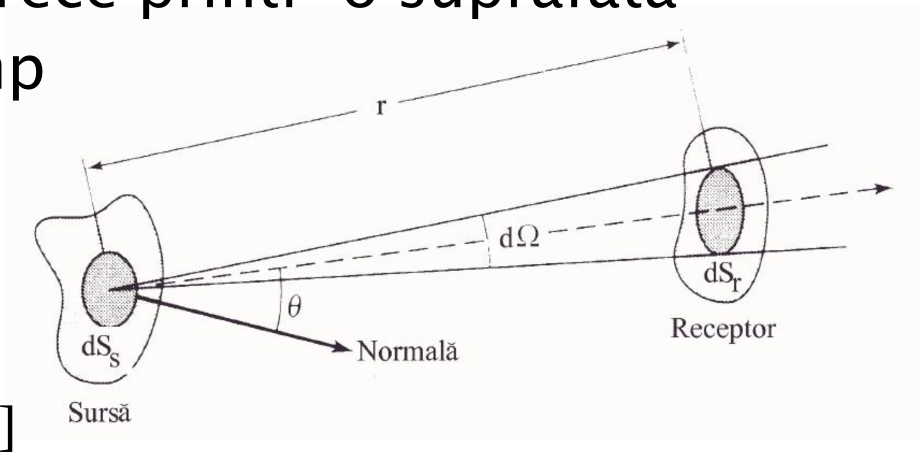
O alta dualitate

- In optoelectronica, lumina poate fi privita din doua puncte de vedere
  - energetic (efect asupra dispozitivului)
  - uman (efect asupra ochiului)
- Dualitatea mărimilor implicate
  - energetice
  - luminoase
- Candela (cd) **este** una din cele 7 mărimi fundamentale ale SI
  - Cd = intensitatea luminoasa a unei surse ce emite o radiație monocromatica cu frecventa $540 \cdot 10^{12}$ Hz (λ = 555nm in vid) si are o intensitate radianta de 1/683 W/sr

Flux energetic

- Flux energetic al luminii
  - viteza cu care energia trece printr-o suprafata
  - energie/unitatea de timp
  - unitatea SI – W

$$\Phi_e = \frac{dE}{dt} \quad [W]$$

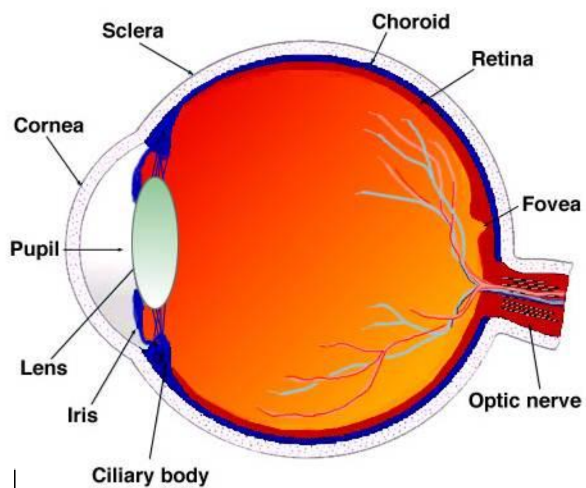


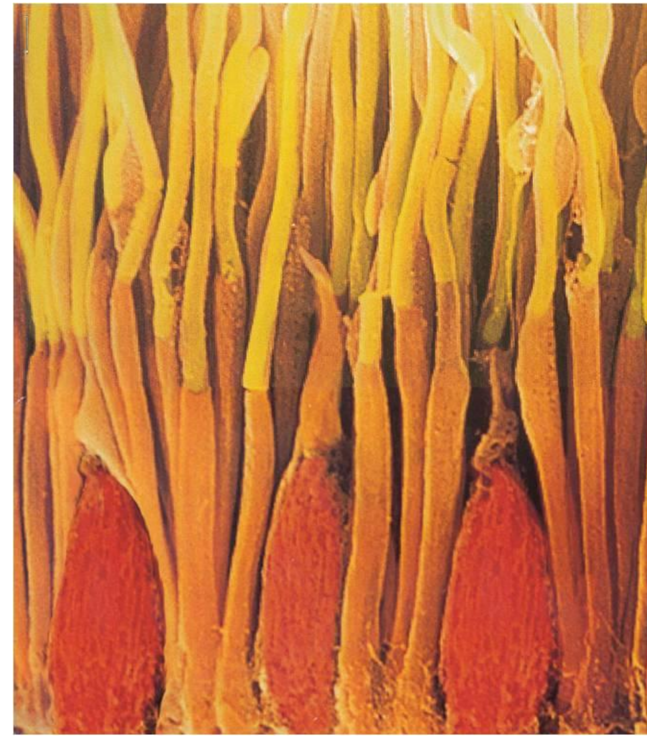
- Unghi solid
  - definitie $\Omega = \frac{A}{r^2} \quad [sr]$
  - valoarea maxima, sfera: Ω = 4π sr
  - pentru con cu deschiderea la varf 2ϕ: $\Omega = 2\pi \cdot (1 - \cos\varphi)$
  - pentru unghiuri mici: $\Omega = \pi \cdot \varphi^2$

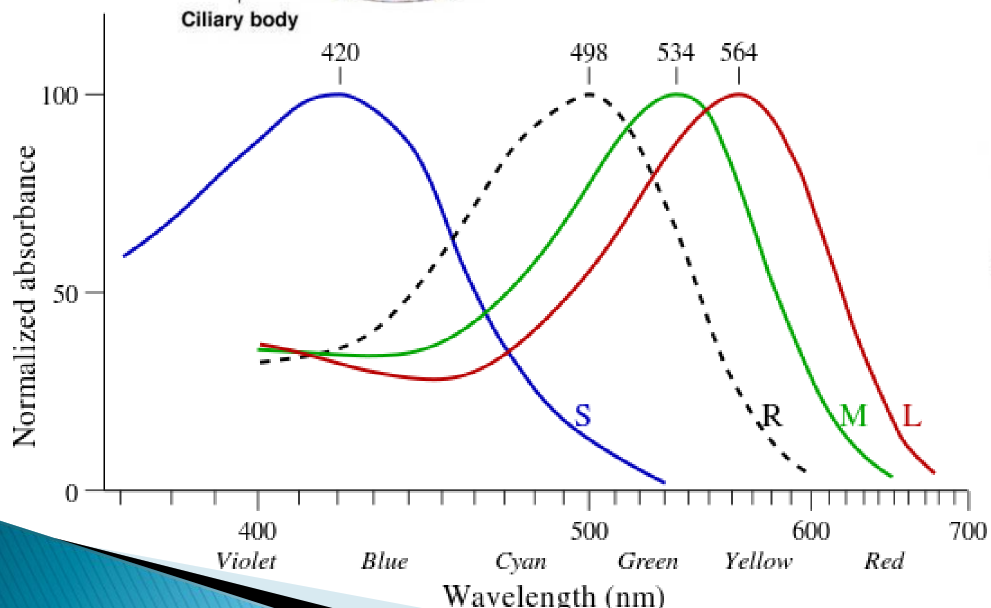
Flux luminos

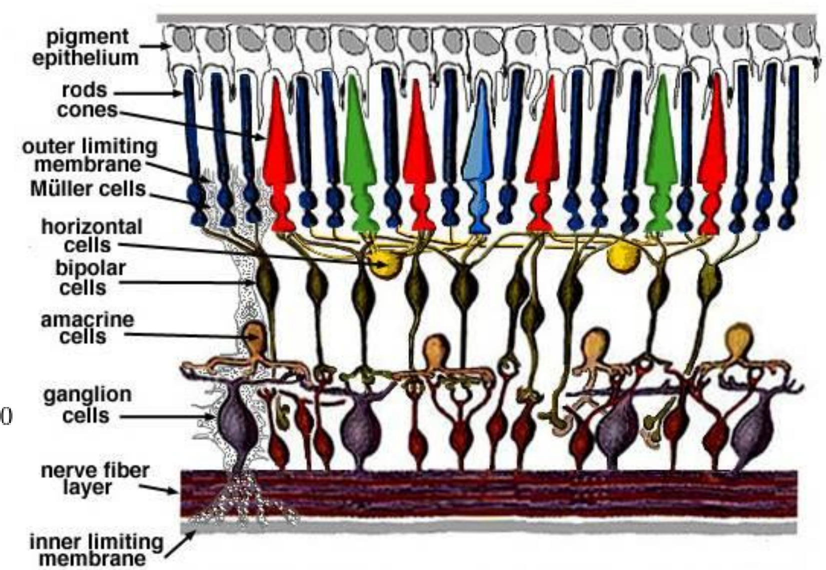
- Flux luminos, definitie
  - o masura a puterii luminoase percepute de om
- Unitate de masura – lm = lumen
  - In SI de unitati **lumenul** este definit ca fluxul luminos al unei surse luminoase punctiforme cu intensitatea luminoasa de o candela intr-un unghi solid egal cu 1 sr.
  - la λ = 555nm $\Phi_e = 1W \Leftrightarrow \Phi_v = 683\, lm$
- Dualitate pentru toate marimile implicate
  - radiometrie – indice “e”
  - fotometrie – indice “v”
- La alte lungimi de unda se tine cont de sensibilitatea relativa medie a ochiului uman

Ochiul uman

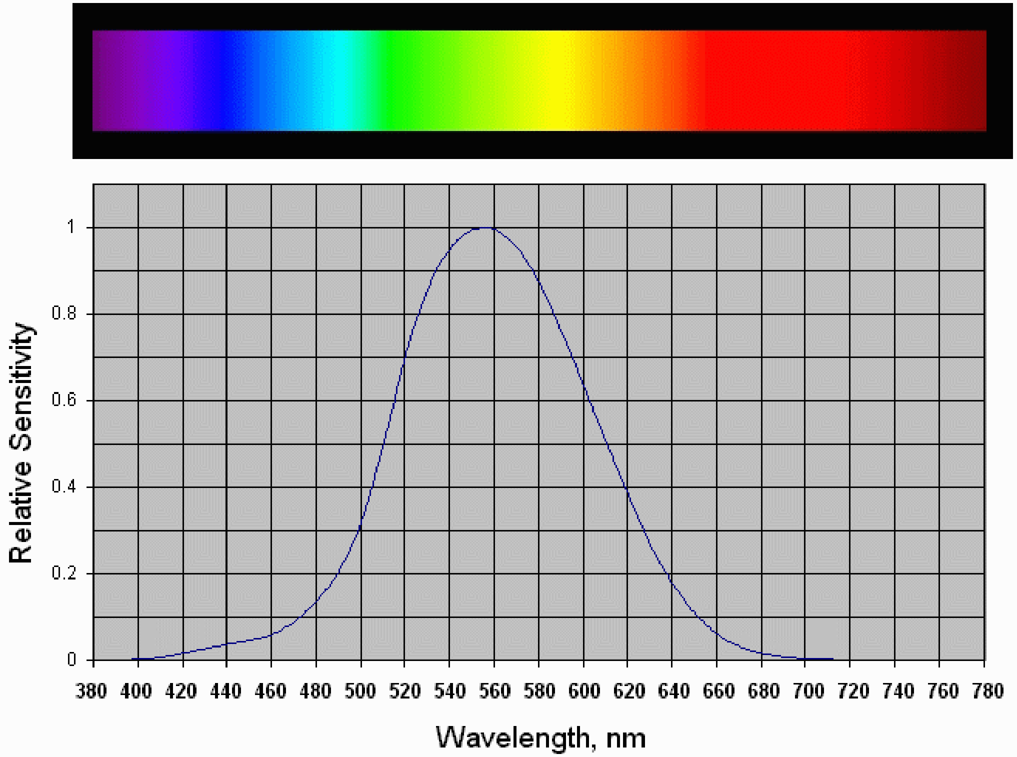

Sclera
Choroid
Retina
Cornea
Fovea
Pupil
Lens
Iris
Optic nerve
Ciliary body




420
498
534
564
100
50
0
Normalized absorbance
S
R
M
L
400
500
600
700
Violet
Blue
Cyan
Green
Yellow
Red
Wavelength (nm)


pigment epithelium
rods
cones
outer limiting membrane
Müller cells
horizontal cells
bipolar cells
amacrine cells
ganglion cells
nerve fiber layer
inner limiting membrane

CIE V(λ)



Response of Human Eye Versus Wavelength

(Data from the 1988 C.I.E. Photopic Luminous Efficiency Function)

Standarde

- Se incearca definirea omului “standard”
- CIE – Commission Internationale de l'Éclairage
  - 1931 – luminozitatea relativa standard V(λ) – **fotopic**
  - 1951 – luminozitatea relativa standard V(λ) – **scotopic**
  - 1978 – Vos
  - 2005 – Sharpe, Stockman, Jagla, Jägle
  - 2008 – CIE V(λ) – fotopic (~Sharpe)
- Sensibilitatea maxima a ochiului uman
  - vedere diurna (**fotopic**), $\lambda=555$ nm, $\eta_v = 683$ lm/W
  - vedere nocturna (**scotopic**), $\lambda=507$ nm , $\eta_v = 1700$ lm/W

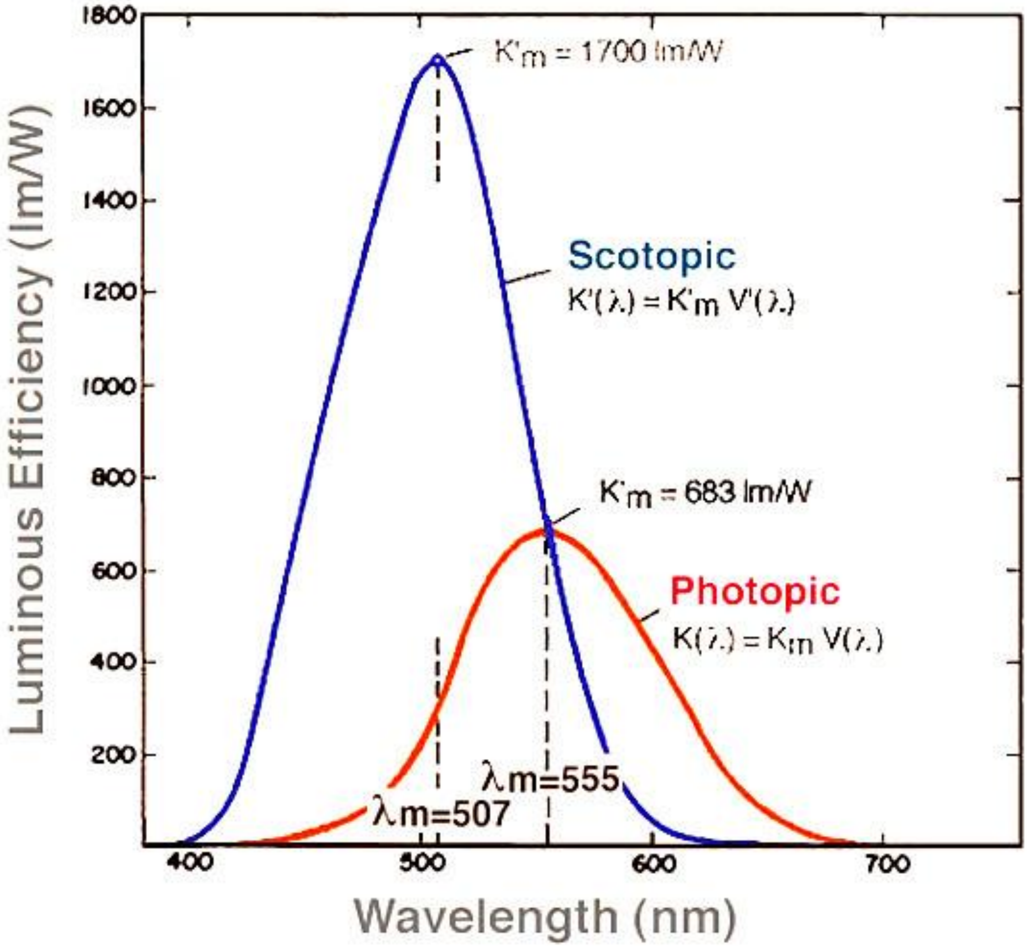


Figure 9. The scotopic and the photopic curves of spectral luminous efficacy (non-normalised values).

efect Purkinje

Curbe normalizate CIE

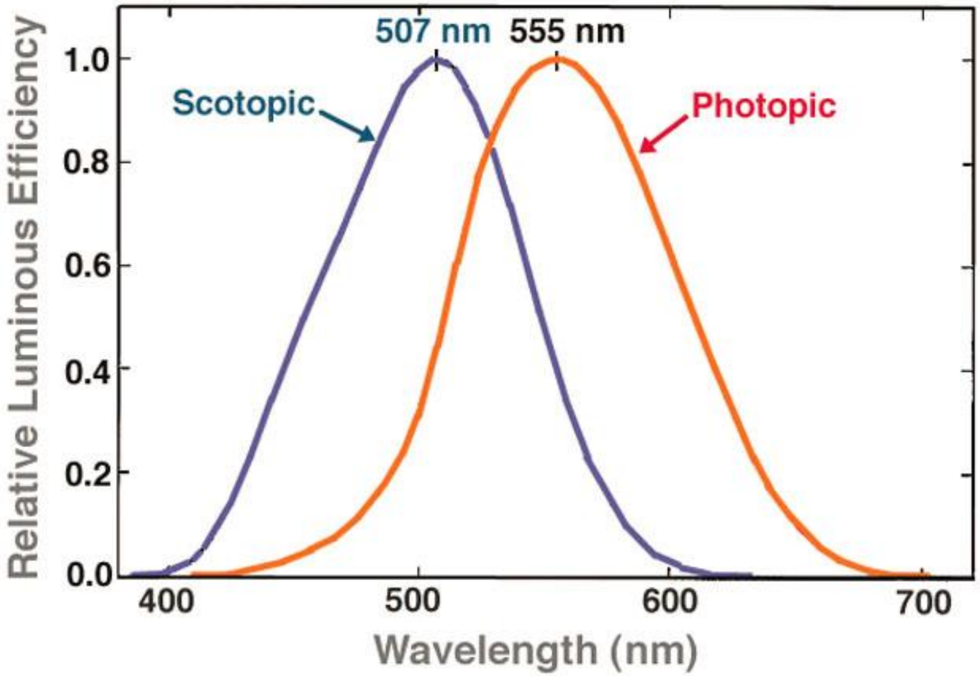
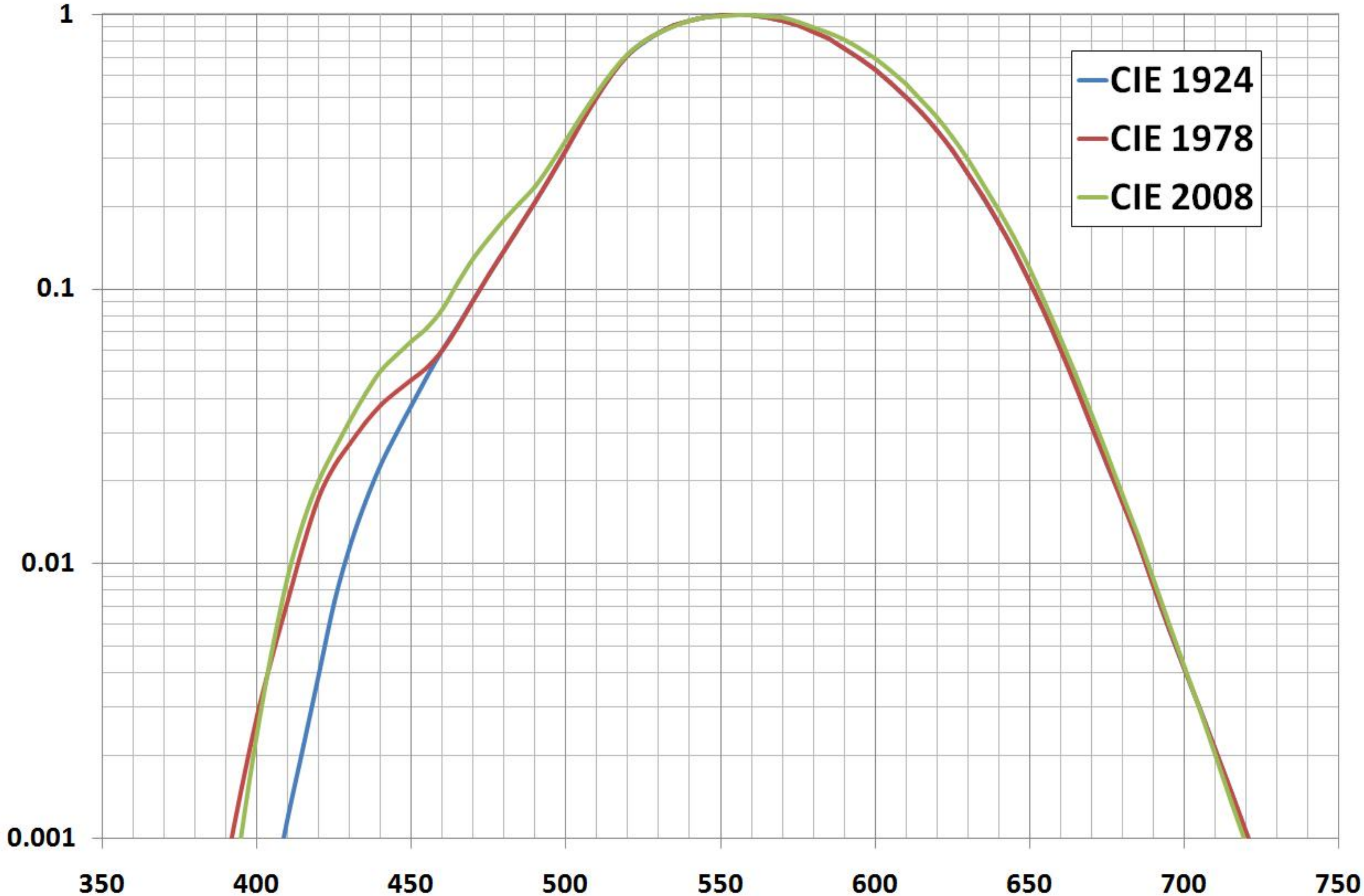
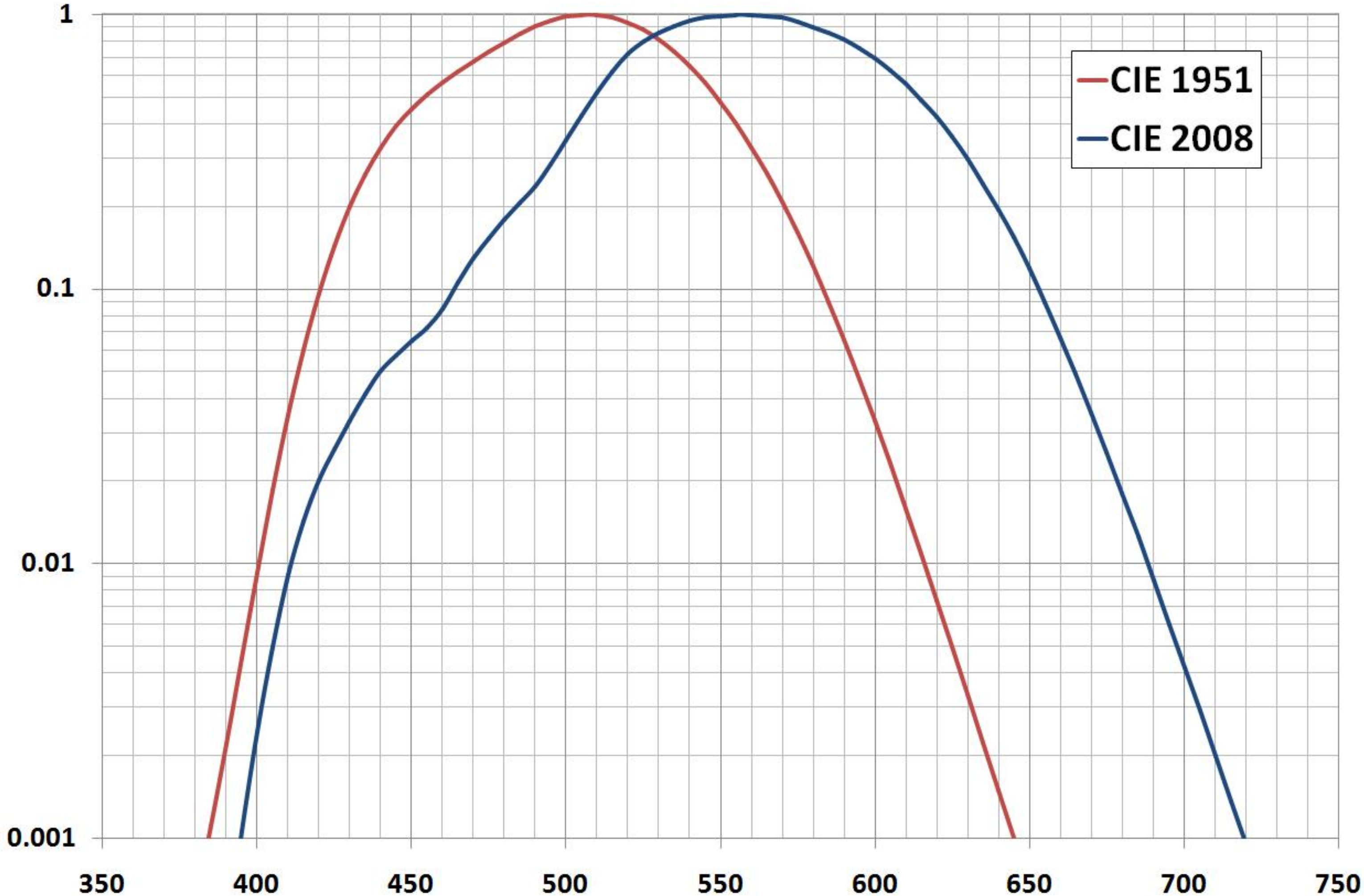


Figure 10. The scotopic and the photopic curves of relative spectral luminous efficiency as specified by the CIE (normalised values).

CIE V(λ) fotopic



CIE V(λ) fotopic / scotopic



Relatie radiometrie/fotometrie

- Pentru radiatii monocromatice

$$\Phi_v = 683\frac{lm}{W}\cdot\Phi_e[W]\cdot V(\lambda)\quad [lm] \qquad \Phi'_v = 1700\frac{lm}{W}\cdot\Phi_e[W]\cdot V'(\lambda)\quad [lm]$$

- Pentru radiatii complexe:

$$\Phi_v = 683\frac{lm}{W}\int_0^\infty \frac{d\Phi_e}{d\lambda}\cdot V(\lambda)\,d\lambda = 683\frac{lm}{W}\int_{390nm}^{830nm} \frac{d\Phi_e}{d\lambda}\cdot V(\lambda)\,d\lambda\quad [lm]$$

$$\Phi'_v = 1700\frac{lm}{W}\int_0^\infty \frac{d\Phi_e}{d\lambda}\cdot V'(\lambda)\,d\lambda = 1700\frac{lm}{W}\int_{390nm}^{830nm} \frac{d\Phi_e}{d\lambda}\cdot V'(\lambda)\,d\lambda\quad [lm]$$

- De cele mai multe ori, sursele sunt discrete, λ_i

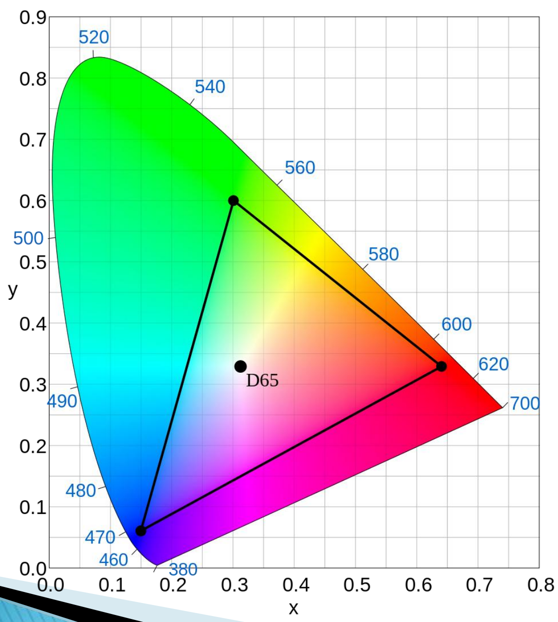
$$\Phi_v = 683\,\frac{lm}{W}\cdot\sum_i \Phi_e(\lambda_i)\cdot V(\lambda_i)\quad [lm]$$

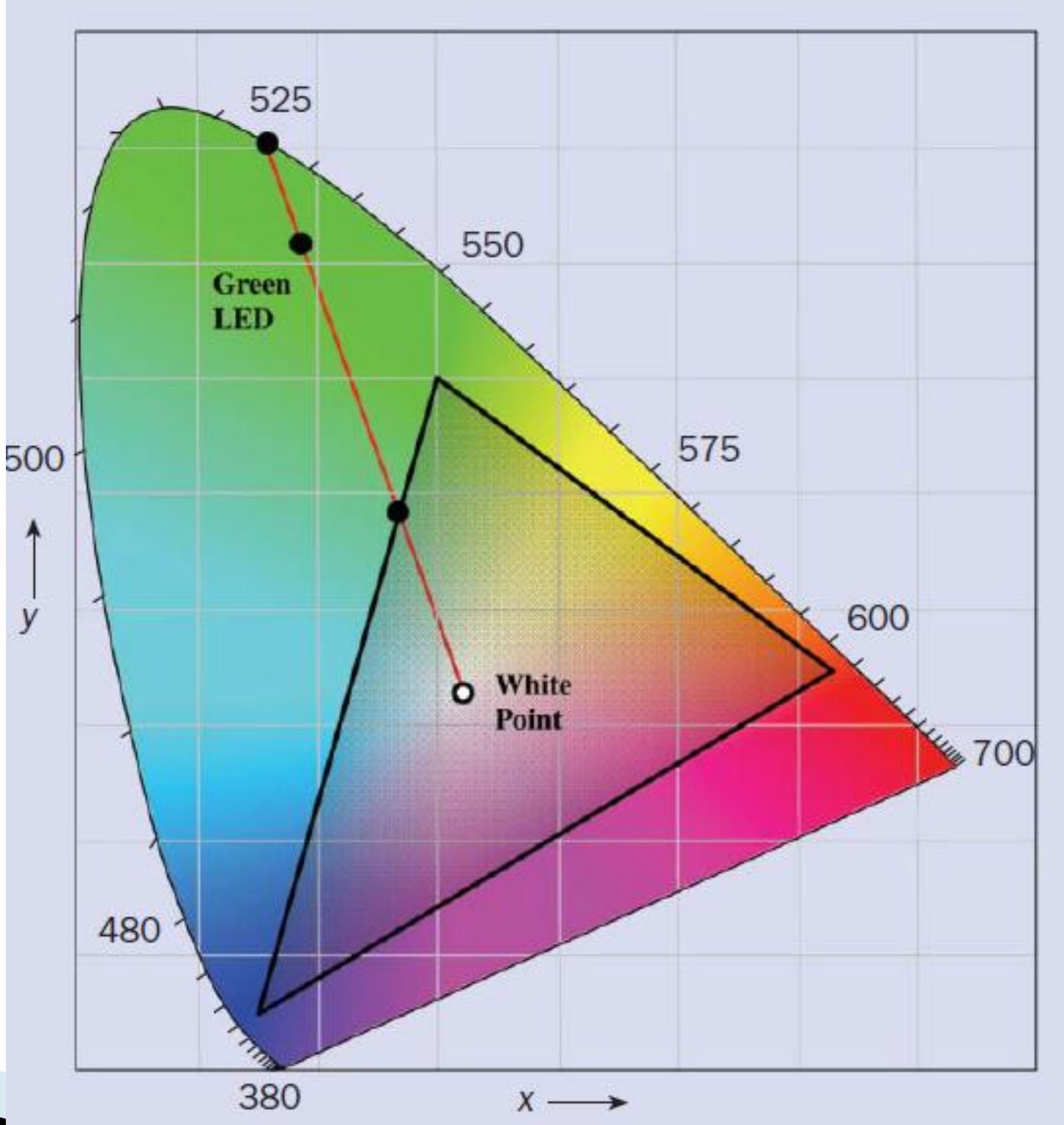
$$\Phi'_v = 1700\,\frac{lm}{W}\cdot\sum_i \Phi_e(\lambda_i)\cdot V'(\lambda_i)\quad [lm]$$

ITU-R BT.709

ITU-R BT.709 phosphor properties		
Phosphor	**x**	**y**
Red	0.640	0.330
Green	0.300	0.600
Blue	0.150	0.060

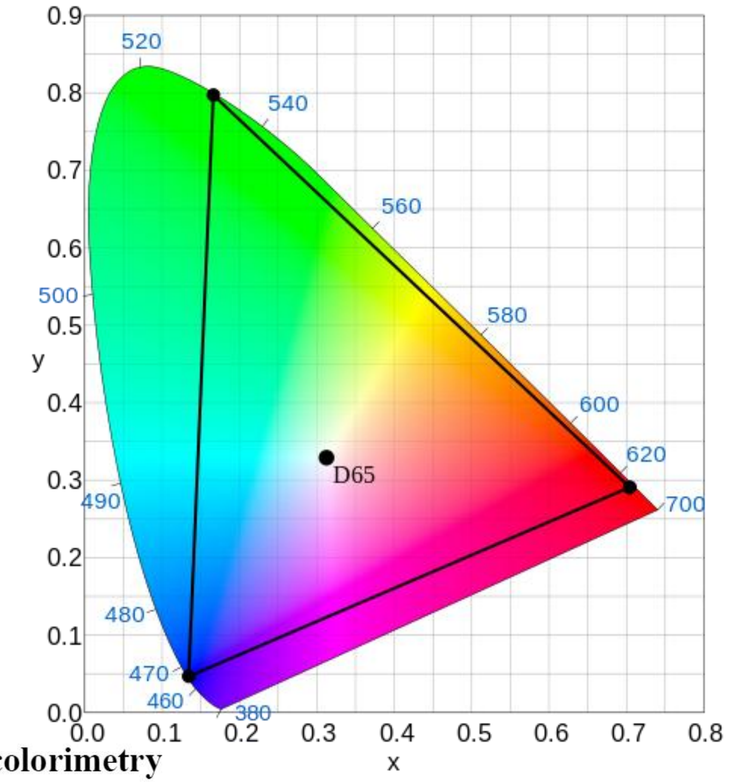
Data refers to xy chromaticity co-ordinates of ITU-R BT.709 phosphors which are used in most CRT displays [1].





ITU-R BT.2020

- **Parameter values for ultra-high definition television systems**
- UHDTV

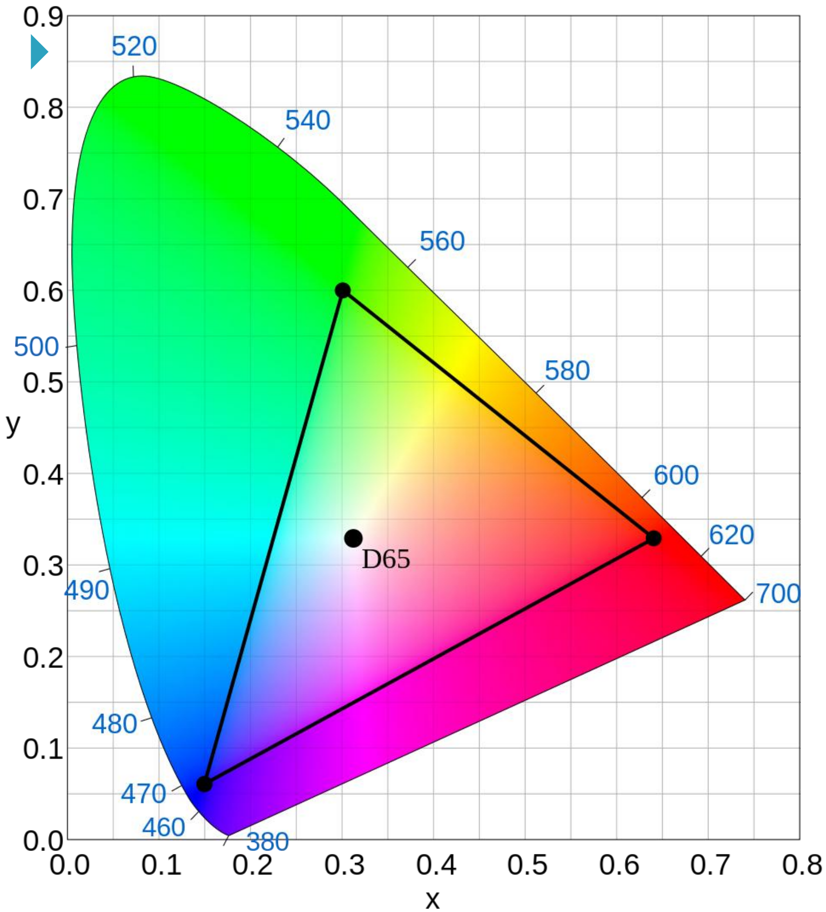


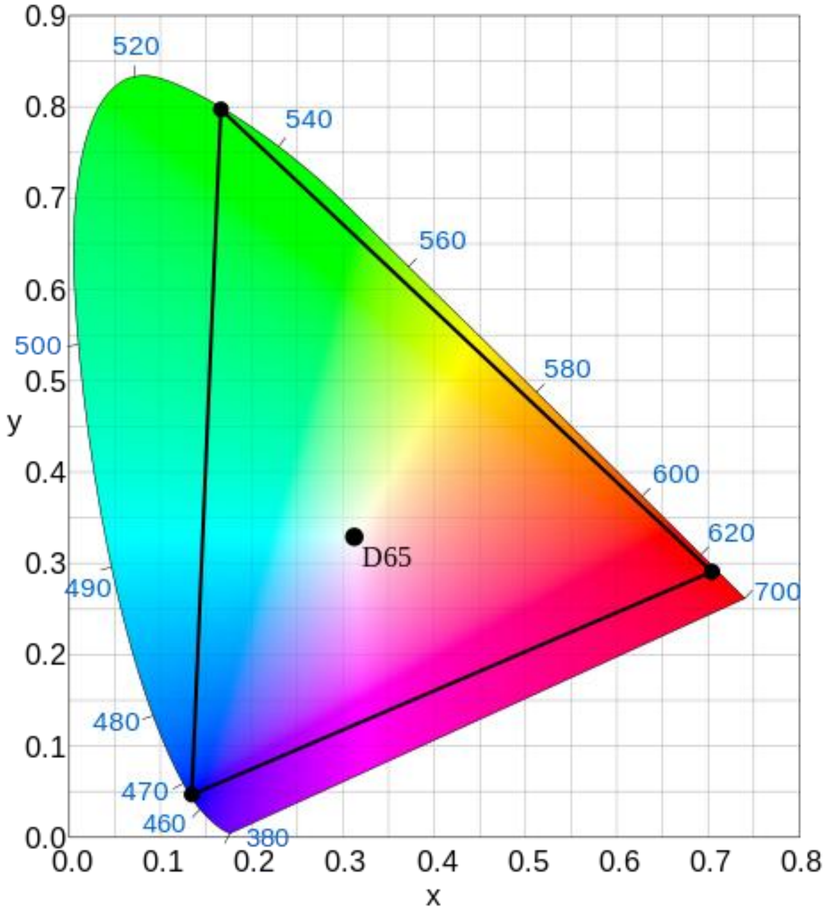
System colorimetry

Parameter	Values		
Opto-electronic transfer characteristics before non-linear pre-correction	Assumed linear(1)		
Primary colours and reference white(2)	Chromaticity coordinates (CIE, 1931)	x	y
	Red primary (R)	0.708	0.292
	Green primary (G)	0.170	0.797
	Blue primary (B)	0.131	0.046
	Reference white (D65)	0.3127	0.3290

(1) Picture information can be linearly indicated by the tristimulus values of RGB in the range of 0-1.

ITU-R BT.709/.2020





Marimi luminoase

- Intensitatea
  - raportul dintre fluxul care părăseşte sursa şi se propagă într-un element de unghi solid ce conţine direcţia de propagare şi elementul de unghi solid.
  - o masura a puterii emise de o sursa intr-un element de unghi solid

Intensitatea			
Fotometrie		Radiometrie	
$I_v = \frac{d\Phi_v}{d\Omega}$	SI: cd	$I_e = \frac{d\Phi_e}{d\Omega}$	SI: W/sr

Marimi luminoase

- Iluminarea
  - raportul dintre fluxul primit de un element de suprafaţă conţinînd punctul şi aria acestui element (definita într-un punct al unei suprafeţe la **receptie**):
  - o masura a intensitatii luminii incidente pe o suprafata

Iluminarea			
Fotometrie		Radiometrie	
$E_v = \frac{d\Phi_v}{dS}$	SI: lx	$E_e = \frac{d\Phi_e}{dS}$	SI: W/m^2

Marimi luminoase

- Excitanţa
  - raportul dintre fluxul care părăseşte un element de suprafaţă conţinînd punctul şi aria elementului de suprafaţă (definita într-un punct al unei suprafeţe la **emisie**):
  - o masura a intensitatii luminii emise de o suprafata

Excitanţa			
Fotometrie		Radiometrie	
$M_v = \frac{d\Phi_v}{dS}$	SI: lm/m²	$M_e = \frac{d\Phi_e}{dS}$	SI: W/m²

Marimi luminoase

- Luminanţa
  - raportul dintre fluxul care părăseşte, atinge sau traversează un element de suprafaţă şi care se propagă în direcţii conţinute într-un con elementar, dΩ, conţinînd direcţia dată, şi produsul dintre unghiul solid al conului şi aria proiecţiei ortogonale a elementului de suprafaţă pe un plan perpendicular pe direcţia dată, dS (definita într-o direcţie, într-un punct de pe suprafaţa unei surse sau unui receptor, sau într-un punct pe traiectul unui fascicol):
  - o masura a densitatii de intensitate luminoasa intr-o anumita directie

Luminanţa			
Fotometrie		Radiometrie	
$L_v = \dfrac{d^2\Phi_v}{d\Omega \cdot dS}$	SI: cd/m^2	$L_e = \dfrac{d^2\Phi_e}{d\Omega \cdot dS}$	SI: $W/m^2/sr$

Continuare

Fibra optică

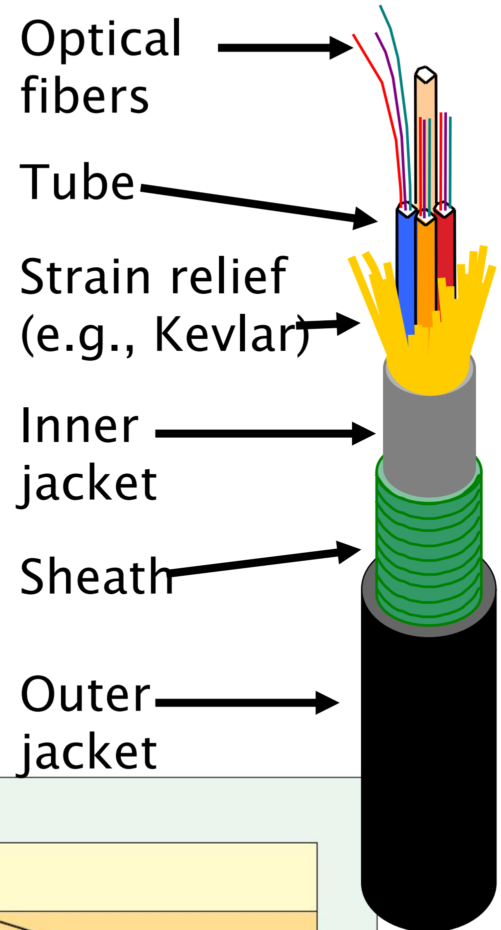
Capitolul 4

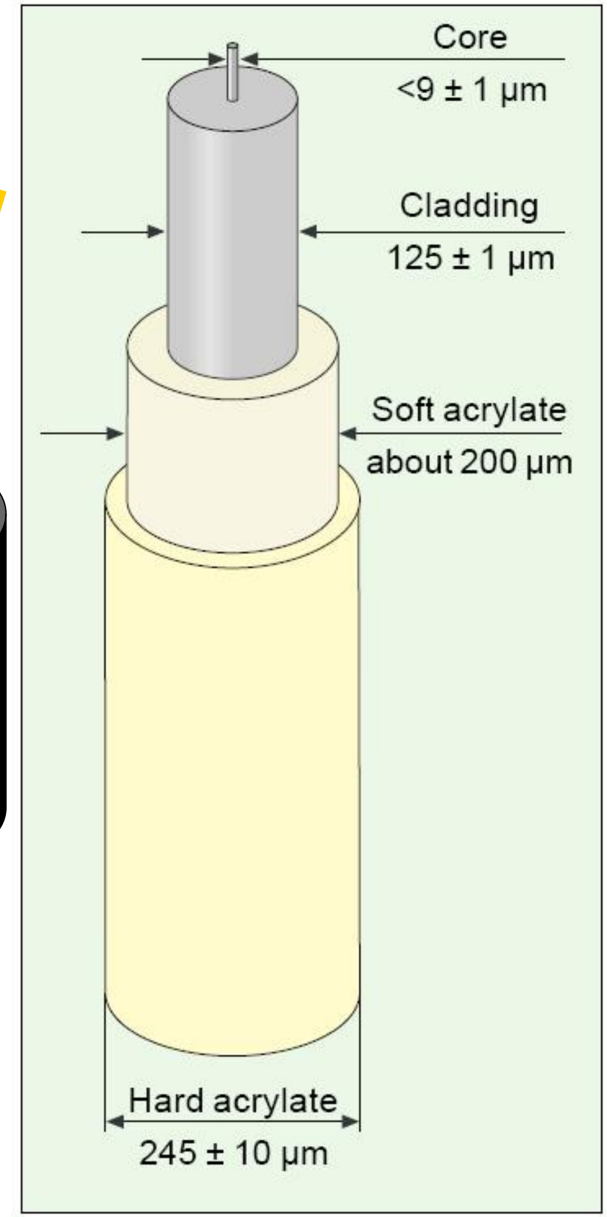
Cuprins

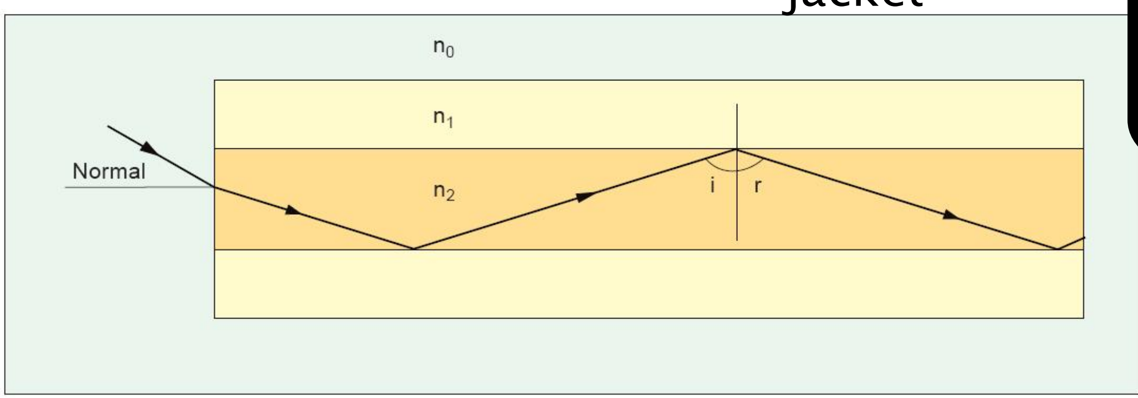
- **Lumina ca undă electromagnetică** (ecuaţiile lui Maxwell, ecuaţia undelor, parametrii de propagare)
- **Elemente de fotometrie şi radiometrie** (mărimi energetice/luminoase)
- **Fibra optică** (realizare, principiu de funcţionare, atenuare, dispersie, banda de frecvenţă)
- **Cabluri optice** (tehnologie, conectori, lipire - splice)
- **Proiectare sistemică a legăturii pe fibra optică** (bandă de frecvenţă, balanţa puterilor)
- **Emiţătoare optice** (LED şi dioda laser - realizare fizică şi functionare)
- **Receptoare optice** (dioda PIN, dioda cu avalanşă - realizare fizică şi functionare)
- **Amplificatoare transimpedanţă** (parametri, scheme tipice, TIA în buclă deschisă, cu reacţie, diferenţiale, control automat al câştigului)
- **Realizarea circuitelor pentru controlul emiţătoarelor optice (**parametri, scheme tipice, controlul puterii, multiplexoare**)**
- **Dispozitive de captare a energiei solare** (principiu de functionare, utilizare, proiectare)

Fibra optica

- un ghid de unda dielectric
  - miez
  - teaca



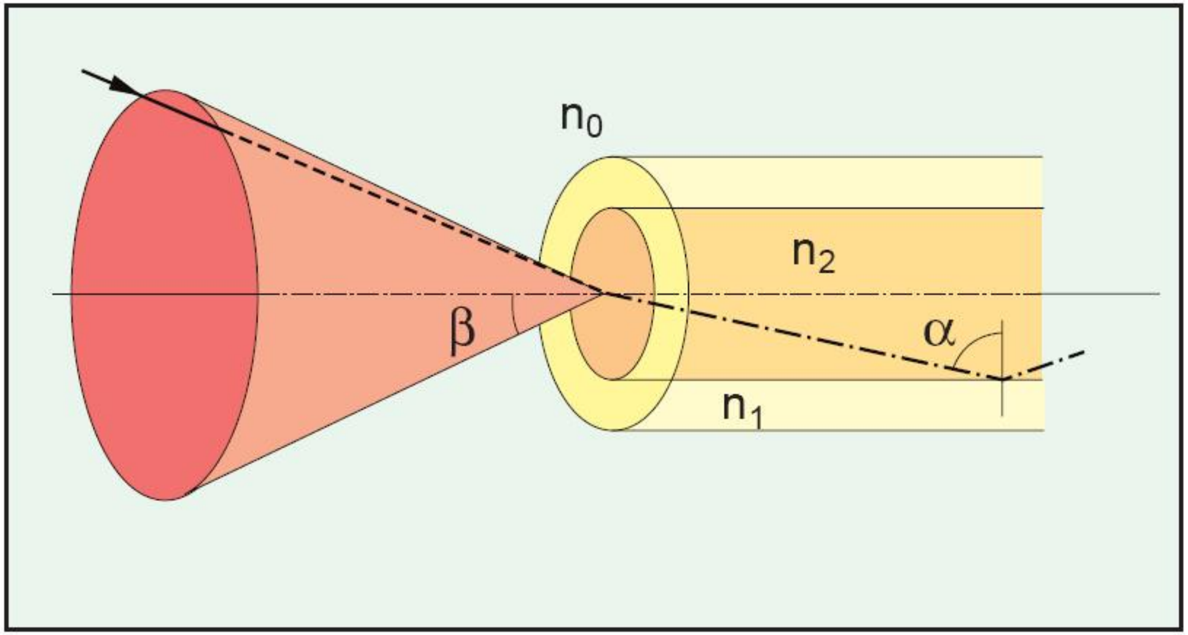




Unghi de acceptanta, apertura numerica

- Unghi de acceptanta

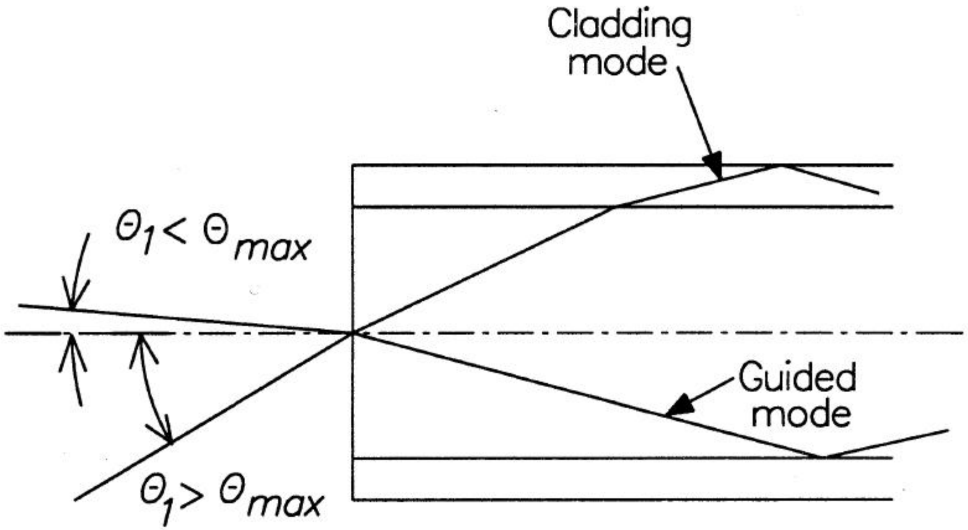
$$n_0 \cdot \sin\theta_{ACC} = n_2 \cdot \sin\phi_c$$



- **Apertura numerica**

$$NA = n_0 \cdot \sin\theta_{ACC}$$

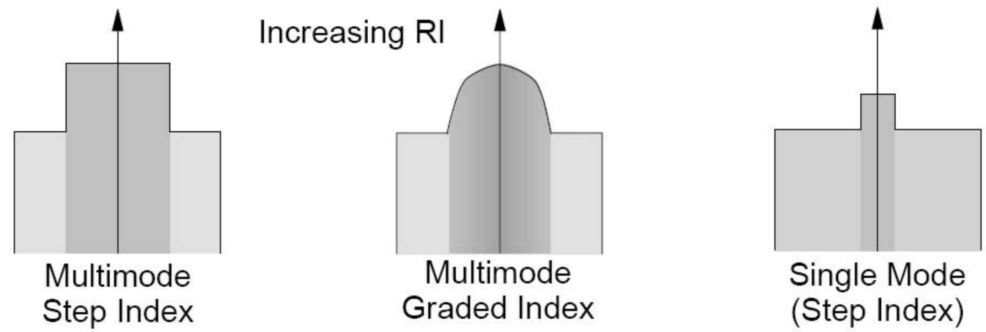
$$NA = n_2\sqrt{\frac{n_2^2 - n_1^2}{n_2^2}} = \sqrt{n_2^2 - n_1^2}$$

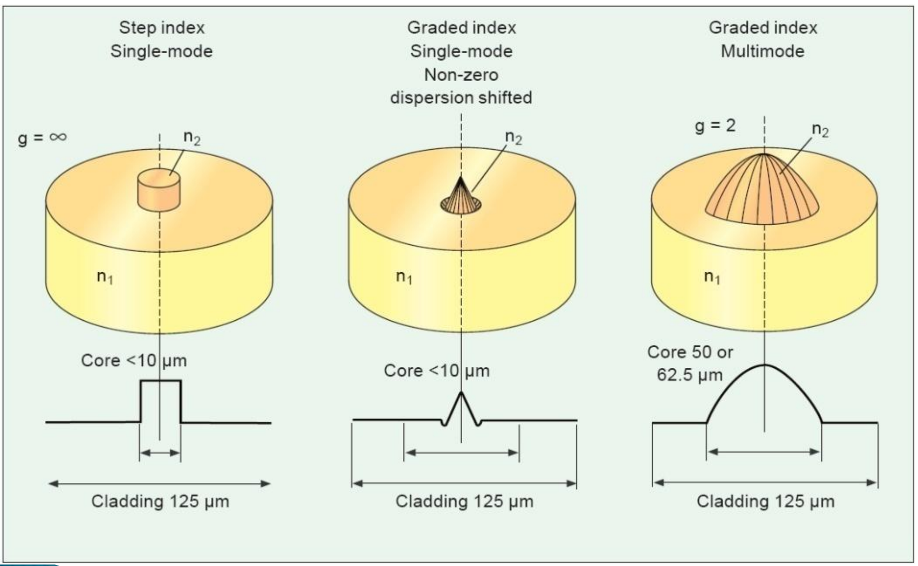


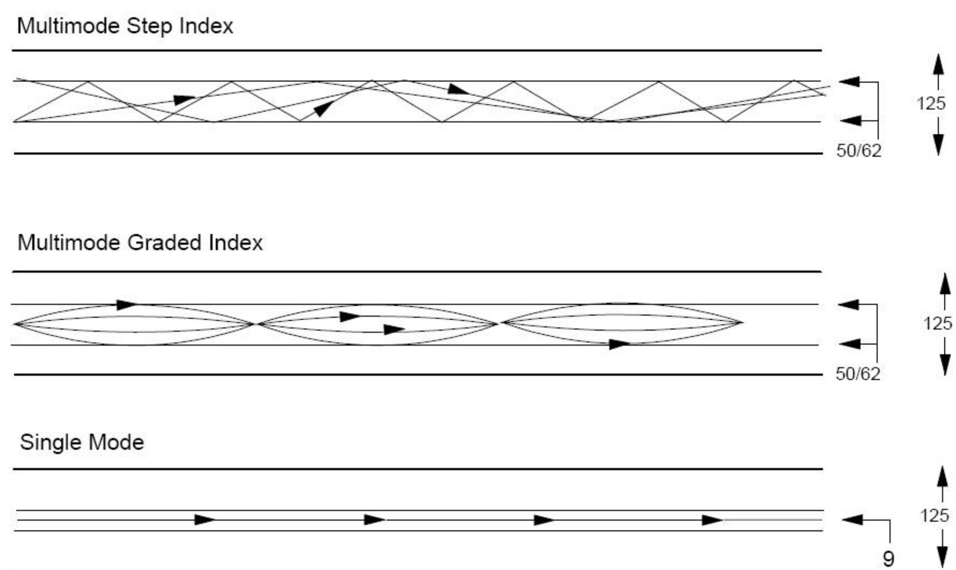
n_2 – miez
n_1 – teaca
$n_2 > n_1$!!

Tipuri de fibra

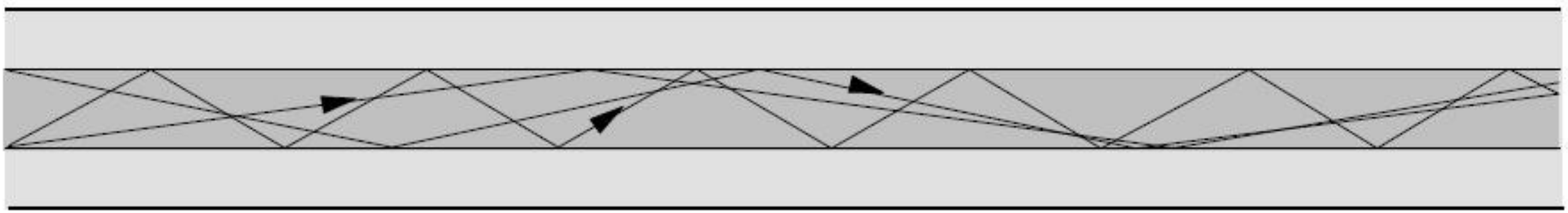
- Monomod
- Multimod
  - cu salt de indice
  - cu indice gradat



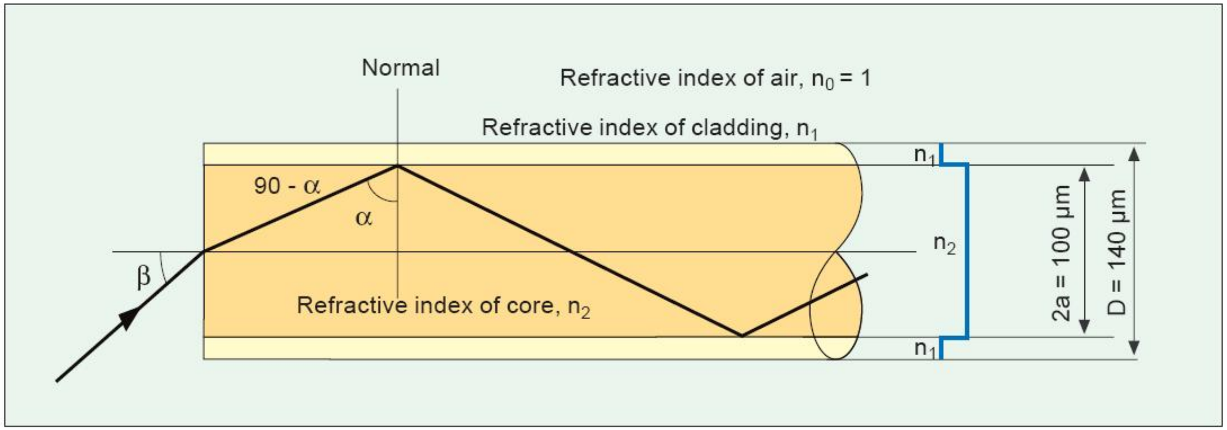


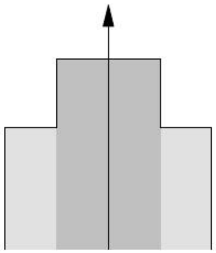


Fibre multimod cu salt de indice



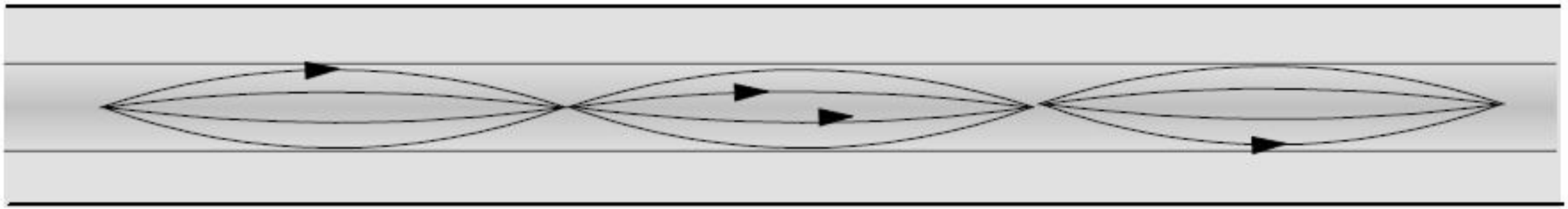
- 50/125 sau 62.5/125 (µm)
- 15-50 MHz · km



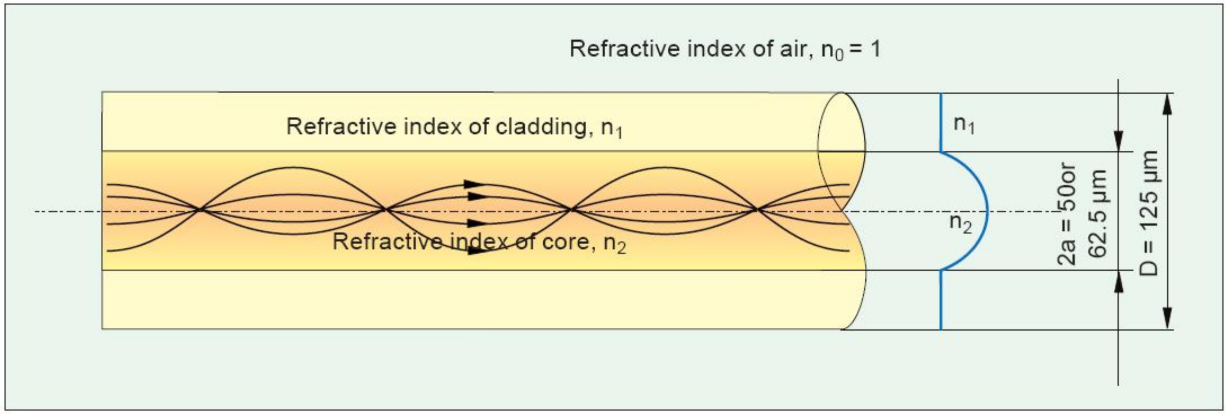


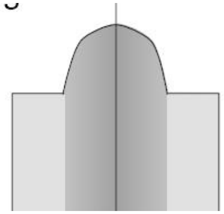
	glass	plastic
core diameter 2a	100 µm	980 µm
cladding diameter D	140 µm	1000 µm
core refractive index n_2	1.48	
cladding refractive index n_1	1.45	

Fibre multimod cu indice gradat



- 50/125 sau 62.5/125 (µm)
- 700-1200 MHz·km

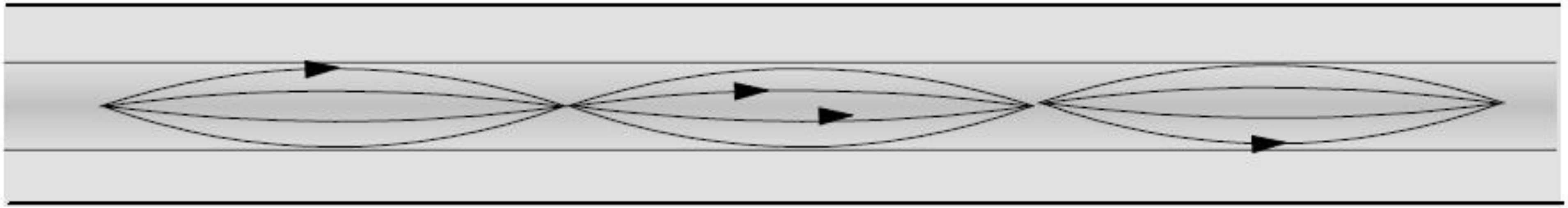




Core diameter 2a	50 or 62.5 µm
Cladding diameter D	125 µm
Maximum refractive index, core	1.46
Relative differential refractive index	0.010

Fata Morgana

Fibre multimod cu indice gradat

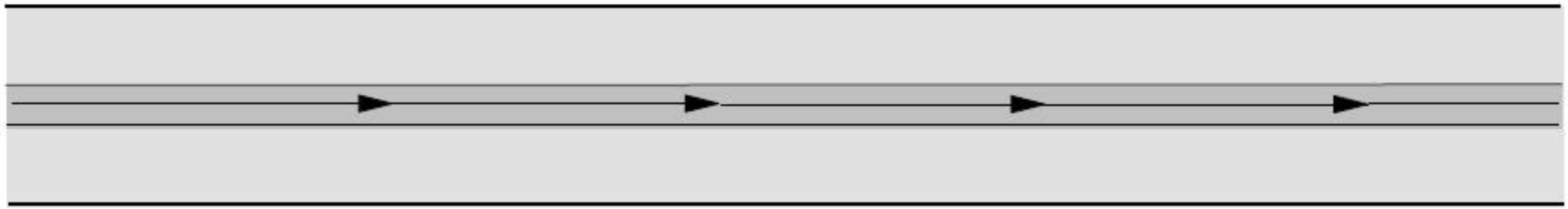


$$n(r) = n_2\left[1 - \Delta\left(\frac{r}{a}\right)^g\right]$$

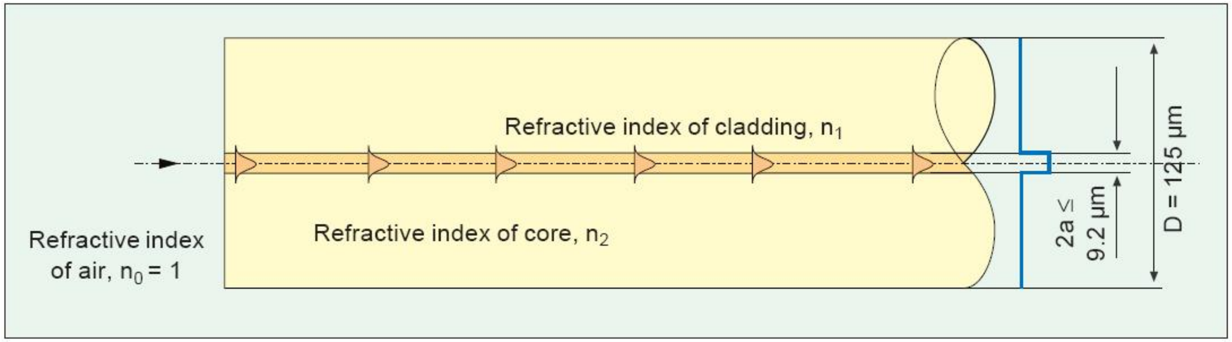
$$\Delta = \frac{NA^2}{2n_2^2} = \frac{n_2^2 - n_1^2}{2n_2^2} \approx \frac{n_2 - n_1}{n_2} \approx \frac{\Delta n}{n} \quad \text{for } \Delta << 1$$

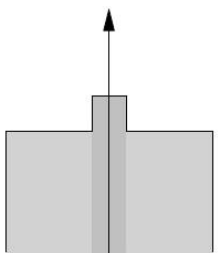
- g = 1 – indice gradat triunghiular
- g = 2 – indice gradat parabolic
- g = ∞ – salt de indice

Fibre monomod



- 6-8/125 (μm)
- MHz·km nerelevant
- MFD – Mode Field Diameter





Cladding diameter D	125 μm
Core refractive index n_2	1.4485
Cladding refractive index n_1	1.4440
Refractive index differential	0.003 = 0.3%

Ghid cilindric dielectric

- Ecuatiile lui Maxwell in coordonate cilindrice

$$\frac{\partial^2 U}{\partial r^2} + \frac{1}{r}\frac{\partial U}{\partial r} + \frac{1}{r^2}\frac{\partial^2 U}{\partial \phi^2} + \frac{\partial^2 U}{\partial z^2} + n^2 k_o^2 U = 0$$

a – raza miezului
U – E(r) sau H(r)

$$U(r, \phi, z) = u(r) e^{-jl\phi} e^{-j\beta z}, \qquad l = 0, \pm 1, \pm 2, \dots$$

$$\frac{d^2 u}{dr^2} + \frac{1}{r}\frac{du}{dr} + \left(n^2(r) k_o^2 - \beta^2 - \frac{l^2}{r^2} \right) u = 0$$

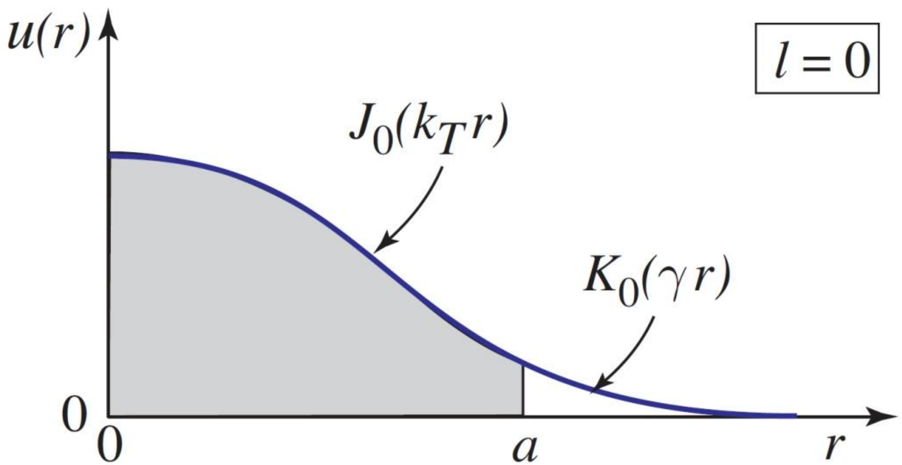
$$\frac{d^2 u}{dr^2} + \frac{1}{r}\frac{du}{dr} + \left(k_T^2 - \frac{l^2}{r^2} \right) u = 0, \qquad r < a$$

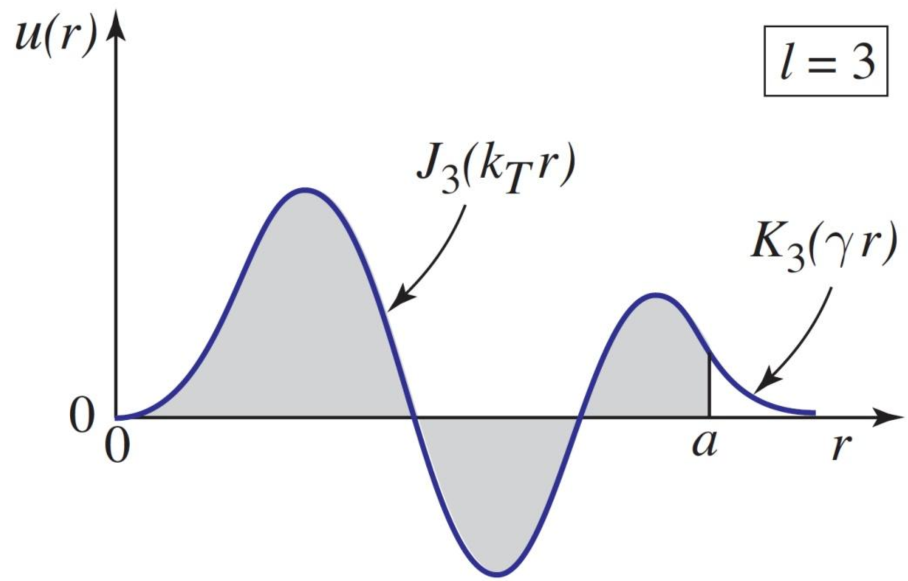
$$\frac{d^2 u}{dr^2} + \frac{1}{r}\frac{du}{dr} - \left(\gamma^2 + \frac{l^2}{r^2} \right) u = 0, \qquad r > a$$

Ghid cilindric dielectric

- solutii proportionale cu functii Bessel

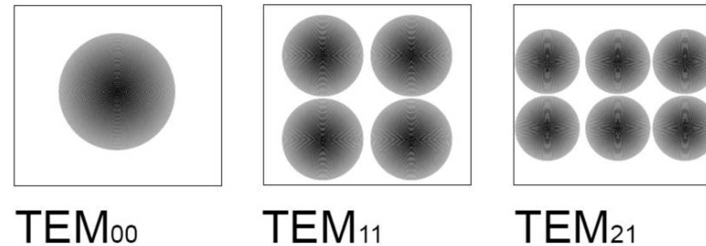
$$u(r) \propto \begin{cases} J_l(k_T r), & r < a \quad \text{(core)} \\ K_l(\gamma r), & r > a \quad \text{(cladding)} \end{cases}$$



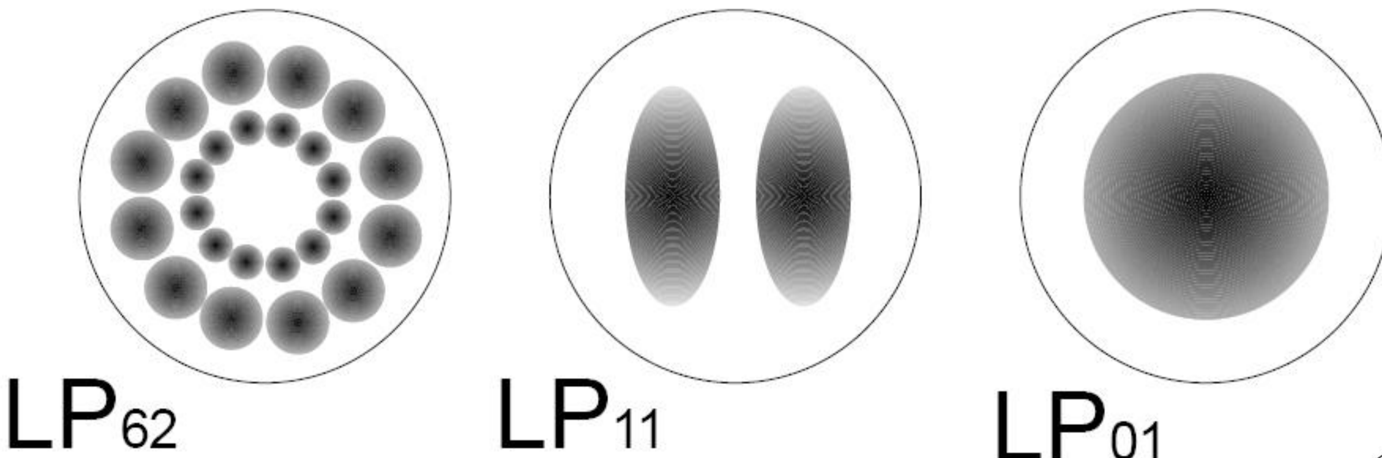


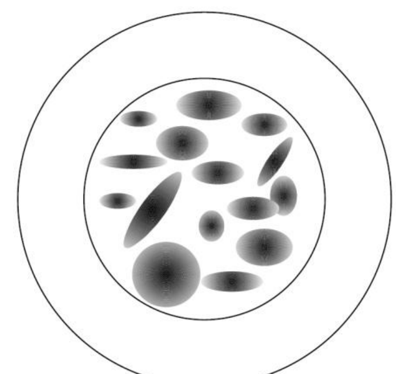
Moduri in fibra

- Moduri in ghid rectangular



- Moduri linear polarizate in fibra





“Sparkle” pattern

Frecventa normalizata

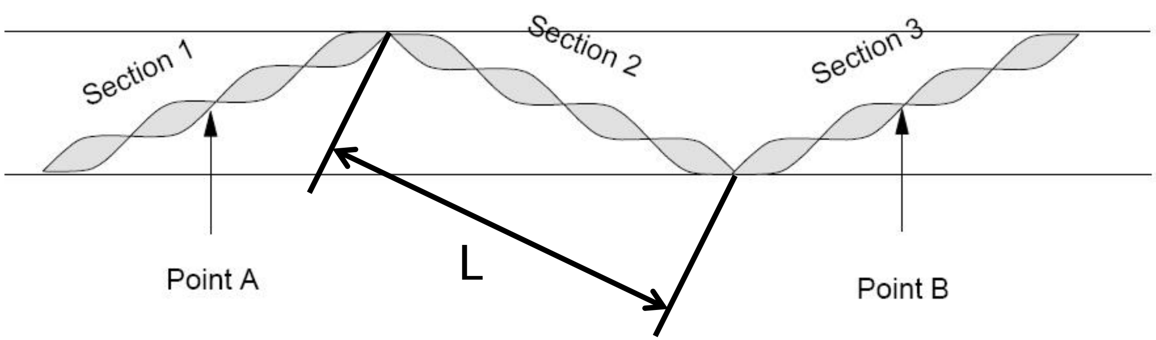
- Frecventa normalizata

$$V = 2\pi \frac{a}{\lambda} NA = k \cdot a \cdot NA$$

a – raza miezului

$$k = \frac{2\pi}{\lambda}$$

- Numar de moduri

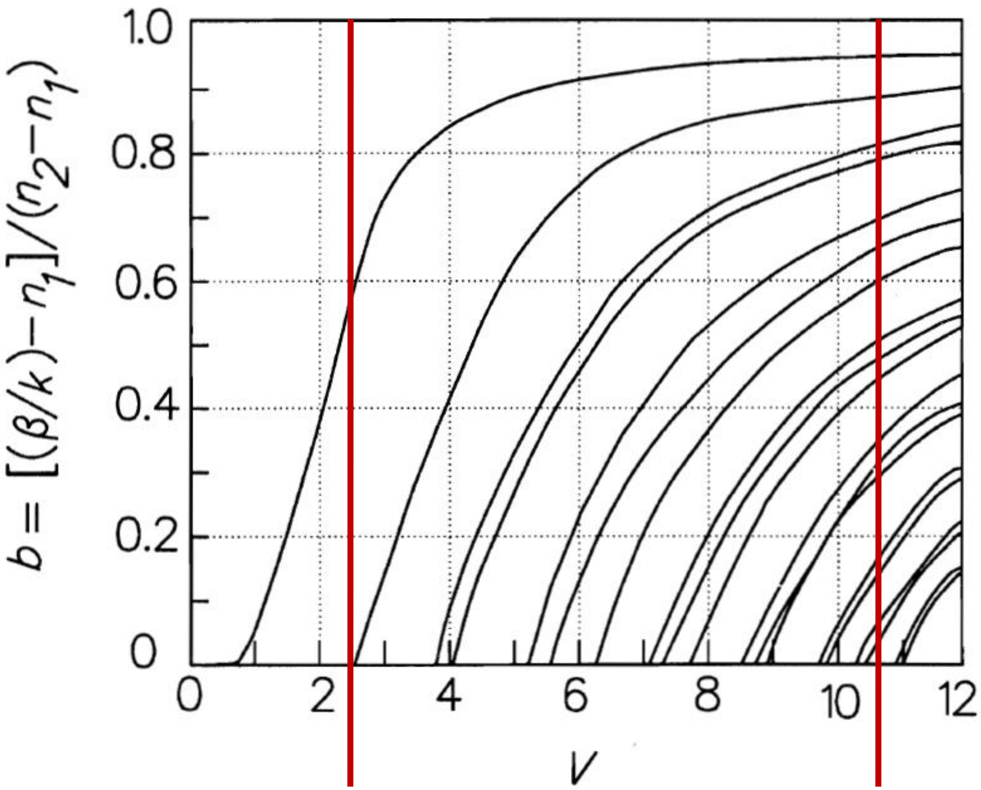


$$L = m \cdot \lambda$$

$$N \approx \frac{V^2}{2} \cdot \frac{g}{g+2}$$

Frecventa normalizata – monomod

- Fibre monomod



b – coeficient de propagare modal relativ

$$V \le V_C = 2.405$$

exista un **singur** mod (solutii fc. Bessel)

$$\lambda \ge \lambda_C = \pi \frac{2a}{V_C} NA = \pi \frac{2a}{2.405} NA$$

Exemplu:

2a = 8.5μm

NA = 0.11

$$\lambda_C = \pi \frac{8.5}{2.405} 0.11 = 1210\text{nm}$$

Frecventa normalizata

- Numar de moduri
  - Multimod cu salt de indice

$$g = \infty \quad \Rightarrow \quad N \approx \frac{V^2}{2}$$

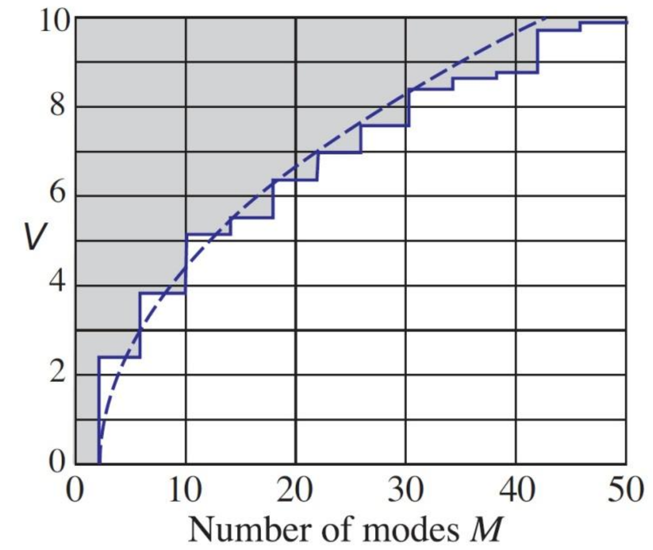
  - Multimod cu indice gradat

$$g = 2 \quad \Rightarrow \quad N \approx \frac{V^2}{4}$$

  - Monomod

$$V \le V_C = 2.405$$ exista un singur mod (solutii fc. Bessel)

$$N \approx \frac{V^2}{2} \cdot \frac{g}{g+2}$$



Exemplu

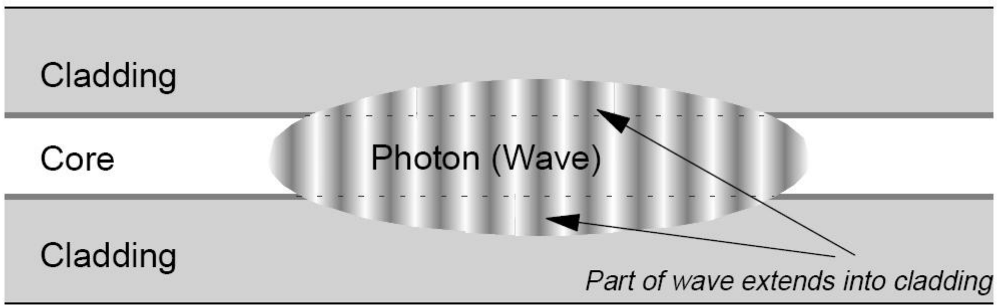
- fibra tipica multimod
  - g=2
  - 2a = 50μm -> a = 25μm
  - NA = 0.2 la λ = 1μm

$$V = 2\pi \frac{a}{\lambda} NA = 2\pi \frac{25}{1} 0.2 = 2 \cdot \pi \cdot 5 \approx 31.4$$

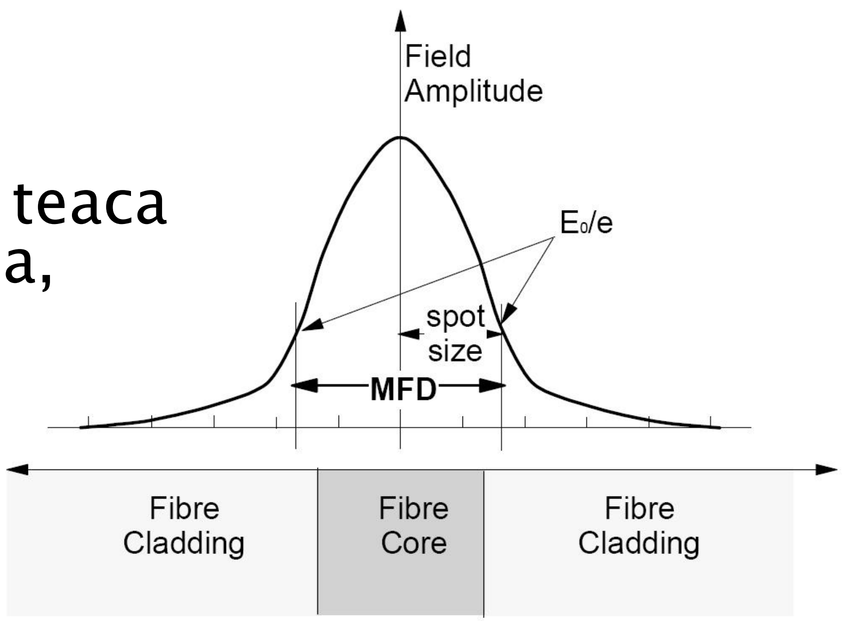
$$g = 2 \quad \Rightarrow \quad N = \frac{V^2}{4} = \frac{31.4^2}{4} = 247$$

Propagarea in fibra monomod

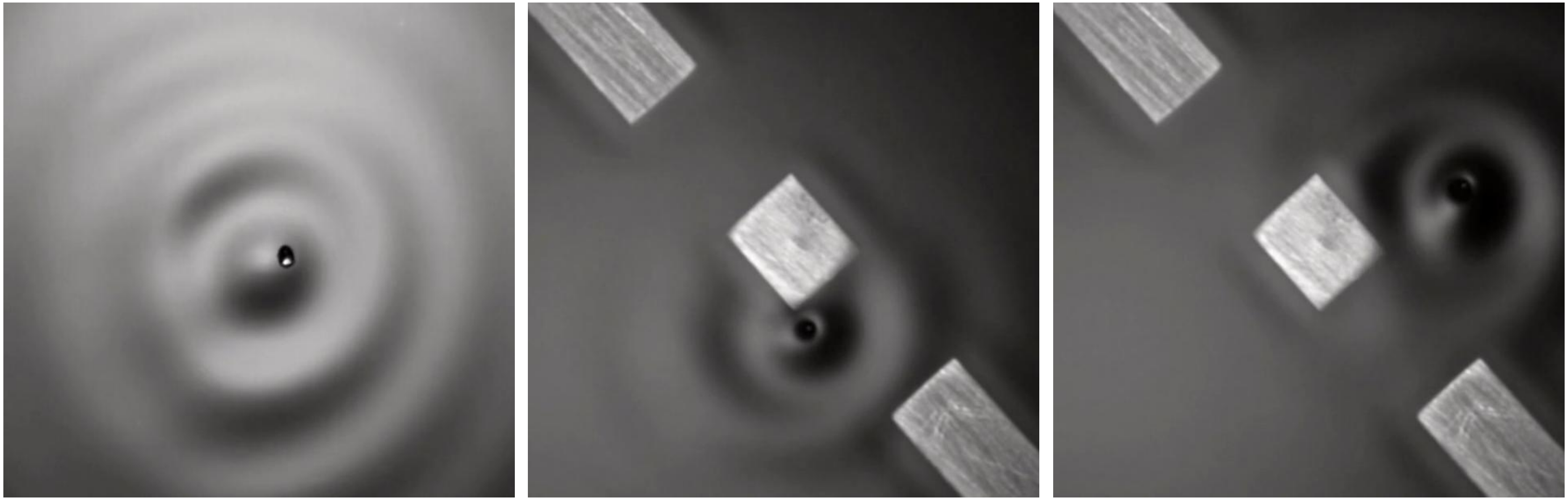
- Propagarea luminii poate fi explicata doar prin teoria electromagnetica



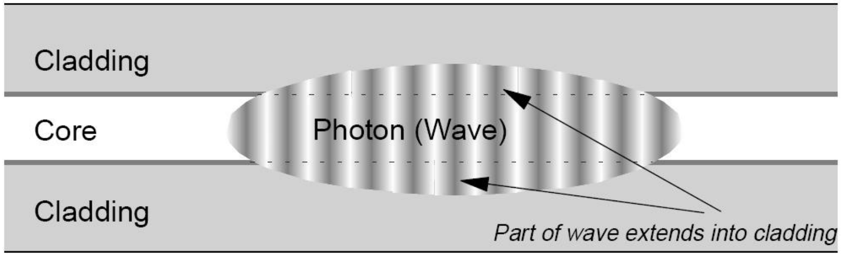
- Energia campului se extinde in teaca (diametrul efectiv al spotului luminos – MFD, Mode Field Diameter)
- MFD > 2a
- Adancimea de patrundere in teaca depinde de lungimea de unda, generand dispersia de ghid



Modelare



Through the Wormhole
S02E07 How Does the Universe Work



Fenomene de interes

- Cat de departe pot transmite semnalul luminos pe fibra
  - **atenuare**
- Cat de rapid pot transmite informația
  - dispersie

Reprezentare logaritmică

$$\text{Pierderi}[dB] = 10 \cdot \log_{10}\left(\frac{P_{out}}{P_{in}}\right)$$

$$P[dBm] = 10 \cdot \log_{10}\left(\frac{P}{P_0}\right) = 10 \cdot \log_{10}\left(\frac{P}{1mW}\right)$$

dB = 10 · $\log_{10}$ (P_2 / P_1)

0 dB	= 1
+ 0.1 dB	= 1.023 (+2.3%)
+ 3 dB	= 2
+ 5 dB	= 3
+ 10 dB	= 10
−3 dB	= 0.5
−10 dB	= 0.1
−20 dB	= 0.01
−30 dB	= 0.001

[dBm] + [dB] = [dBm]

dBm = 10 · $\log_{10}$ (P / 1 mW)

0 dBm	= 1 mW
3 dBm	= 2 mW
5 dBm	= 3 mW
10 dBm	= 10 mW
20 dBm	= 100 mW
−3 dBm	= 0.5 mW
−10 dBm	= 100 μW
−30 dBm	= 1 μW
−60 dBm	= 1 nW

[dBm/Hz] + [dB] = [dBm/Hz]

[x] + [dB] = [x]

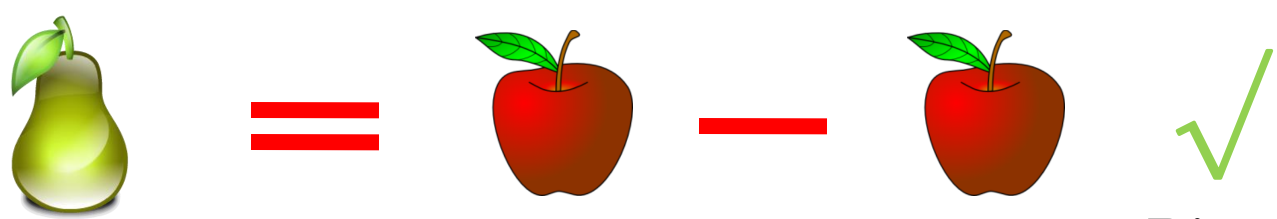
Calculul atenuarii

$$\text{Pierderi} = \frac{P_{out}}{P_{in}}$$

$$\text{Pierderi}[\text{dB}] = [-]10 \cdot \log_{10}\left(\frac{P_{out}}{P_{in}}\right)$$

$$\text{Pierderi}[\text{dB}] = [-]10 \cdot \log_{10}\left(\frac{P_{out}}{P_0} \cdot \frac{P_0}{P_{in}}\right) = [-]10 \cdot \left[\log_{10}\left(\frac{P_{out}}{P_0}\right) - \log_{10}\left(\frac{P_{in}}{P_0}\right)\right]$$

$$\text{Pierderi}[\text{dB}] = [-]\left(P_{out}[\text{dBm}] - P_{in}[\text{dBm}]\right)$$

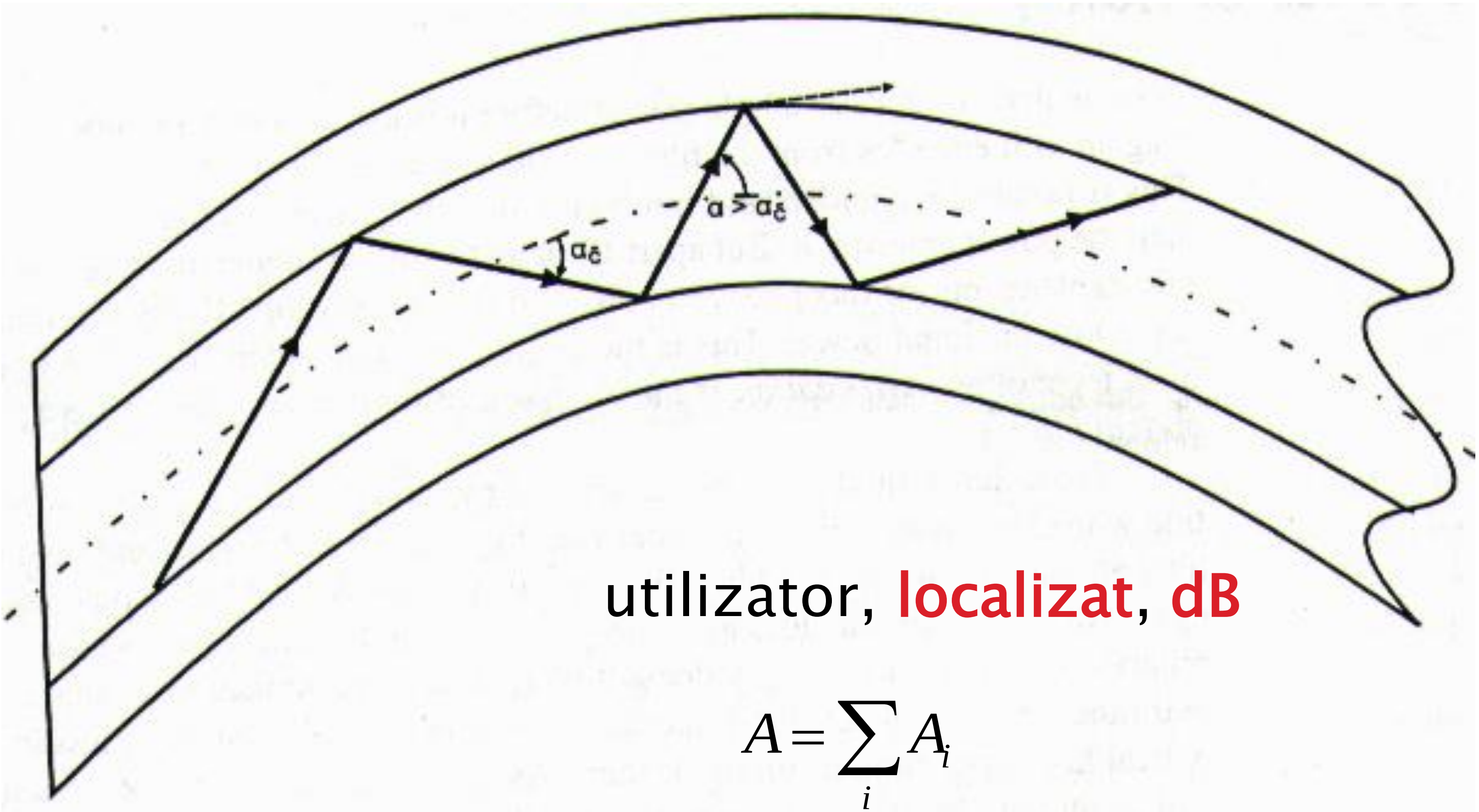


$$\text{Atenuare}[\text{dB/km}] = \frac{\text{Pierderi}[\text{dB}]}{\text{lungime}[\text{km}]}$$

Atenuare

- Macrocurburi
  - utilizator, localizat, dB
- Discontinuitate in fibra
  - utilizator, localizat, dB
- Microcurburi
  - distribuit, tehnologie, dB/km
- Imprastiere
  - distribuit, tehnologie, dB/km
- Absorbtie
  - distribuit, material, dB/km

Macrocurburi



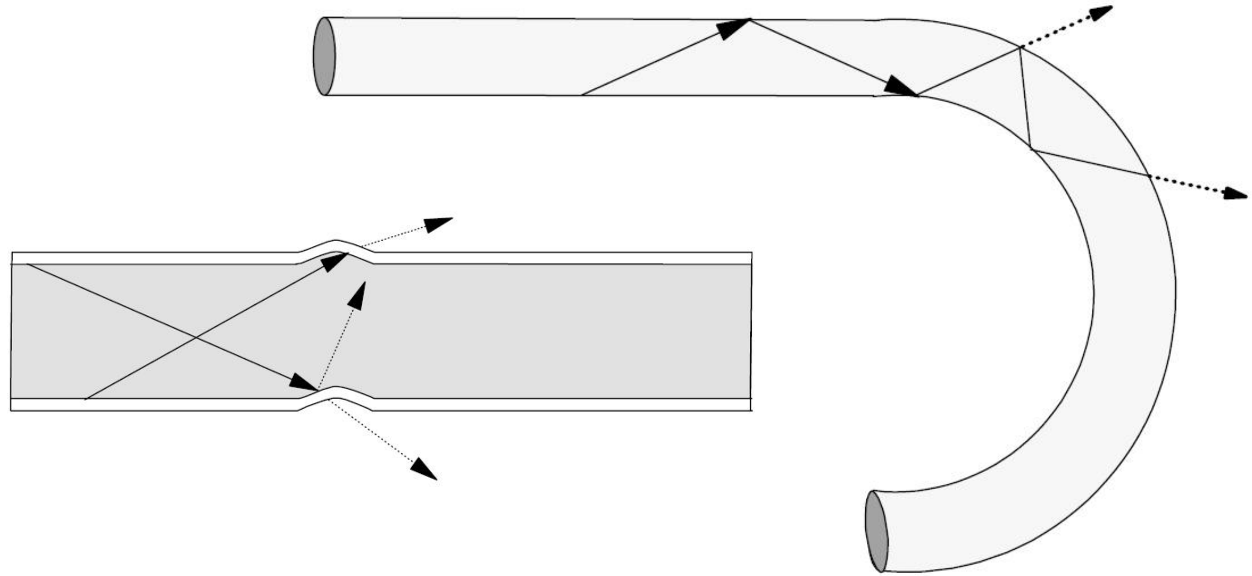
utilizator, localizat, dB

$$A = \sum_i A_i$$

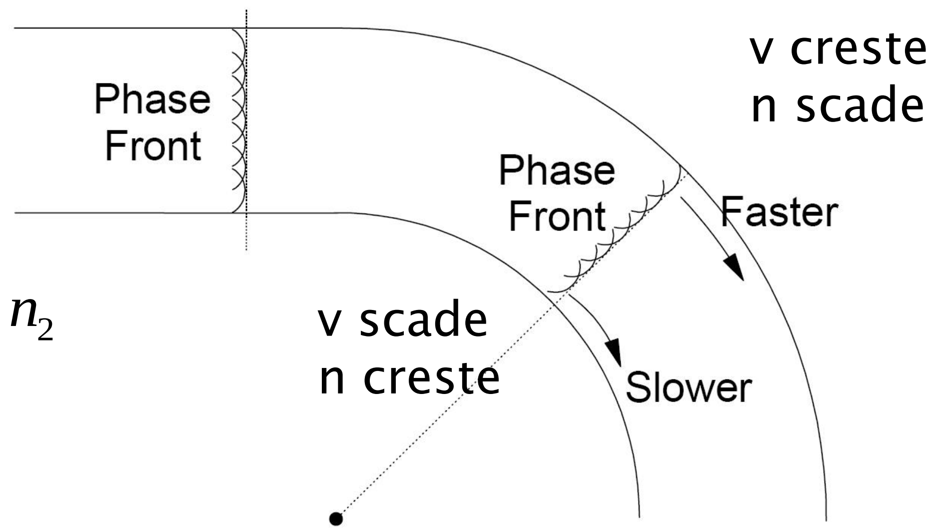
$$A = N \cdot A_i$$

Efectul curburilor

- Multimod



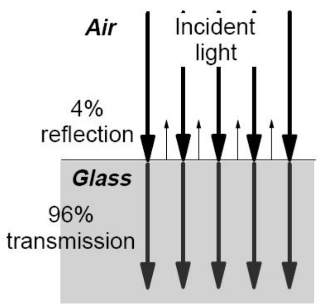
- Monomod

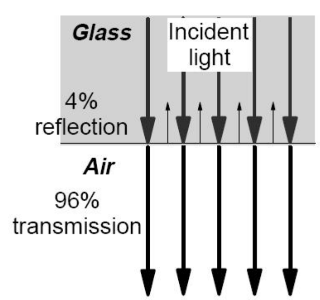


$$R > R_C \quad \Rightarrow \quad n_{1,ext} > n_2$$

Discontinuitate in fibra

- Apare cand nu putem considera fibra un singur ghid dielectric
  - defectiuni
  - conectori



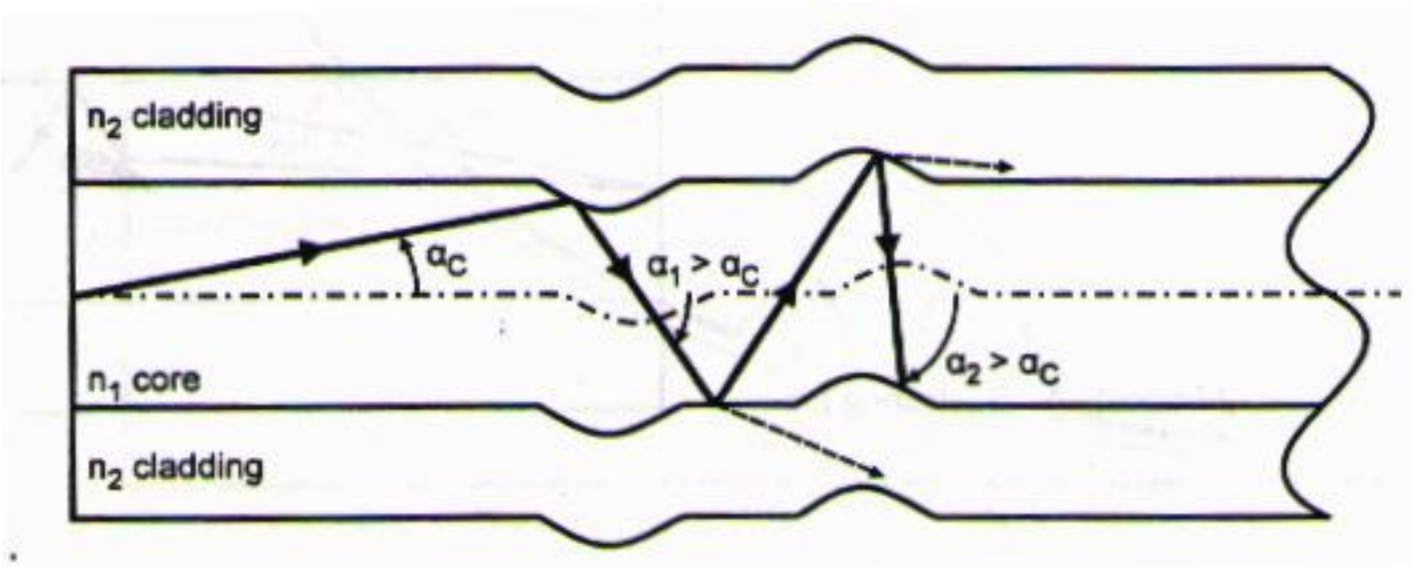


utilizator, **localizat**, **dB**

$$A = \sum_i A_i$$

$$A = N \cdot A_i$$

Microcurburi

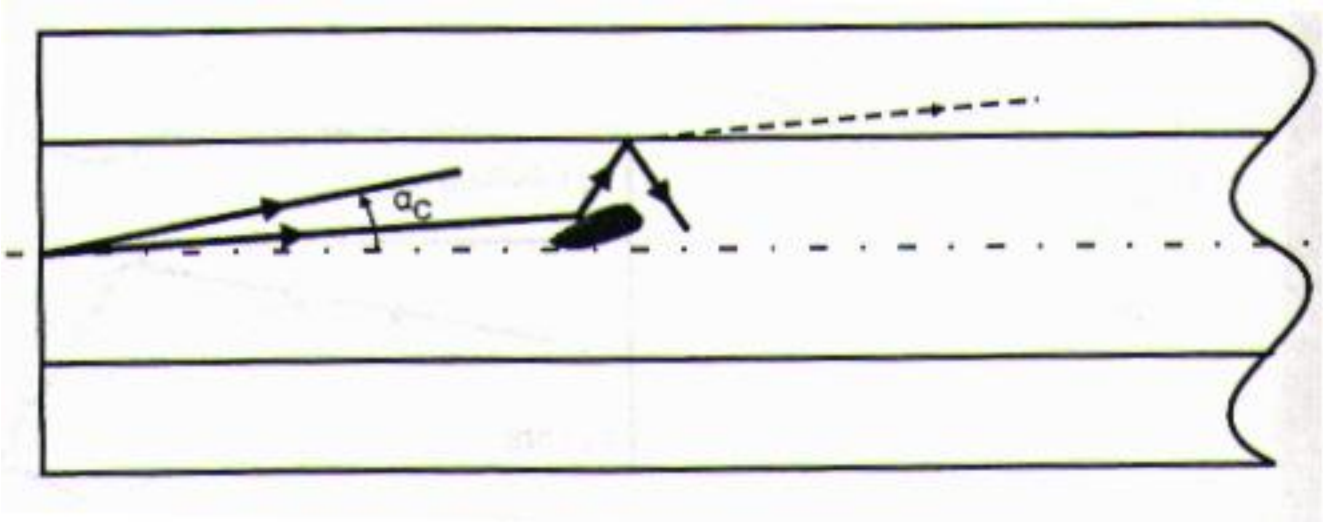


distribuit, tehnologie, dB/km

$$A = A_i \cdot L$$

$$A[dB] = A_i[dB/km] \cdot L[km]$$

Imprastiere

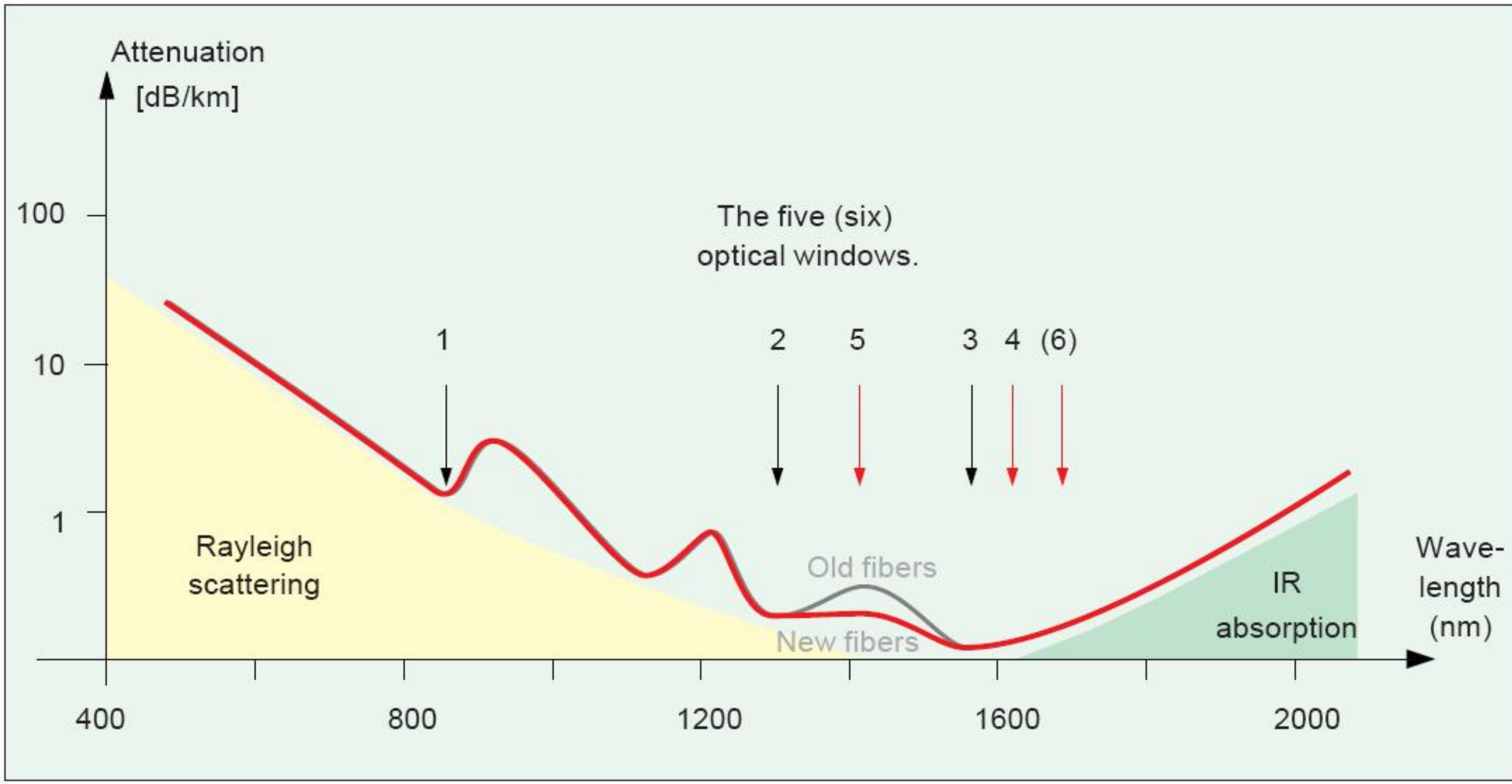


distribuit, tehnologie, dB/km

$$A = A_i \cdot L$$

$$A[dB] = A_i[dB/km] \cdot L[km]$$

Absorbtie

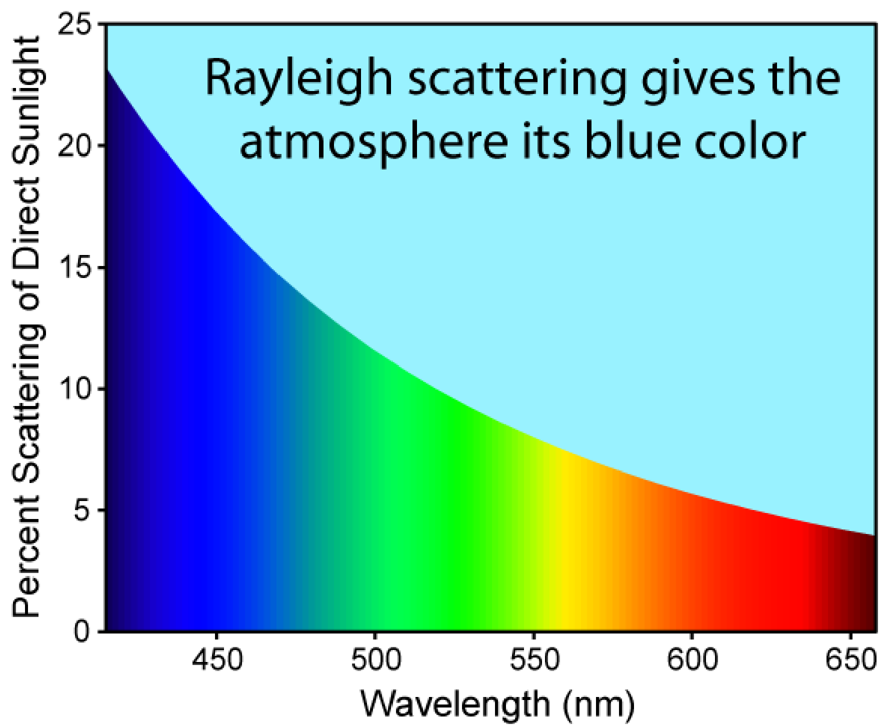


distribuit, material, **dB/km**

$$A[dB] = A_i[dB/km] \cdot L[km]$$

Difractie Rayleygh

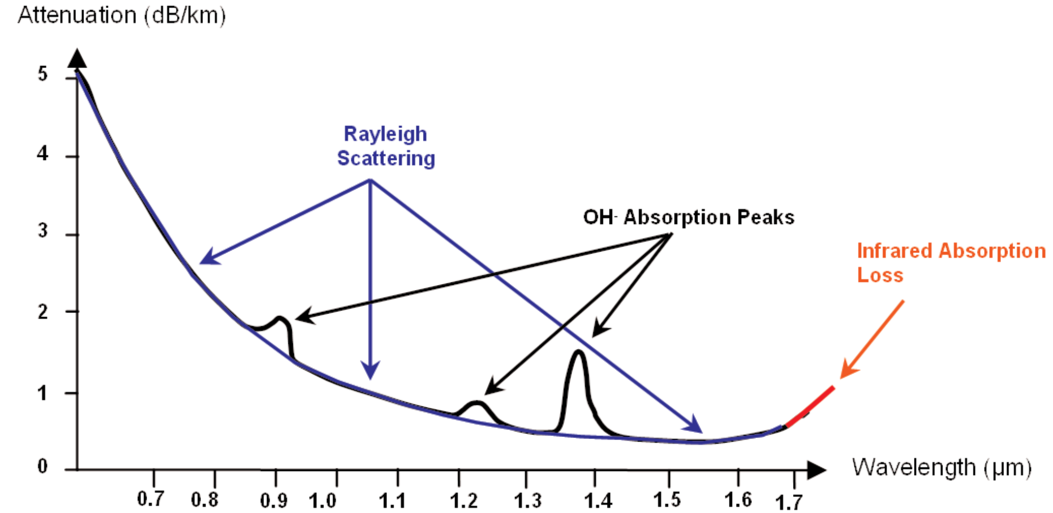
- imprastierea luminii (si a altor radiatii electromagnetice) de particule (molecule) mult mai mici decat lungimea de unda

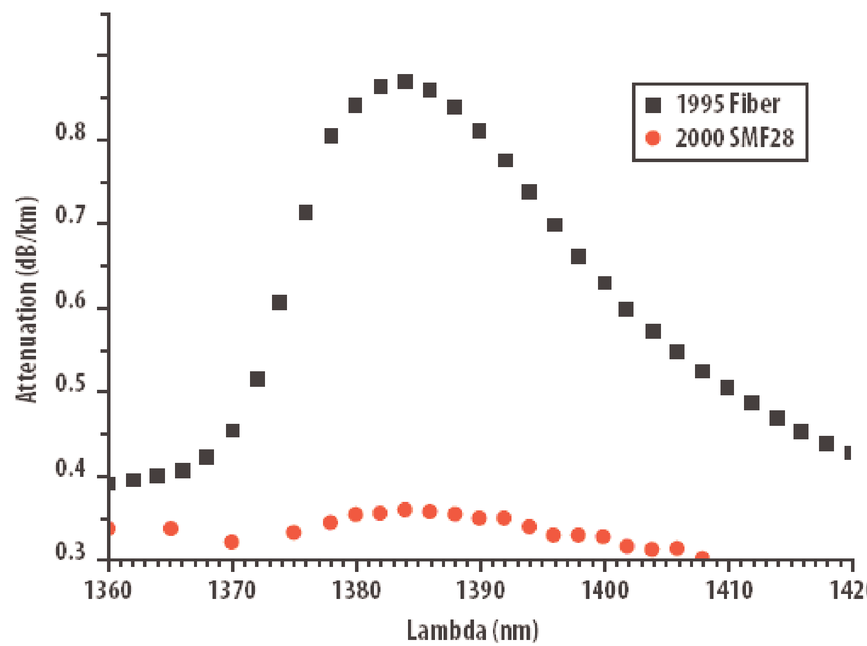


$$A \sim \frac{1}{\lambda^4}$$

Absorbtie OH

- Absorbtie
  - 950nm
  - 1244nm
  - 1383nm
- Apa!





Fiber Attenuation Comparison

Atenuare

$$E_y(z_1) = Ct \cdot e^{-\alpha \cdot z_1} \cdot e^{j(\omega t - \beta \cdot z_1)} \qquad E_y(z_2) = Ct \cdot e^{-\alpha \cdot z_2} \cdot e^{j(\omega t - \beta \cdot z_2)}$$

$$W, P \sim \int E^2$$

$$A = \frac{P_2}{P_1} = \frac{Ct^2 \cdot e^{-2\alpha \cdot z_2}}{Ct^2 \cdot e^{-2\alpha \cdot z_1}} = e^{-2\alpha \cdot (z_2 - z_1)}$$

$$A[dB] = 10 \log_{10} \frac{P_2}{P_1} = 10 \log_{10} \left[e^{-2\alpha \cdot (z_2 - z_1)} \right]$$

$$A[dB] = -20 \cdot \alpha \cdot (z_2 - z_1) \log_{10} e = -8.686 \cdot \alpha \cdot (z_2 - z_1)$$

$$A / L[dB/km] = -8.686 \cdot \alpha < 0$$

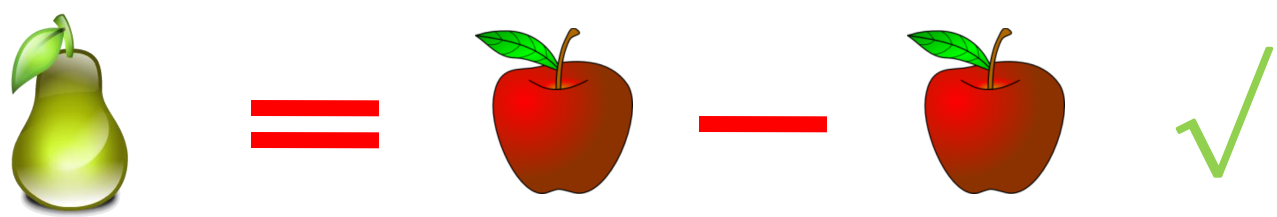
- Atenuarea se exprima de obicei in **dB/km**
  - de obicei valori pozitive
  - semnul = **implicit**

Calculul atenuarii

$$\text{Pierderi} = \frac{P_{out}}{P_{in}}$$

$$\text{Pierderi}[\text{dB}] = [-]10 \cdot \log_{10}\left(\frac{P_{out}}{P_{in}}\right)$$

$$\text{Pierderi}\,[\text{dB}] = [-]\left(P_{out}\,[\text{dBm}] - P_{in}\,[\text{dBm}]\right)$$

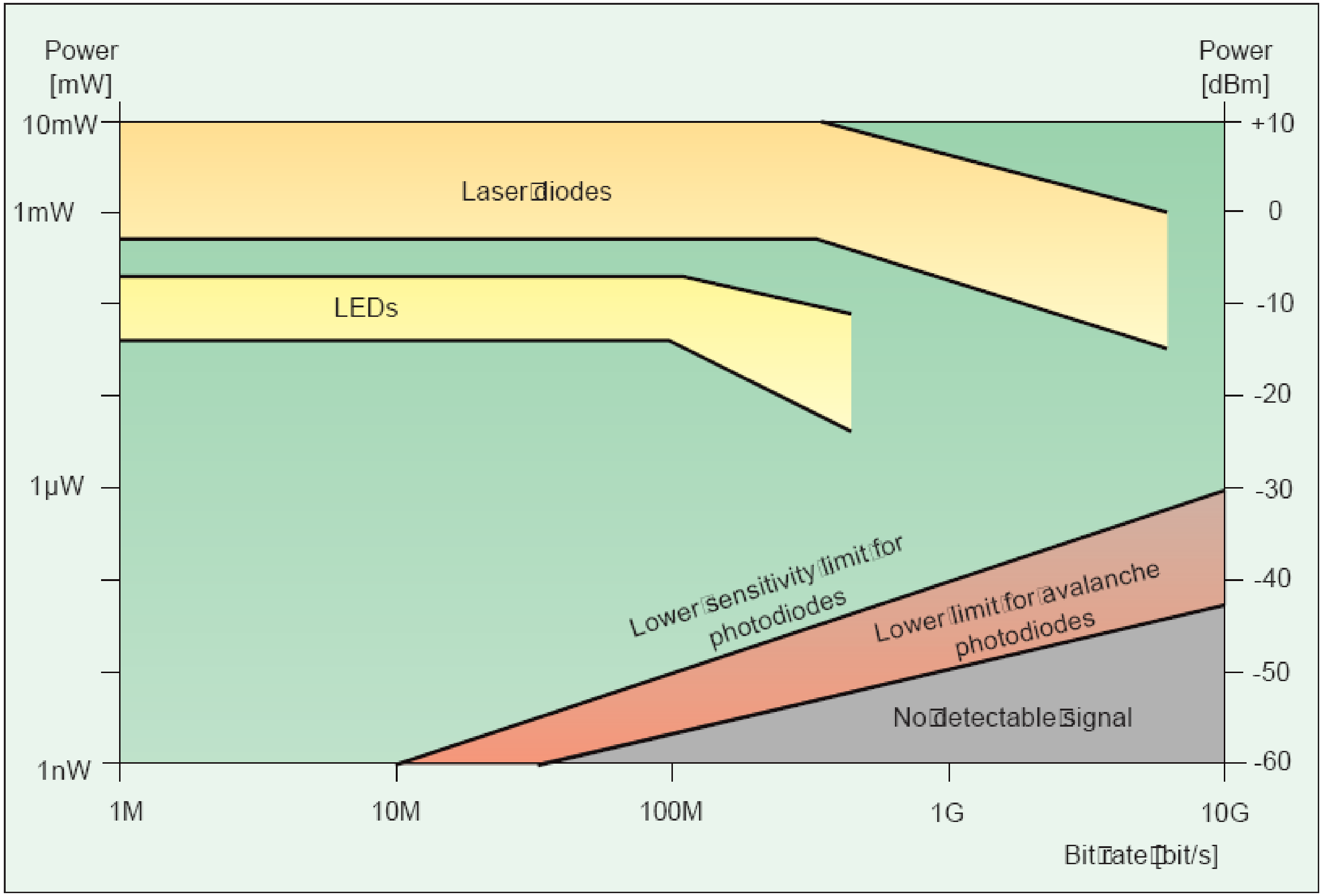


$$\text{Atenuare}[\text{dB/km}] = \frac{\text{Pierderi}[\text{dB}]}{\text{lungime}[\text{km}]}$$

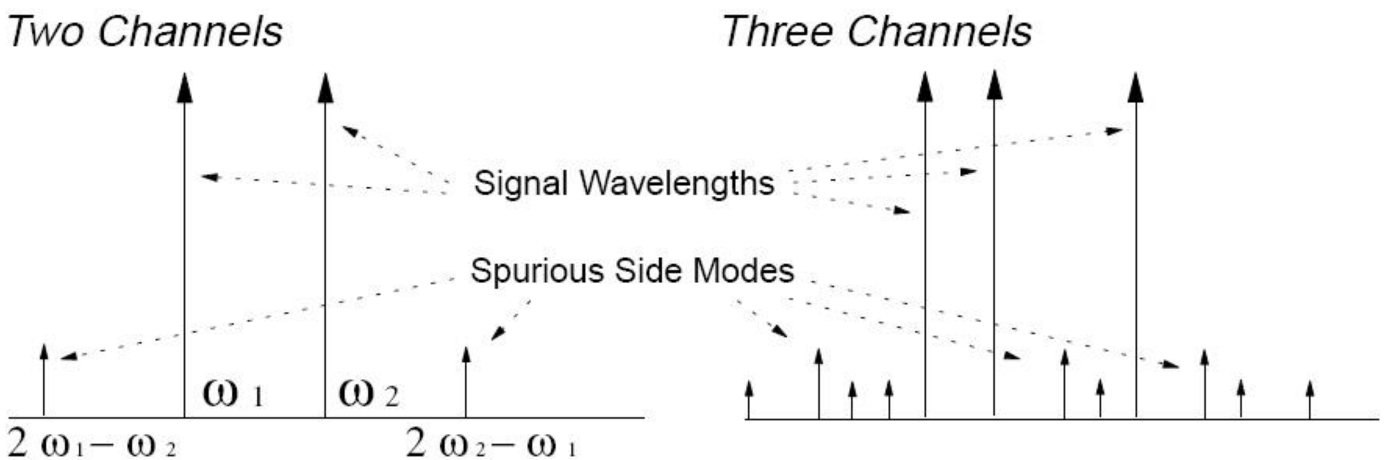
Efecte neliniare in fibra

- Stimulated Brillouin Scattering, SBC
  - difractia luminii inspre emitator datorita undelor mecano-acustice generate in fibra
  - 6-10 dBm
- Stimulated Raman Scattering, SRS
  - interactiunea luminii cu vibratiile moleculare
  - 27 dBm (~1W)
- Self Phase Modulation, SPM
  - Frontiera impulsului implica indice de refractie variabil in timp moduland faza impulsului
  - 5 dBm
  - Cross Phase Modulation, CPM
- Four-Wave Mixing, FWM
  - 0 dBm

Limite putere/bandă a dispozitivelor optoelectronice

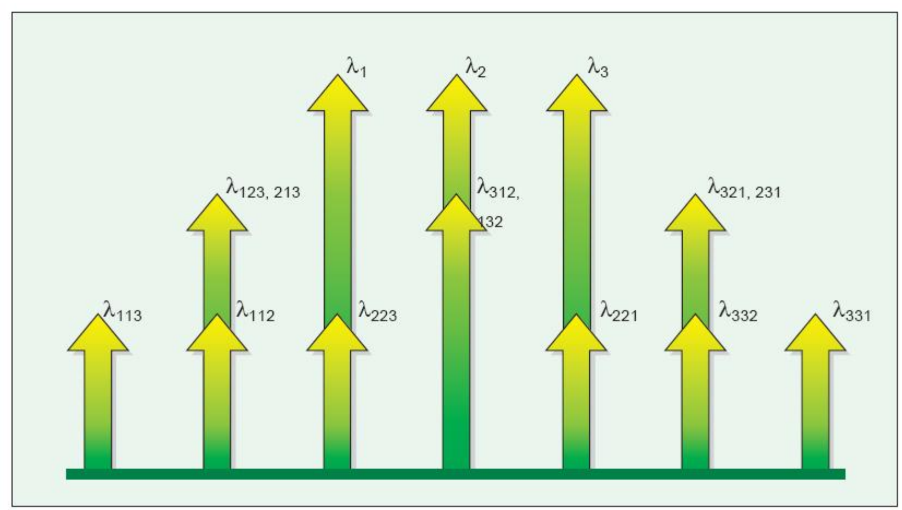


Four-Wave Mixing, FWM



$$NL = \frac{1}{2}\left(N^3 - N^2\right)$$

N = 2, NL = 4
N = 3, NL = 9
N = 16, NL = 1920

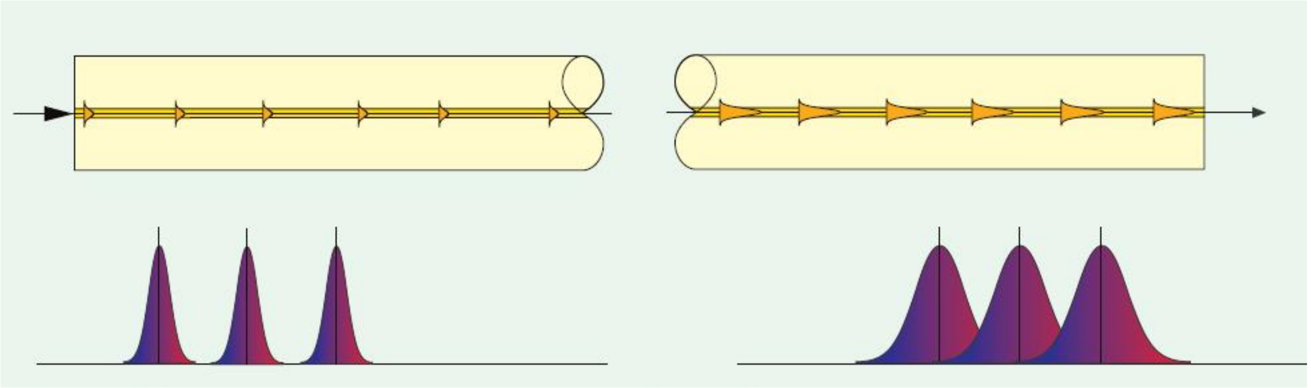


Fenomene de interes

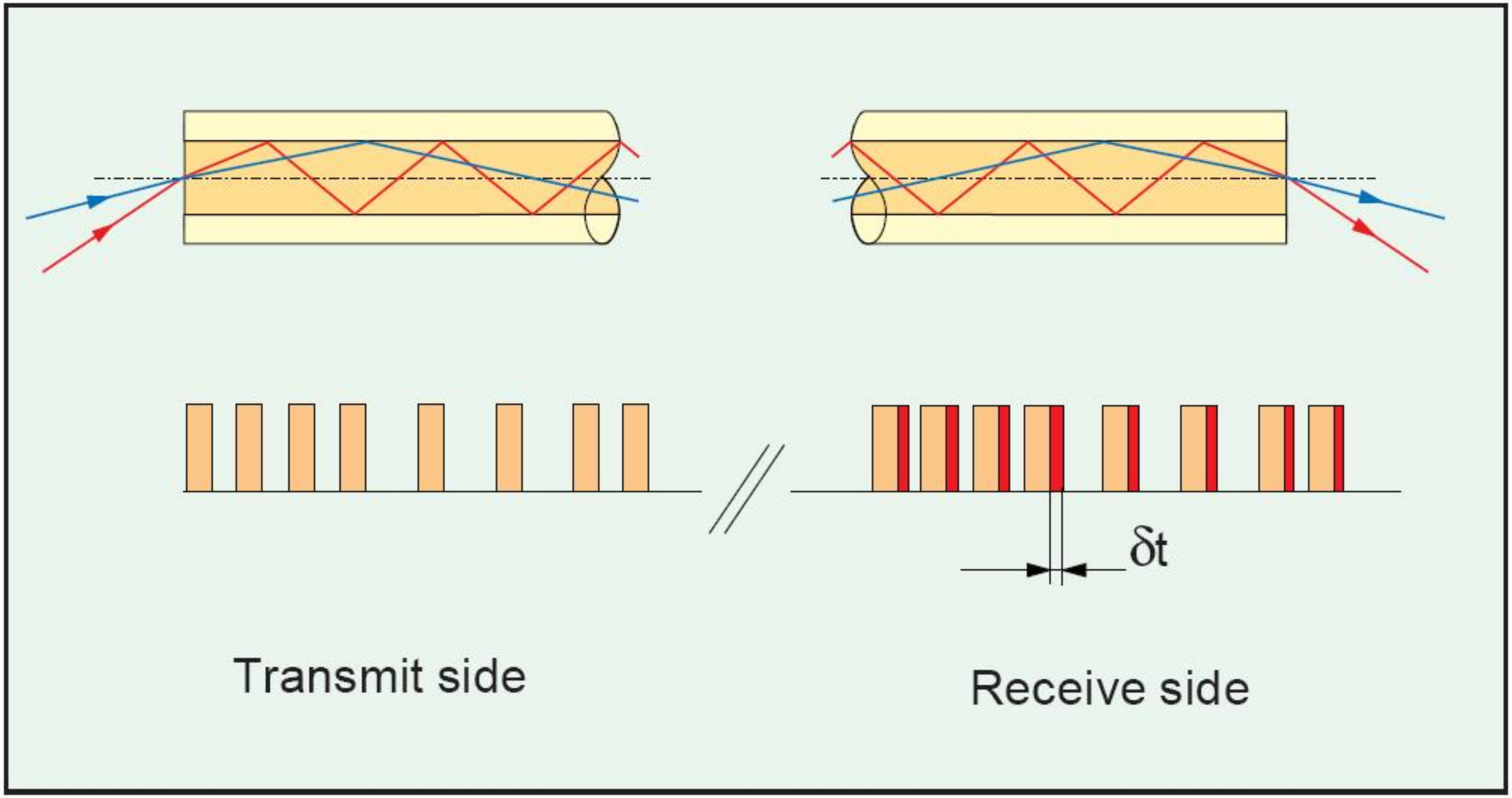
- Cat de departe pot transmite semnalul luminos pe fibra
  - atenuare
- Cat de rapid pot transmite informația
  - **dispersie**

Dispersia

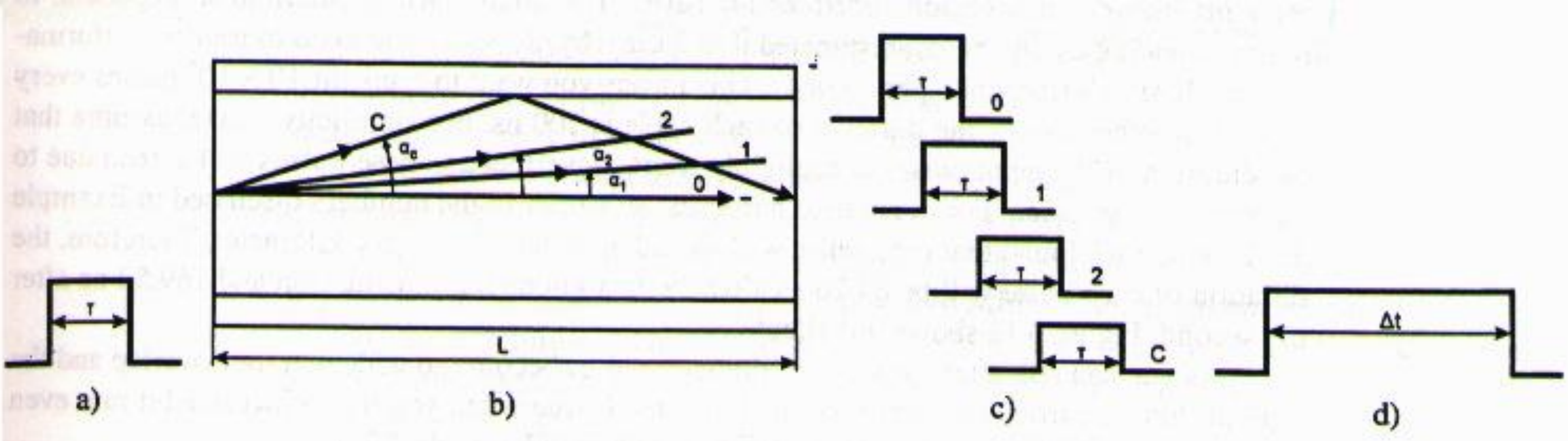
- Propagarea cu viteze diferite a radiatiilor cu trasee/lungimi de unda diferite
  - intermodala (**modala** – depinde de prezenta modurilor)
  - intramodala (**cromatica** – depinde de lungimea de unda)
    - de material
    - de ghid



Dispersia modala



Dispersia modala



$$t_0 = \frac{L}{v} \qquad t_C = \frac{L}{v \cdot \cos\alpha_C} \qquad v = \frac{c}{n_2} \qquad \cos\alpha_C = NA$$

$$\Delta t_{SI} = t_C - t_0 = \frac{L \cdot n_2}{c} \cdot \left(\frac{n_2 - n_1}{n_2} \right) \qquad \Delta t_{SI} = t_C - t_0 = \frac{L \cdot n_2}{c} \cdot \Delta$$

$$\Delta = \frac{n_2 - n_1}{n_1} << 1 \qquad \Delta t_{SI} = t_C - t_0 \approx \frac{L}{2 \cdot c \cdot n_2} \cdot (NA)^2$$

$$\Delta t_{SI} \to dt$$

Dispersia modala

- salt de indice

$$dt = \frac{L \cdot n_2^2}{c \cdot n_1}\left(\frac{n_2 - n_1}{n_2}\right) \approx \frac{L \cdot NA^2}{2 \cdot c \cdot n_2}$$

intarzierea intre moduri cand

$$\Delta = \frac{n_2 - n_1}{n_1} << 1$$

$$\Delta\tau_{\text{mod}}^2 = \frac{1}{3}\left(\frac{dt}{2}\right)^2$$

$$\Delta\tau_{\text{mod}} \cong \frac{L \cdot n_2 \cdot \Delta}{2\sqrt{3} \cdot c} \approx \frac{L \cdot NA^2}{4\sqrt{3} \cdot c \cdot n_2}$$

- indice gradat

$$dt = \frac{L \cdot n_2 \cdot \Delta^2}{2c} \approx \frac{L \cdot NA^4}{8 \cdot c \cdot n_2^3}$$

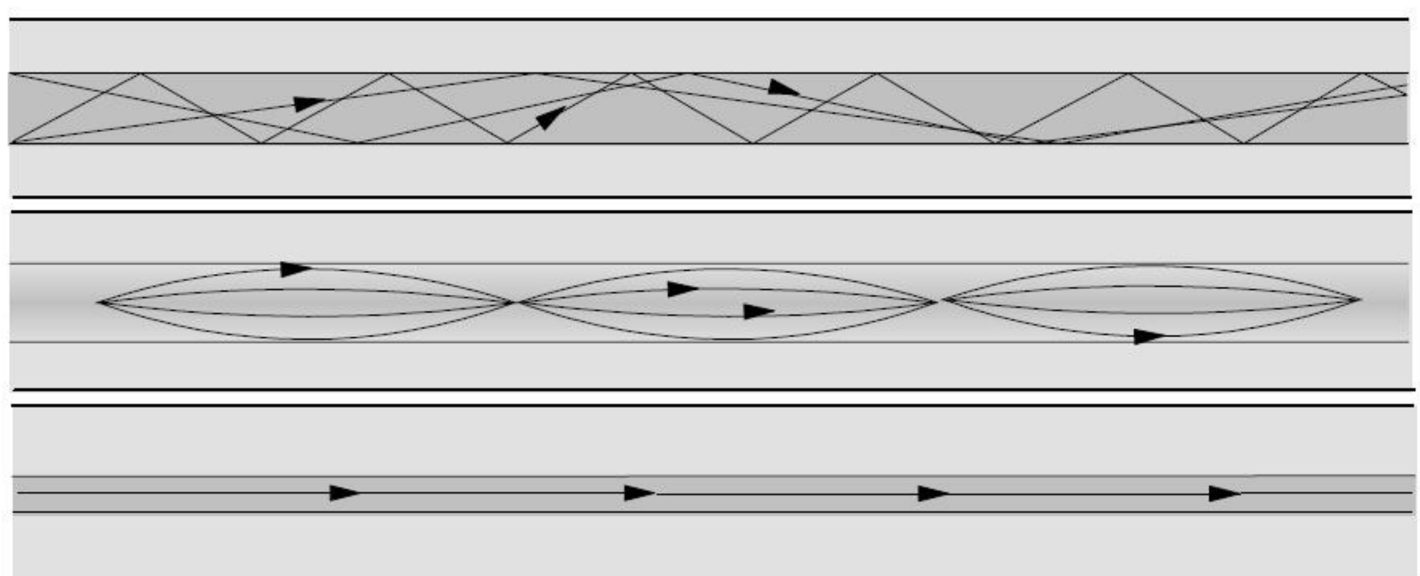
$$\Delta\tau_{\text{mod}} \cong \frac{L \cdot n_2 \cdot \Delta^2}{4\sqrt{3} \cdot c}$$

$$NA = 0.1 \div 0.2 < 1$$

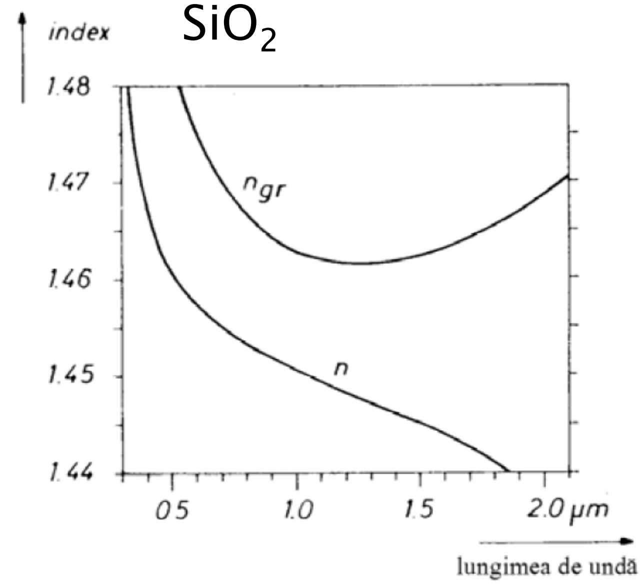
n_2 – miez
n_1 – teaca
$n_2 > n_1$!!

Dispersia modala

- Mai mare la fibre multimod cu salt de indice
- Mai mica la fibre multimod cu indice gradat
  - traseele mai lungi trec prin zone cu indice mai mic
- Inexistenta la fibrele monomod

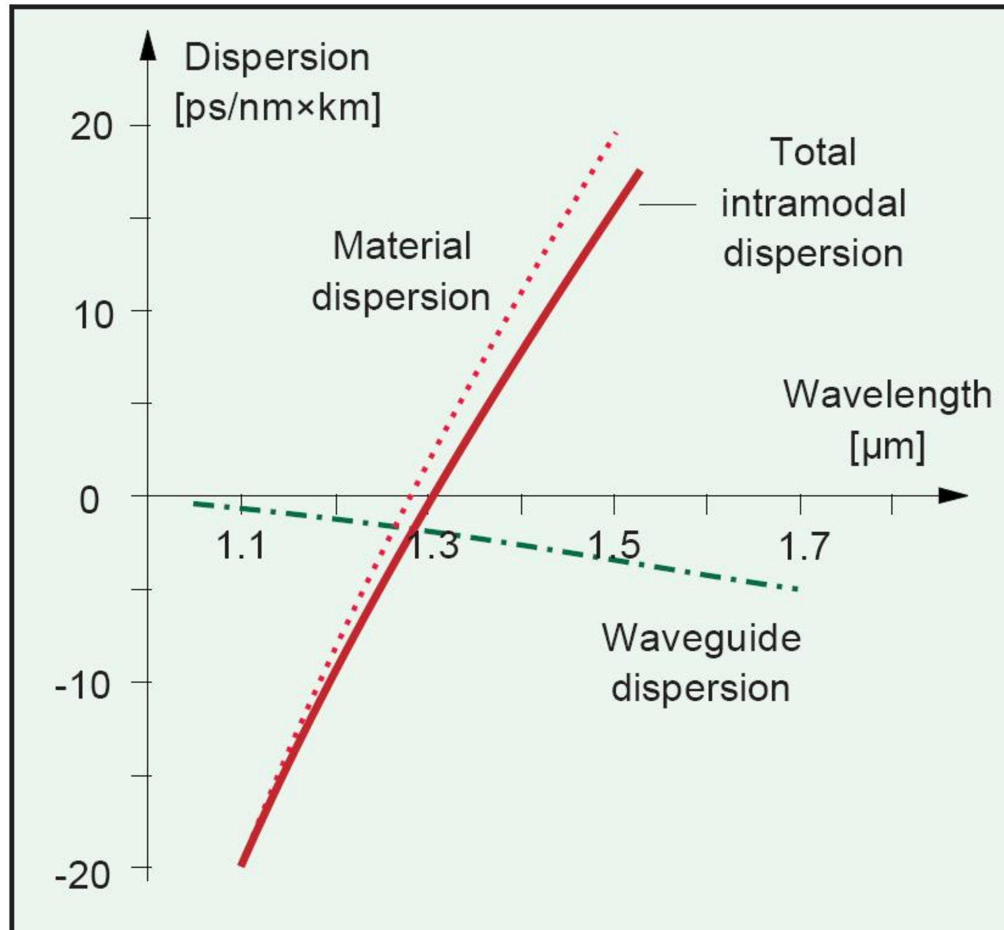


Dispersia de material



$$n_{gr} = n - \lambda \frac{dn}{d\lambda}$$

$$\Delta \tau_{mat} = \frac{L \cdot \lambda \cdot \Delta\lambda}{c} \cdot \frac{d^2 n}{d\lambda^2}$$

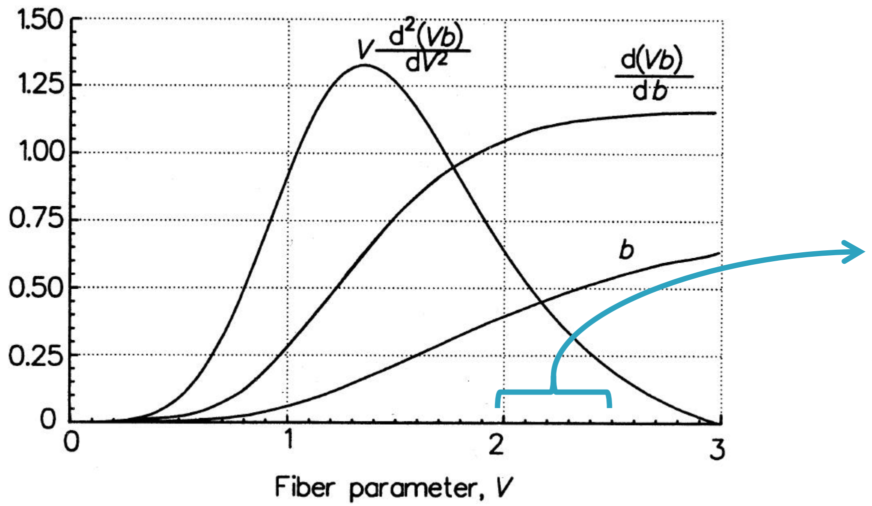


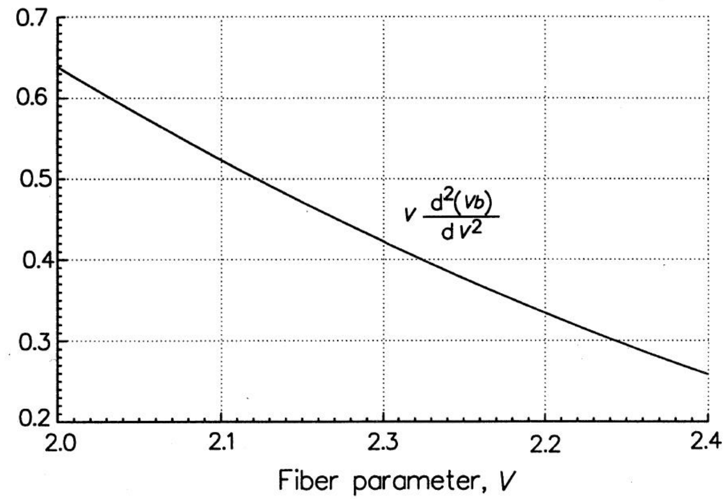
Dispersia de ghid

- Neglijabila in fibrele multimod fata de dispersia modala

$$\Delta\tau_{gh} = \frac{n \cdot L \cdot \Delta}{c} \cdot \frac{\Delta\lambda}{\lambda} \cdot \left(V \frac{d^2(Vb)}{dV^2} \right)$$

b – constanta de propagare normalizata

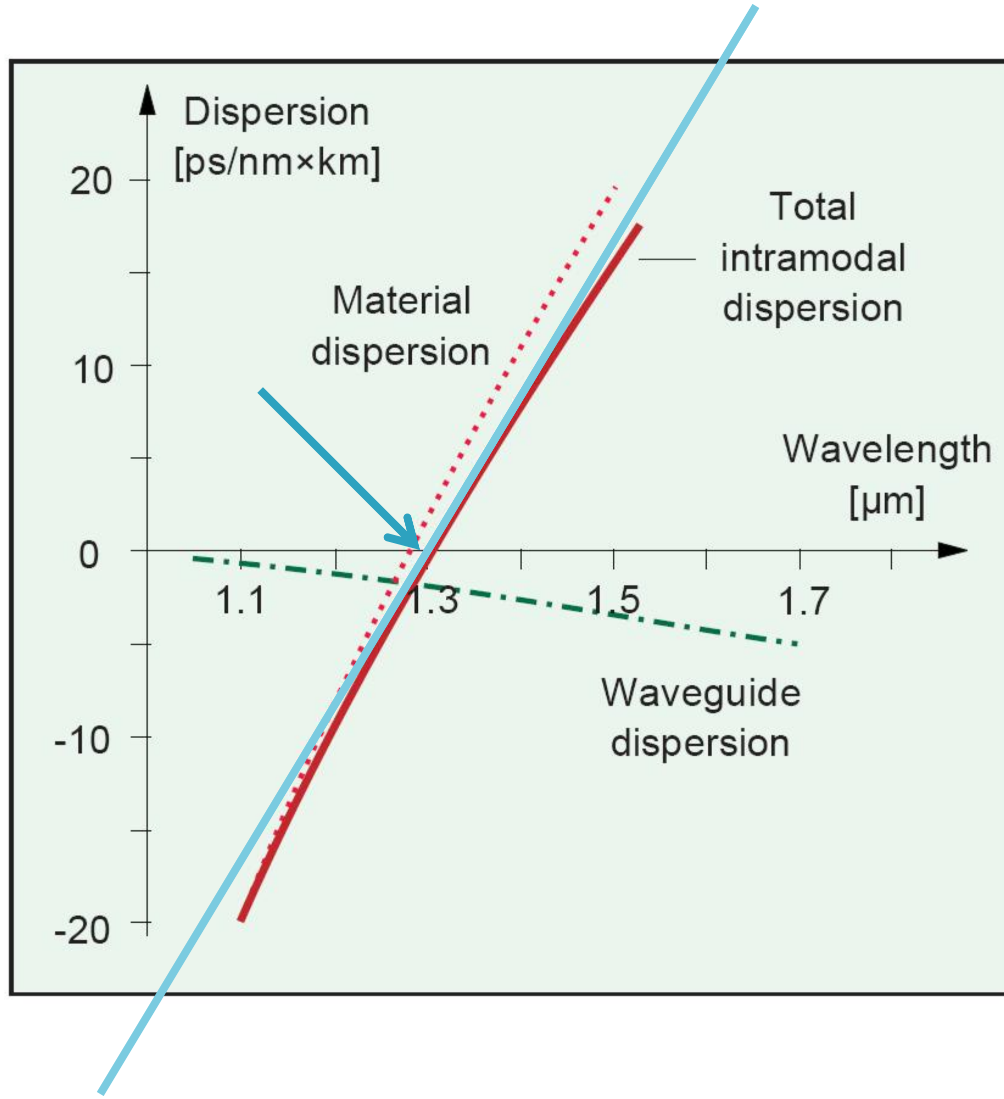




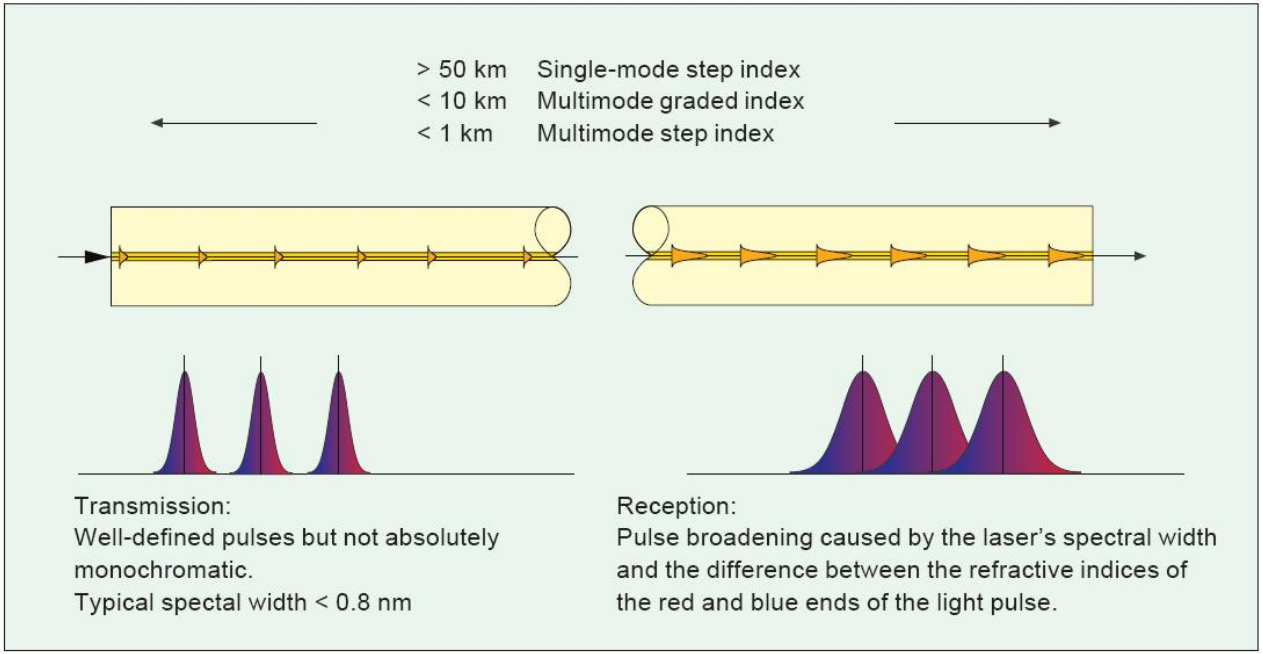
$$V \le V_C = 2.405$$

Dispersia cromatica (gh+mat)

- Variatie aproximativ liniara
- Caracterizata de panta si punctul de trecere prin 0



Dispersia cromatica (gh+mat)



$$\Delta\tau_{cr} = D(\lambda)\cdot\Delta\lambda\cdot L$$

$$D(\lambda) = \frac{S_0}{4}\cdot\left(\lambda - \frac{\lambda_0^4}{\lambda^3}\right)$$

S_0 panta dispersiei – $ps/nm^2/km$

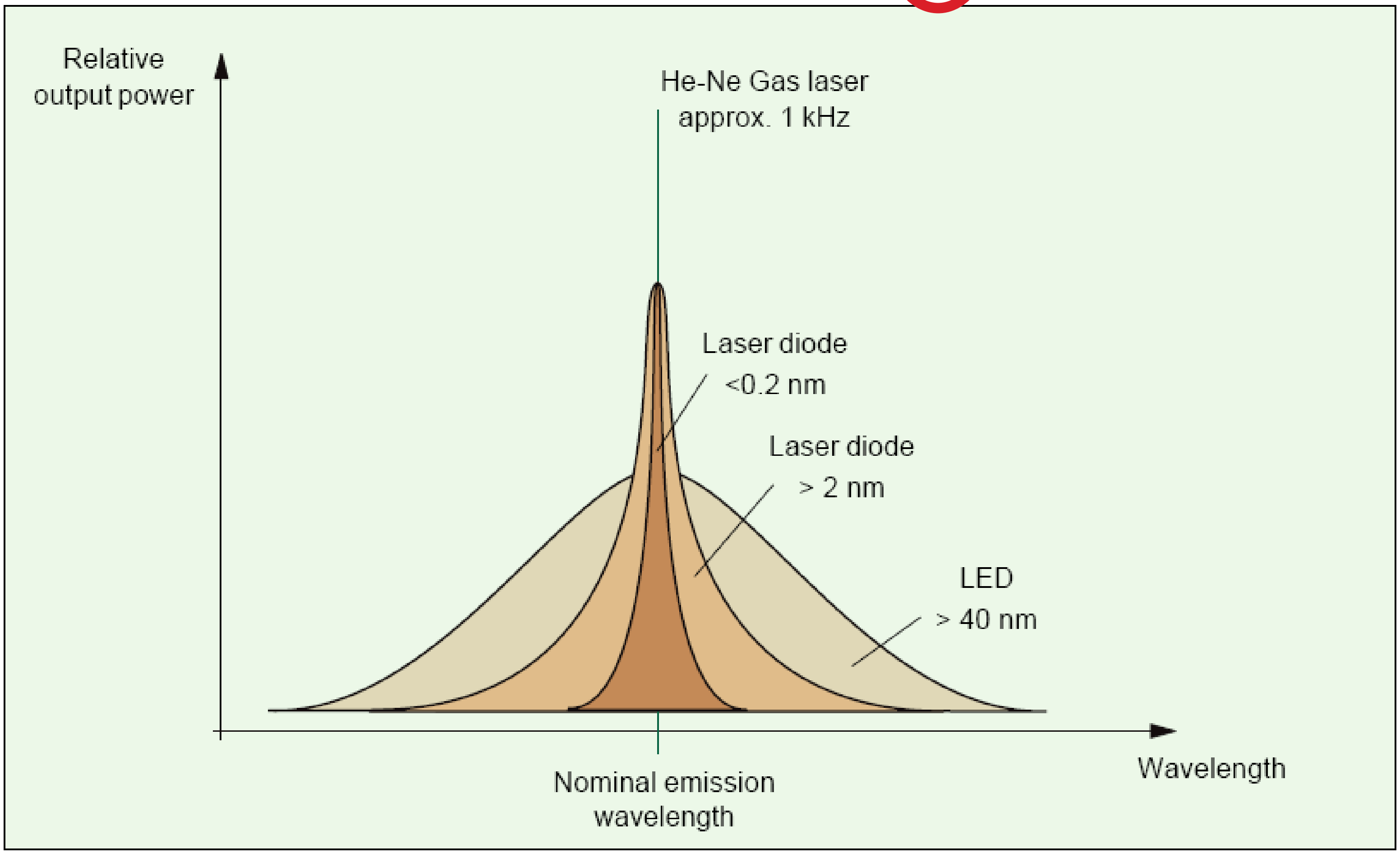
$$D(\lambda_0) = 0$$

- D(λ) ≈ 100 + 0.4 (850 – λ) [ps/nm/km] pentru 800 < λ < 900 nm
- D(λ) ≤ 3,5 ps/nm/km pentru 1285 < λ < 1330 nm
- D(λ) ≤ 17 ps/nm/km pentru 1525 < λ < 1575 nm

$$D(\lambda) = \frac{S_0}{4}\cdot\left(\lambda - \frac{\lambda_0^4}{\lambda^3}\right)$$

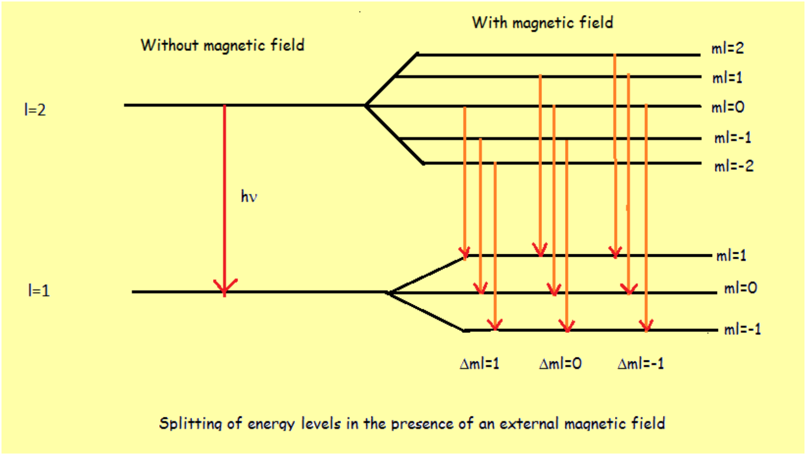
Calitatea spectrală a emiţătorilor optici

$$\Delta\tau_{cr} = D(\lambda)\cdot\Delta\lambda\cdot L$$



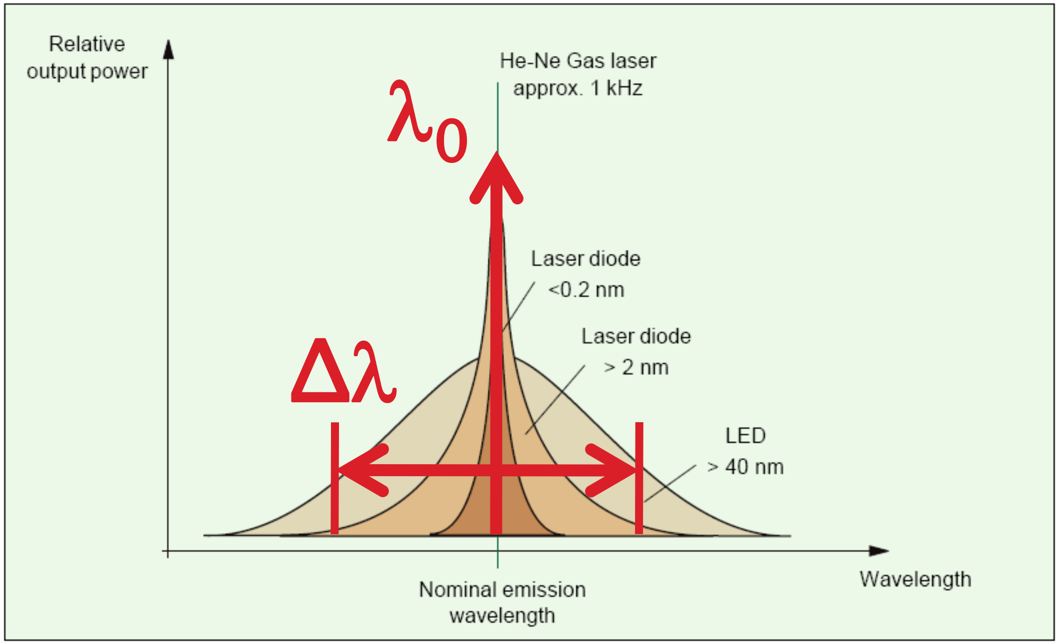
Calitatea spectrală a emiţătorilor optici

- degenerarea nivelelor energetice duce la aparitia benzilor energetice

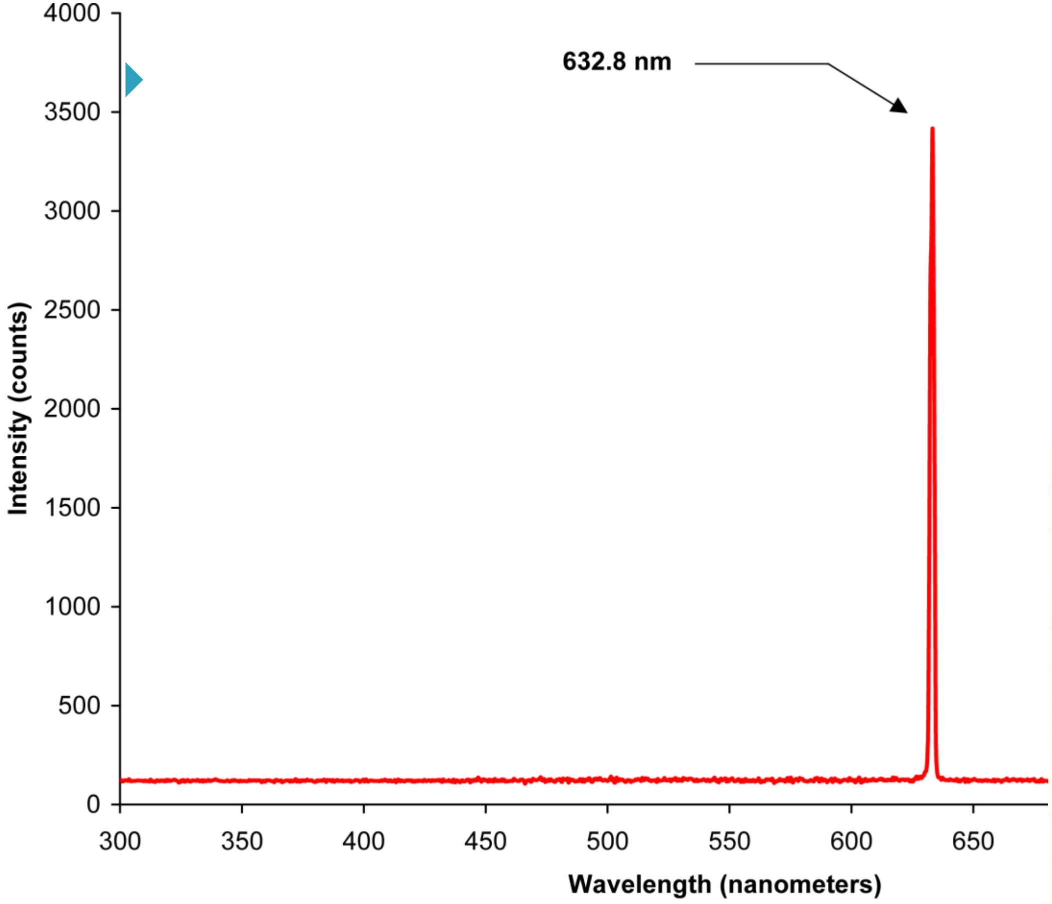


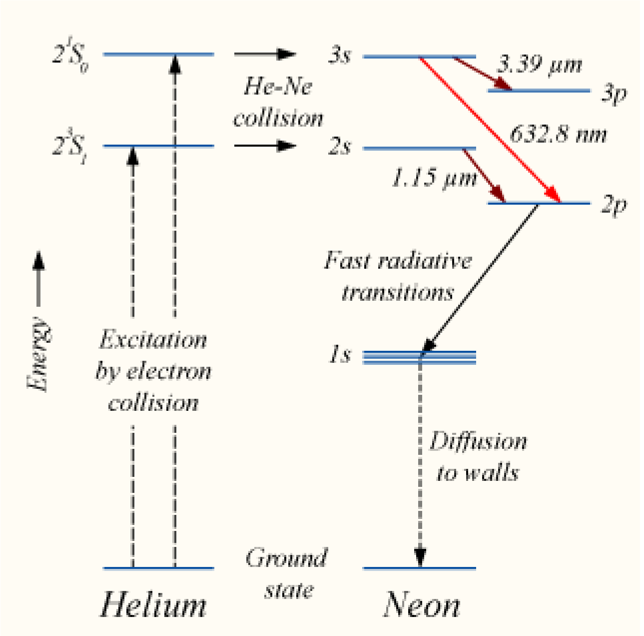
- Multitudinea de tranzitii posibile intre cate doua nivele situate in benzi energetice diferite duce la largirea caracteristicii spectrale a surselor

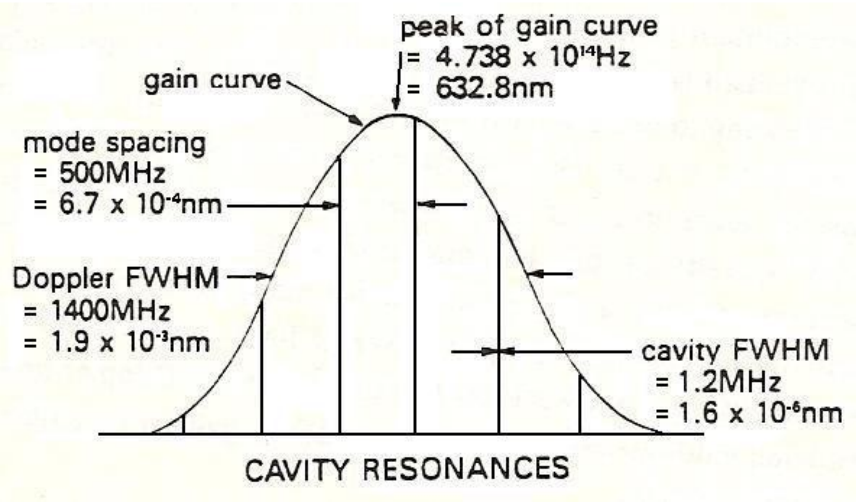
$$\lambda_0 \rightarrow \left[\lambda_0 - \frac{\Delta\lambda}{2}, \lambda_0 + \frac{\Delta\lambda}{2}\right]$$



He–Ne Laser

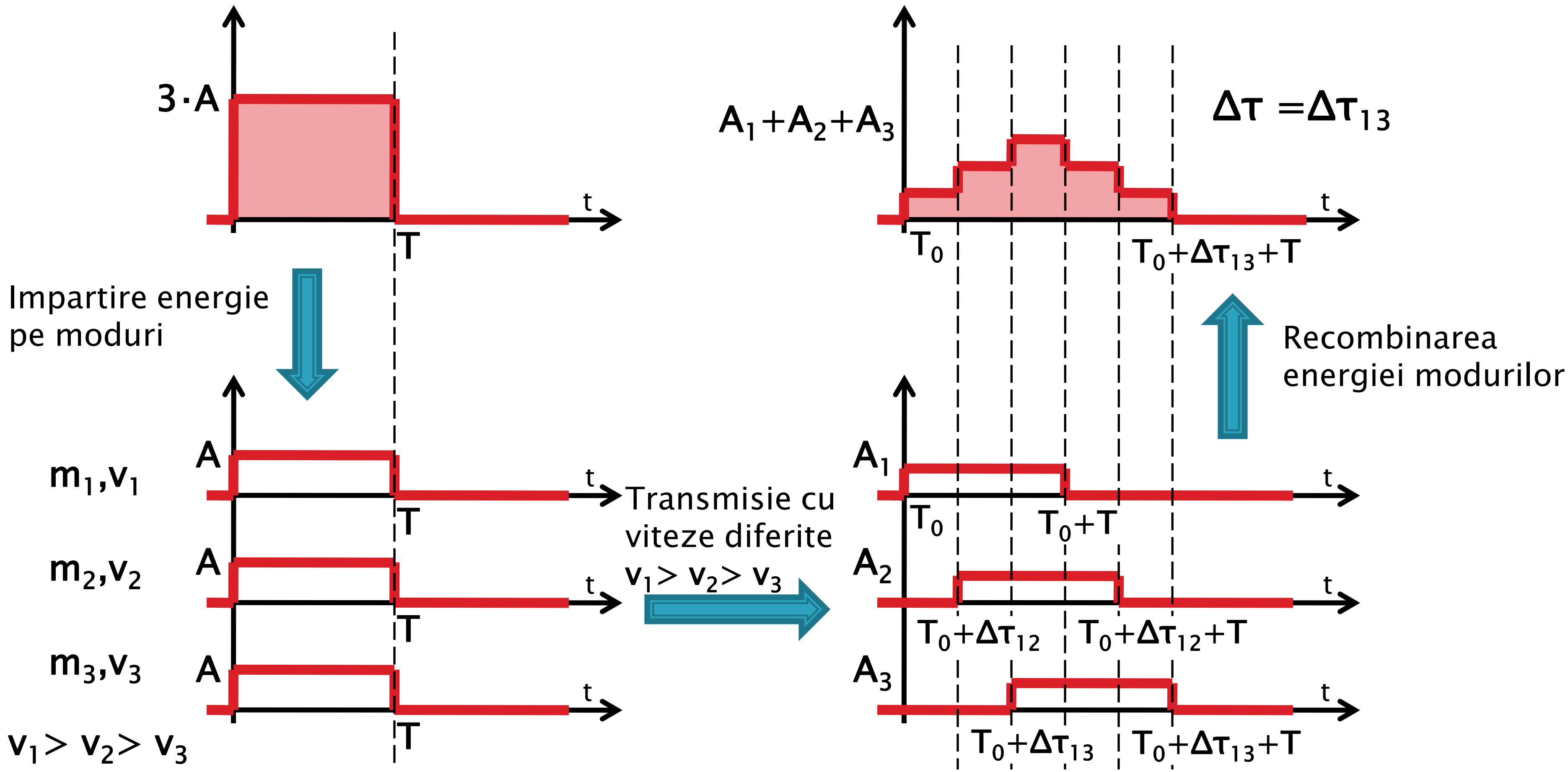






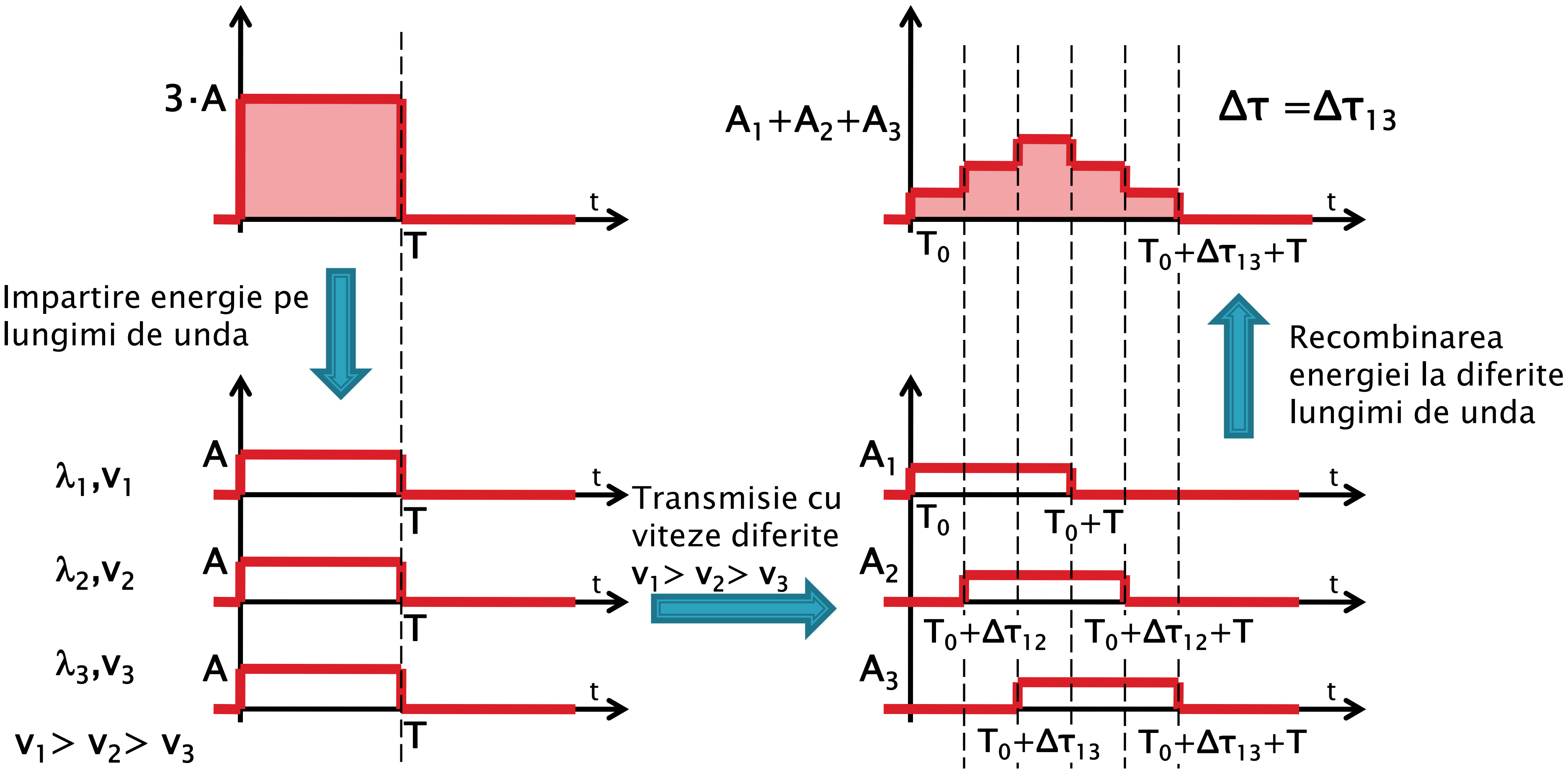
$$\Delta\lambda = 0.002\, nm$$

Dispersia modala



Conceptual→ $f(t)=\int_{-\infty}^{\infty} g(\omega)\cdot e^{j\omega t}d\omega$

Dispersia cromatica (gh+mat)

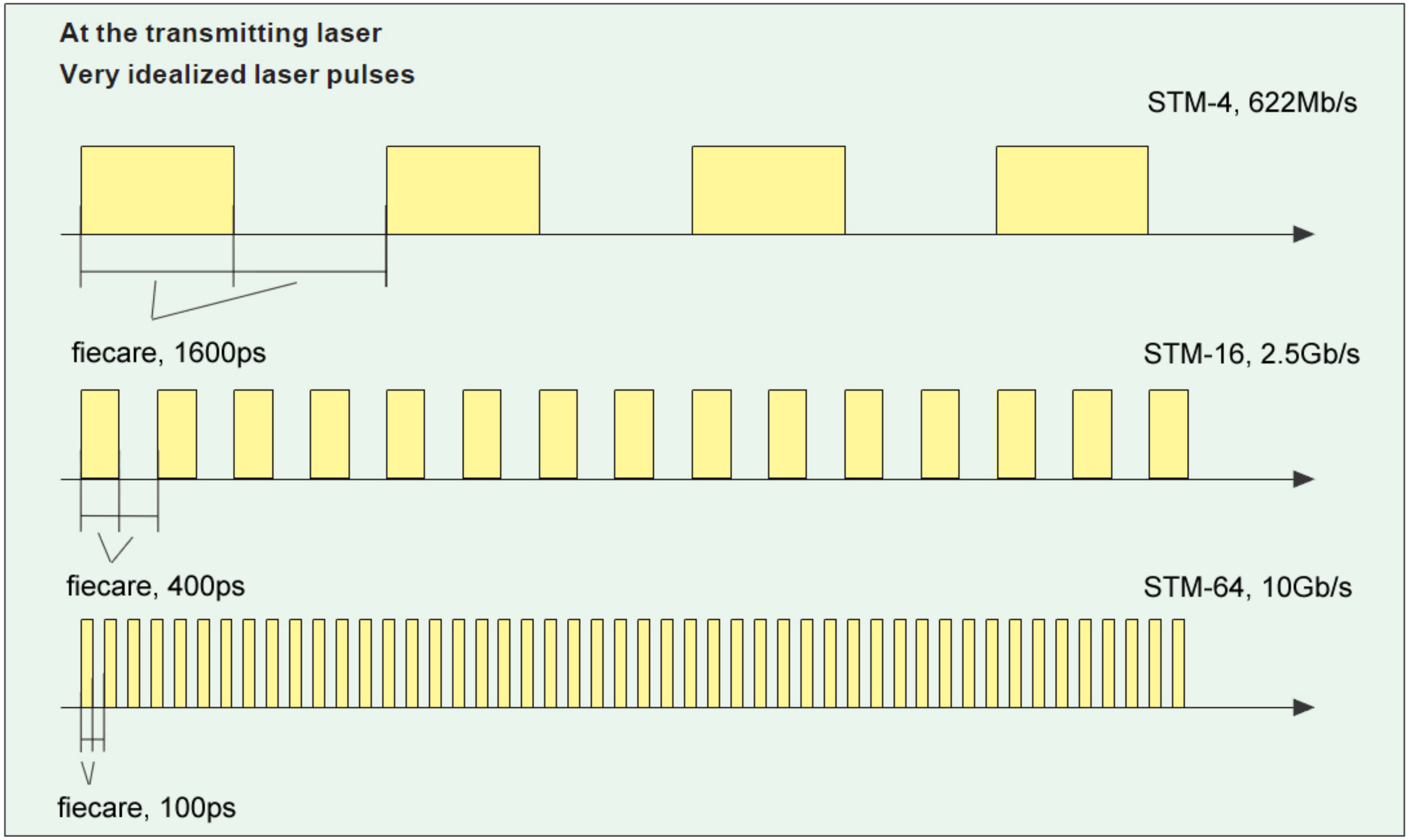


Efectiv→ $f(t) = \int_{-\infty}^{\infty} g(\omega) \cdot e^{j\omega t} d\omega$

Dispersie exemplu – 1

- transmisii cu viteze diferite

$$\Delta\tau_{cr} = D(\lambda)\cdot\Delta\lambda\cdot L$$



Dispersie exemplu – 2

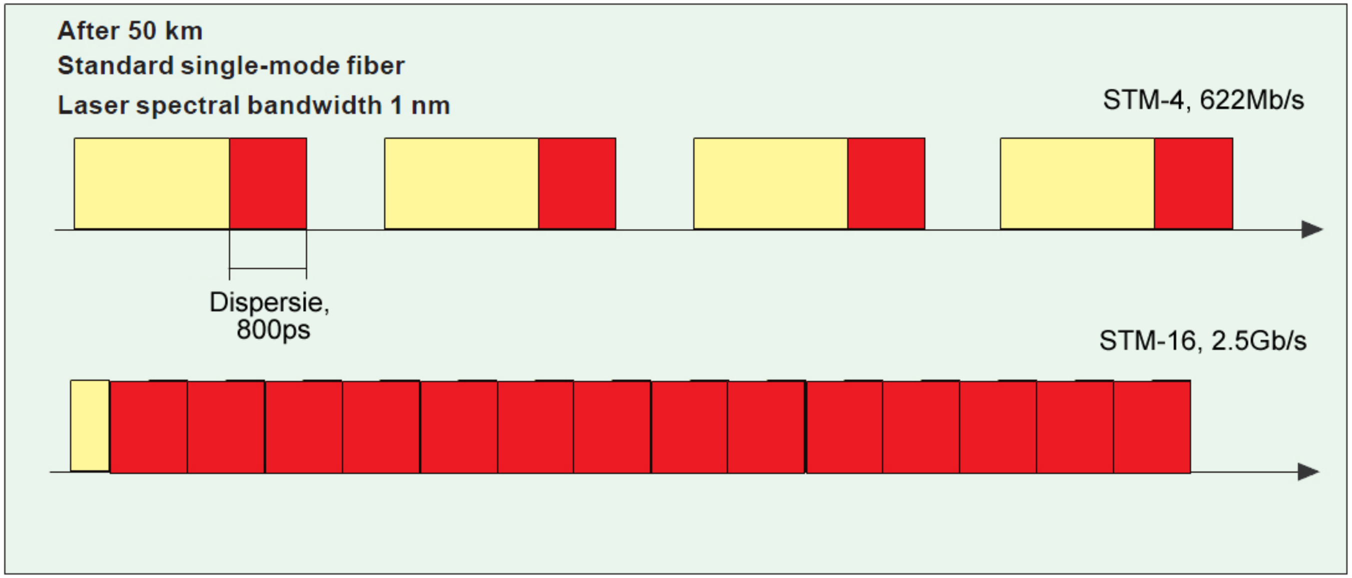
- 1550nm
- Efectul **sursei**
  - fibra monomod cu dispersia 16ps/nm/km@1550
  - latimea spectrala a sursei $\Delta\lambda$=1nm
  - 50km

$$\Delta\tau_{cr} = D(\lambda)\cdot\Delta\lambda\cdot L$$

$$\Delta\tau_{cr} = D(\lambda)\cdot\Delta\lambda\cdot L$$

$$\Delta\tau_{cr} = 16\cdot 1\cdot 50\ ps = 800\ ps$$

$$[\Delta\tau_{cr}] = \frac{ps}{nm\cdot km}\cdot nm\cdot km = ps$$



100<400<800<1600

Dispersie exemplu – 3

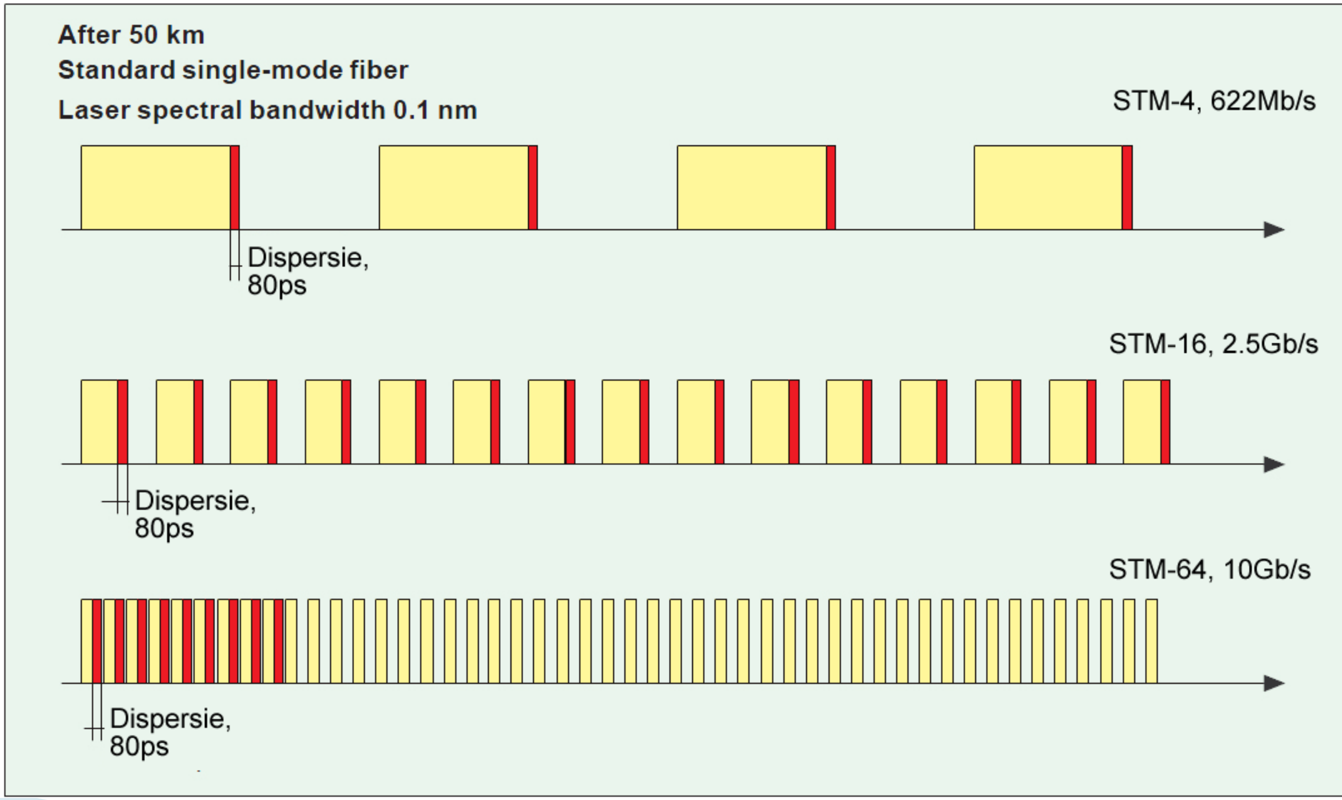
- 1550nm
- Efectul **sursei**
  - fibra monomod cu dispersia 16ps/nm/km@1550
  - latimea spectrala a sursei **Δλ=0.1nm**
  - 50km

$$\Delta\tau_{cr} = D(\lambda)\,\Delta\lambda\,L$$

$$\Delta\tau_{cr} = D(\lambda)\cdot\Delta\lambda\cdot L$$

$$\Delta\tau_{cr} = 16\cdot 0.1\cdot 50\ ps = 80\ ps$$

$$[\Delta\tau_{cr}] = \frac{ps}{nm\cdot km}\cdot nm\cdot km = ps$$



100≈80<400<1600

Dispersie exemplu – 4

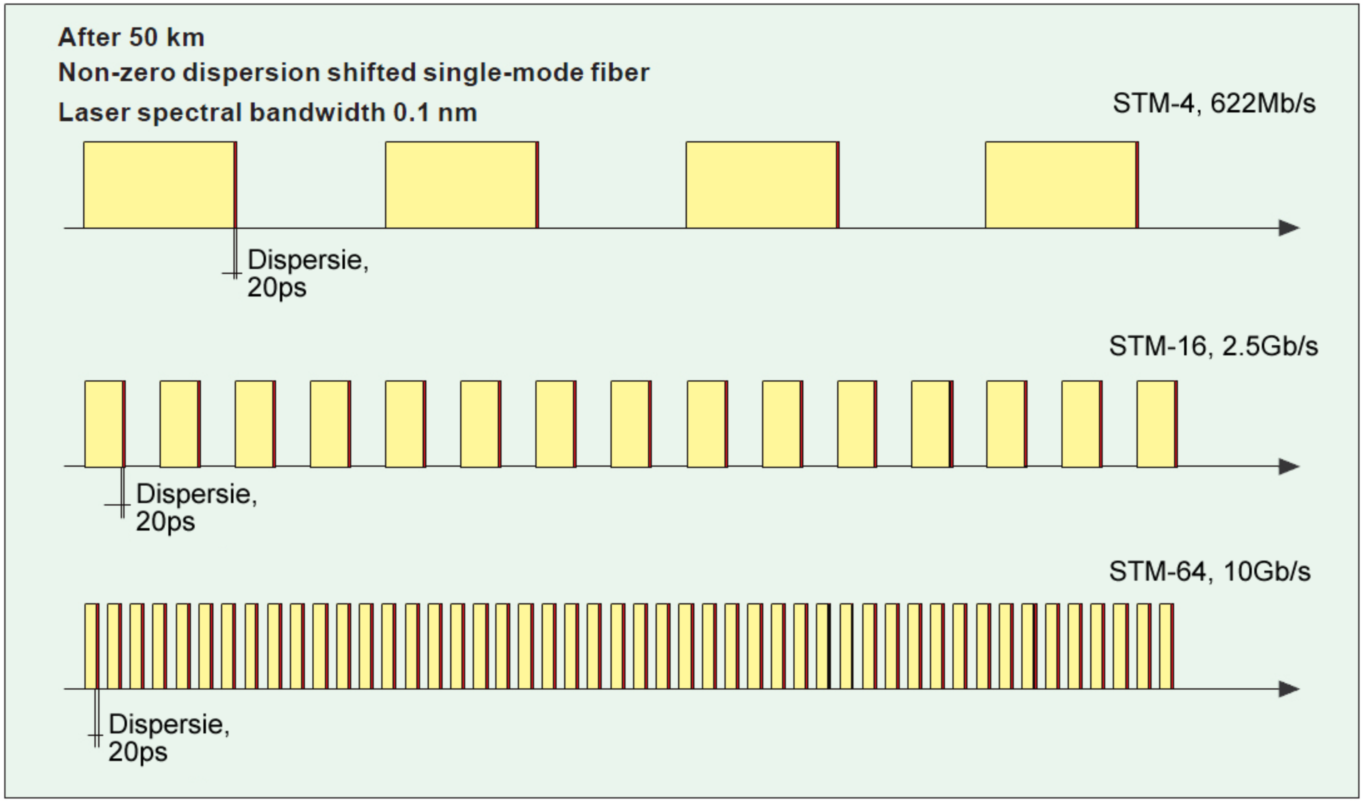
$$\Delta\tau_{cr} = D(\lambda)\cdot\Delta\lambda\cdot L$$

- Efectul **fibrei**
  - fibra cu dipersie deplasata: **4ps**/nm/km@1550
  - latimea spectrala a sursei Δλ=0.1nm
  - 50km

$$\Delta\tau_{cr} = D(\lambda)\cdot\Delta\lambda\cdot L$$

$$\Delta\tau_{cr} = 4\cdot 0.1\cdot 50\ ps = 20\ ps$$

$$[\Delta\tau_{cr}] = \frac{ps}{nm\cdot km}\cdot nm\cdot km = ps$$



20<100<400<1600

Dispersie exemplu – 5

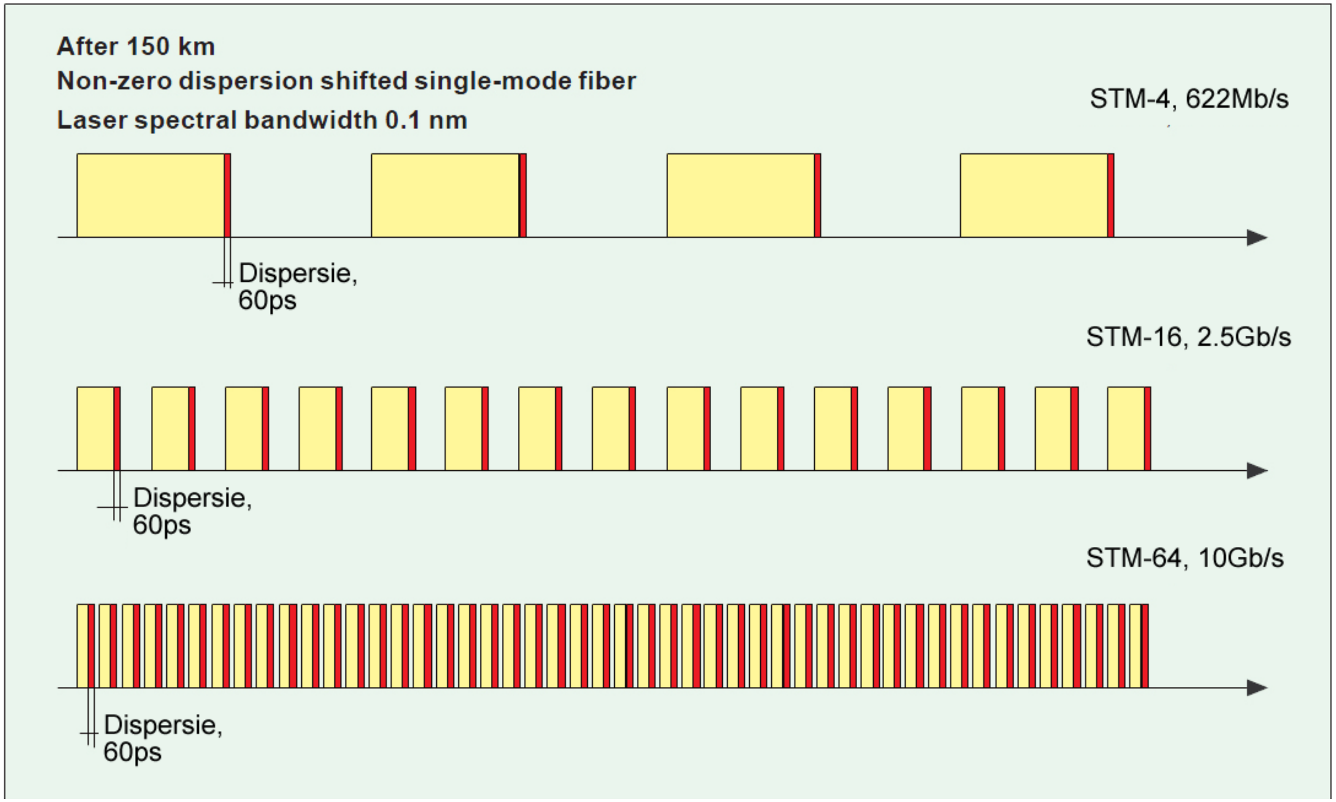
$$\Delta\tau_{cr} = D(\lambda)\cdot\Delta\lambda\cdot L$$

- Efectul **fibrei**
  - fibra cu dipersie deplasata: 4ps/nm/km@1550
  - latimea spectrala a sursei Δλ=0.1nm
  - 150km

$$\Delta\tau_{cr} = D(\lambda)\cdot\Delta\lambda\cdot L$$

$$\Delta\tau_{cr} = 4\cdot 0.1\cdot 150\ ps = 60\ ps$$

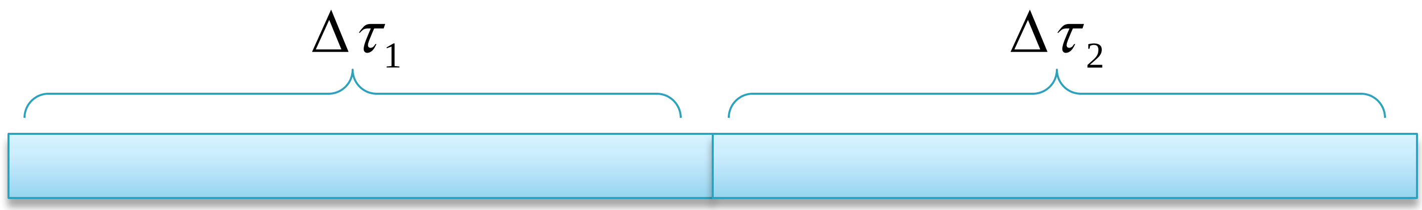
$$[\Delta\tau_{cr}] = \frac{ps}{nm\cdot km}\cdot nm\cdot km = ps$$



60<100<400<1600

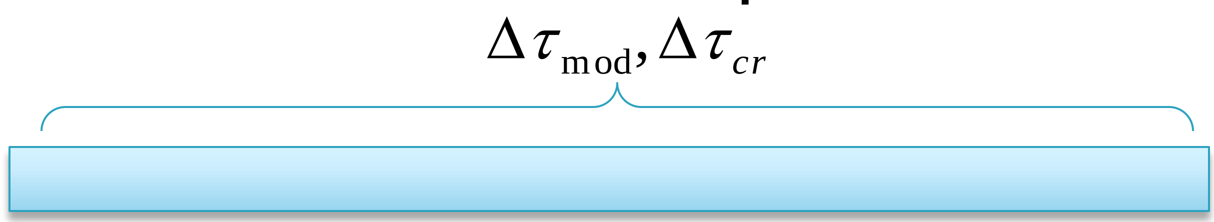
Sumarea efectelor

- efecte **succesive** se adună liniar



$$\Delta\tau_{tot} = \Delta\tau_1 + \Delta\tau_2$$

- efecte **simultane** se adună pătratic



$$\Delta\tau_{tot} = \sqrt{\Delta\tau_{cr}^2 + \Delta\tau_{\text{mod}}^2}$$

Dispersia

- Dispersia modala
  - salt de indice

$$\Delta\tau_{\text{mod}} \cong \frac{L \cdot n_2 \cdot \Delta}{2\sqrt{3} \cdot c} \approx \frac{L \cdot NA^2}{4\sqrt{3} \cdot c \cdot n_2}$$

  - indice gradat

$$\Delta\tau_{\text{mod}} \cong \frac{L \cdot n_2 \cdot \Delta^2}{4\sqrt{3} \cdot c} \cong \frac{L \cdot NA^4}{16\sqrt{3} \cdot c \cdot n_2^3}$$

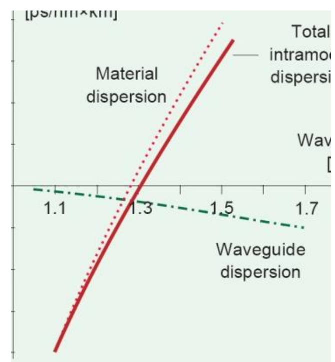
$$\Delta = 0.01 \div 0.02 << 1$$

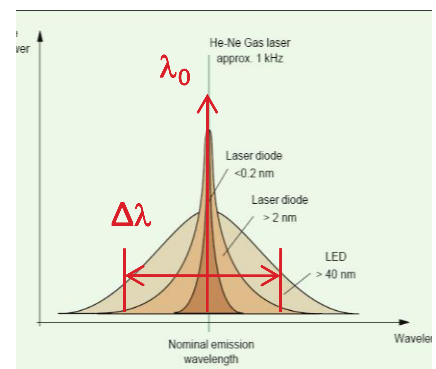
$$NA = 0.1 \div 0.2 < 1$$

- Dispersia cromatica

$$\Delta\tau_{cr} = D(\lambda) \cdot \Delta\lambda \cdot L$$

$$D(\lambda) = \frac{S_0}{4} \cdot \left(\lambda - \frac{\lambda_0^4}{\lambda^3} \right)$$





$$\Delta\tau_{tot} = \sqrt{\Delta\tau_{cr}^2 + \Delta\tau_{\text{mod}}^2}$$

Banda

- Dispersia totala

$$\Delta\tau_{tot} = \sqrt{\Delta\tau_{cr}^2 + \Delta\tau_{mod}^2} \quad \text{sau} \quad \Delta\tau_{tot} = \Delta\tau_1 + \Delta\tau_2$$

- Banda

$$B_{opt} \cong \frac{0.44}{\Delta\tau_{tot}[ns]} \quad [GHz]$$

- Banda optica la 3 dB corespunde unei benzi electrice la 6 dB
  - $P_{opt} \sim I; \quad P_{el} \sim I^2$ $\qquad$ $B_{opt} = \sqrt{2}B_{el}$
- Viteza legaturii

$$V[Gb/s] \cong 2 \cdot B_{el}[GHz]$$

Produs Banda · Distanta

$$\Delta\tau_{\text{mod}} \cong \frac{L \cdot n_2 \cdot \Delta}{2\sqrt{3} \cdot c} \approx \frac{L \cdot NA^2}{4\sqrt{3} \cdot c \cdot n_2}$$

$$\Delta\tau_{tot} = \sqrt{\Delta\tau_{cr}^2 + \Delta\tau_{\text{mod}}^2}$$

$$\Delta\tau_{cr} = D(\lambda) \cdot \Delta\lambda \cdot L$$

$$\Delta\tau_{tot} = const \cdot L$$

$$B_{opt} = \frac{0.44}{\Delta\tau_{tot}[ns]} \quad [GHz]$$

$$B_{opt} = \sqrt{2} B_{el}$$

$$V[Gb/s] \cong 2 \cdot B_{el}$$

$$V[Gb/s] \cong \frac{const}{L}$$

$$V[Gb/s] \cdot L[km] \cong const$$

Produs Banda X Distanta

$$\Delta\tau_{\mathrm{mod}} \sim L \qquad \Delta\tau_{cr} \sim L \qquad \Delta\tau_{tot} \sim L$$

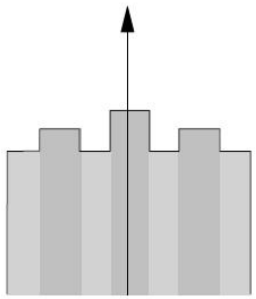
$$V[Gb/s] \sim B_{el}[GHz] \sim \frac{1}{\Delta\tau_{tot}} \sim \frac{1}{L[km]}$$

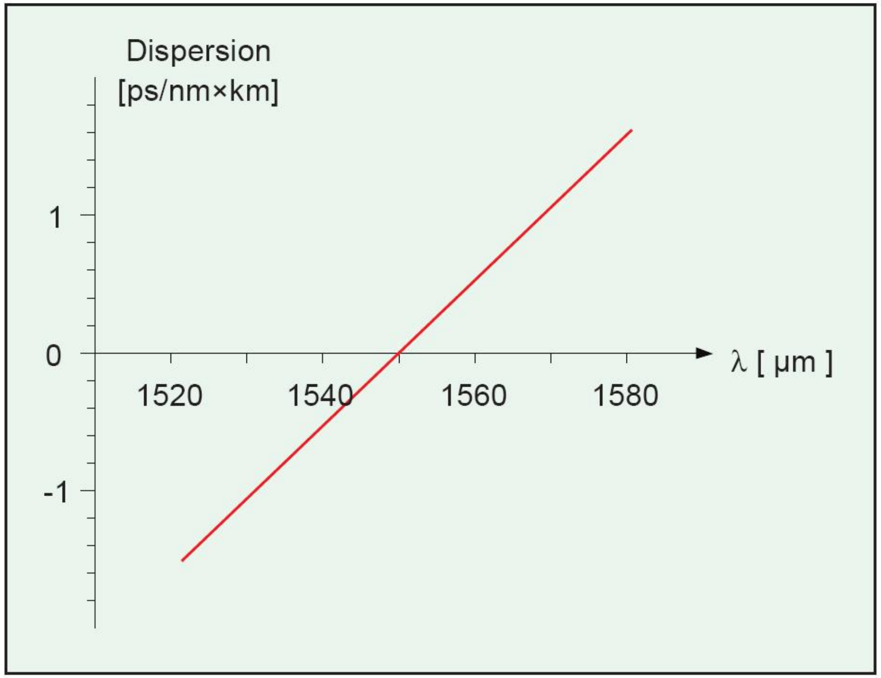
$$V[Gb/s] \times L[km] = \mathrm{ct.}$$

$$B_{el}[MHz] \times L[km] = \mathrm{ct.}$$

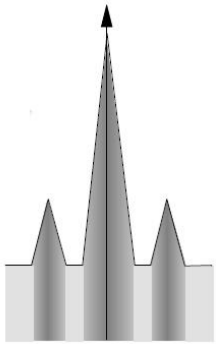
Dispersion shifted fibers

- Sticla are (nativ) dispersie cromatica 0 la 1310nm
- Atenuarea e mai mica la 1550 nm
- EDFA (Erbium doped fibre amplifiers) opereaza in banda 1550nm
- Sistemele WDM (Wavelength division Multiplexing) necestia banda larga amplificata

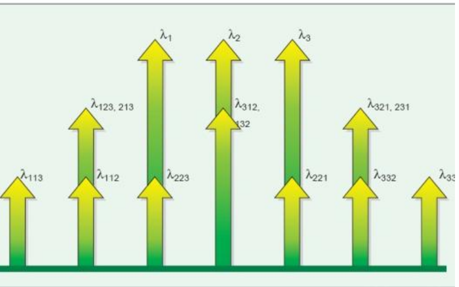


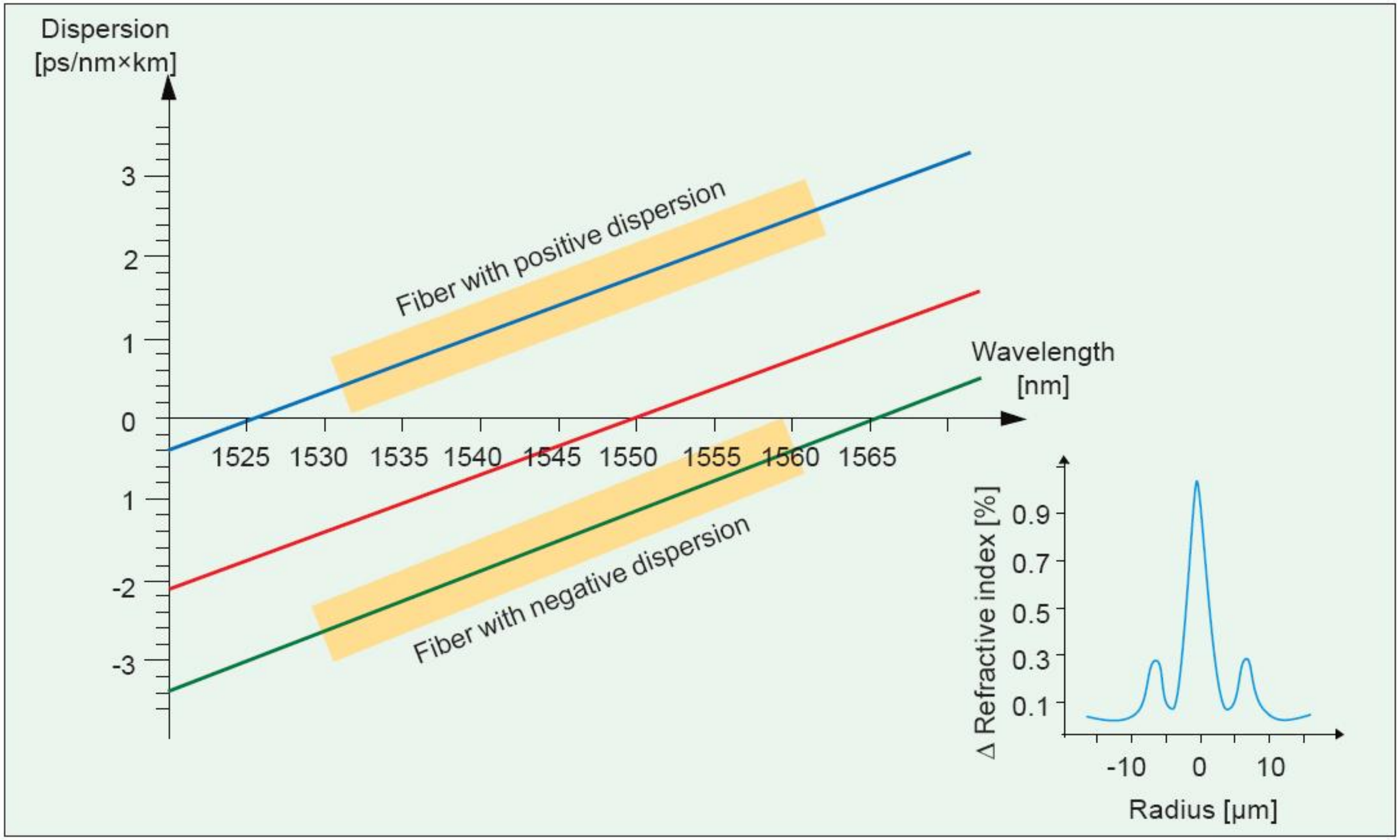


Non-zero Dispersion shifted fibers

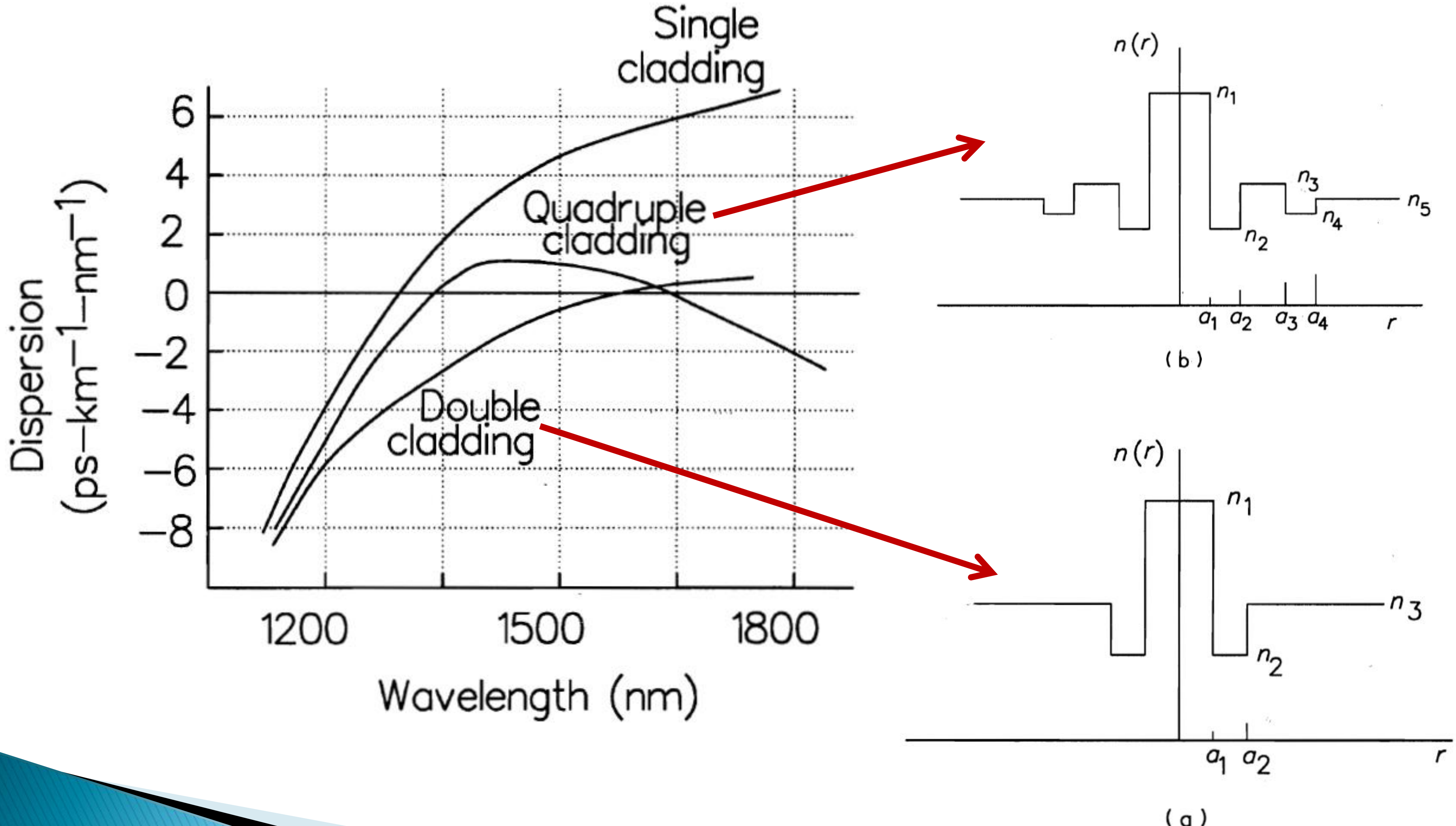


FWM

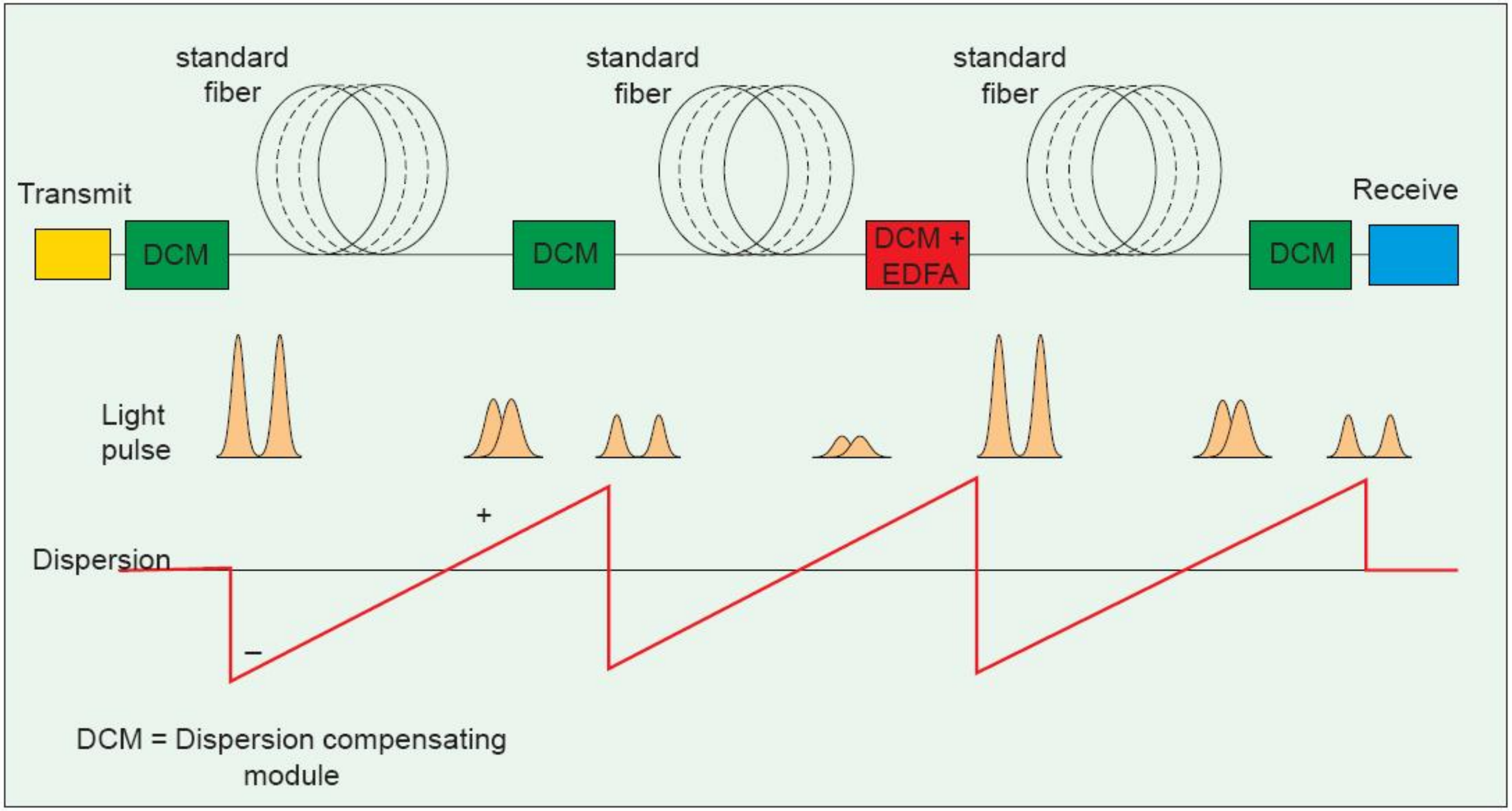




Dispersion shifted fibers



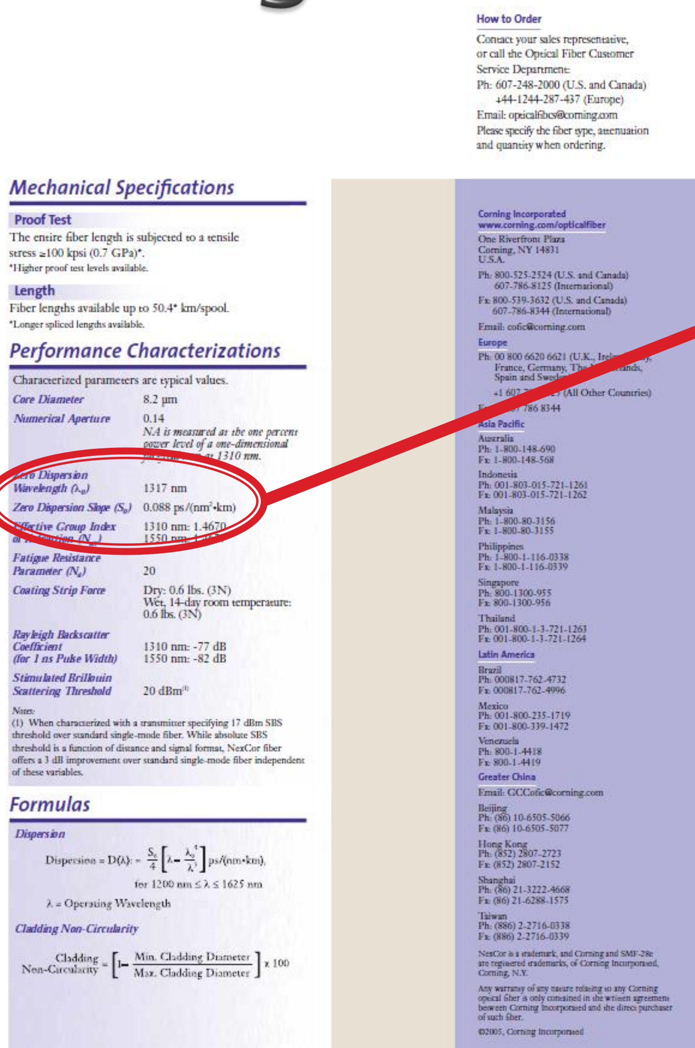
Fibra pentru compensarea dispersiei



- Dispersie: -100 ps/nm/km
- Atenuare 0.5 dB/km

Catalog – monomod

$$D(\lambda) = \frac{S_0}{4} \cdot \left(\lambda - \frac{\lambda_0^4}{\lambda^3} \right)$$



How to Order

Contact your sales representative, or call the Optical Fiber Customer Service Department:
Ph: 607-248-2000 (U.S. and Canada)
+44-1244-287-437 (Europe)
Email: opticalfiber@corning.com
Please specify the fiber type, attenuation and quantity when ordering.

Mechanical Specifications

Proof Test

The entire fiber length is subjected to a tensile stress ≥100 kpsi (0.7 GPa)*.
*Higher proof test levels available.

Length

Fiber lengths available up to 50.4* km/spool.
*Longer spliced lengths available.

Performance Characterizations

Characterized parameters are typical values.

Core Diameter	8.2 µm
Numerical Aperture	0.14 *NA is measured at the one percent power level of a one-dimensional far-field scan at 1310 nm.*
Zero Dispersion Wavelength (λ_0)	1317 nm
Zero Dispersion Slope (S_0)	0.088 ps/(nm²•km)
Effective Group Index of Refraction (N_{eff})	1310 nm: 1.4670 1550 nm: 1.4677
Fatigue Resistance Parameter (N_d)	20
Coating Strip Force	Dry: 0.6 lbs. (3N) Wet, 14-day room temperature: 0.6 lbs. (3N)
Rayleigh Backscatter Coefficient (for 1 ns Pulse Width)	1310 nm: -77 dB 1550 nm: -82 dB
Stimulated Brillouin Scattering Threshold	20 dBm(1)

Notes:
(1) When characterized with a transmitter specifying 17 dBm SBS threshold over standard single-mode fiber. While absolute SBS threshold is a function of distance and signal format, NexCor fiber offers a 3 dB improvement over standard single-mode fiber independent of these variables.

Formulas

Dispersion

$$\text{Dispersion} = D(\lambda) = \frac{S_0}{4}\left[\lambda - \frac{\lambda_0^4}{\lambda^3}\right] \text{ps/(nm•km)},$$

for $1200 \text{ nm} \le \lambda \le 1625 \text{ nm}$

λ = Operating Wavelength

Cladding Non-Circularity

$$\text{Cladding Non-Circularity} = \left[1 - \frac{\text{Min. Cladding Diameter}}{\text{Max. Cladding Diameter}}\right] \times 100$$

Corning Incorporated
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Taiwan
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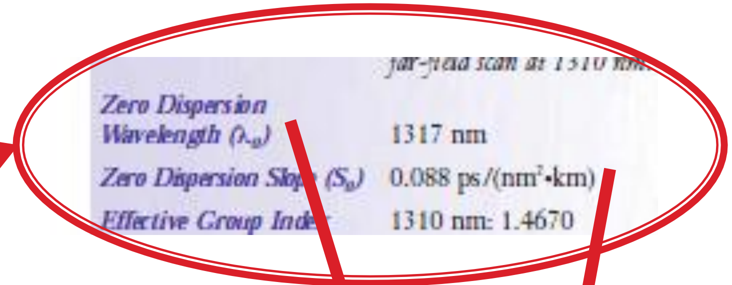
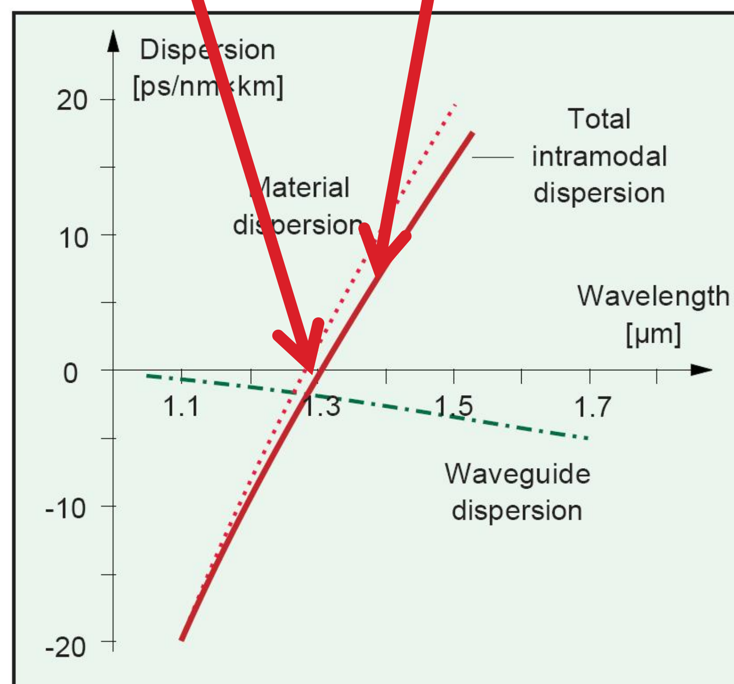




Catalog – multimod

$$D(\lambda) = \frac{S_0}{4} \cdot \left(\lambda - \frac{\lambda_0^4}{\lambda^3} \right)$$

+

Bandwidth

Standard Bandwidth Cells
850/1300 nm (MHz•km)
400/400
400/600
400/1200
500/500
600/600
600/1000

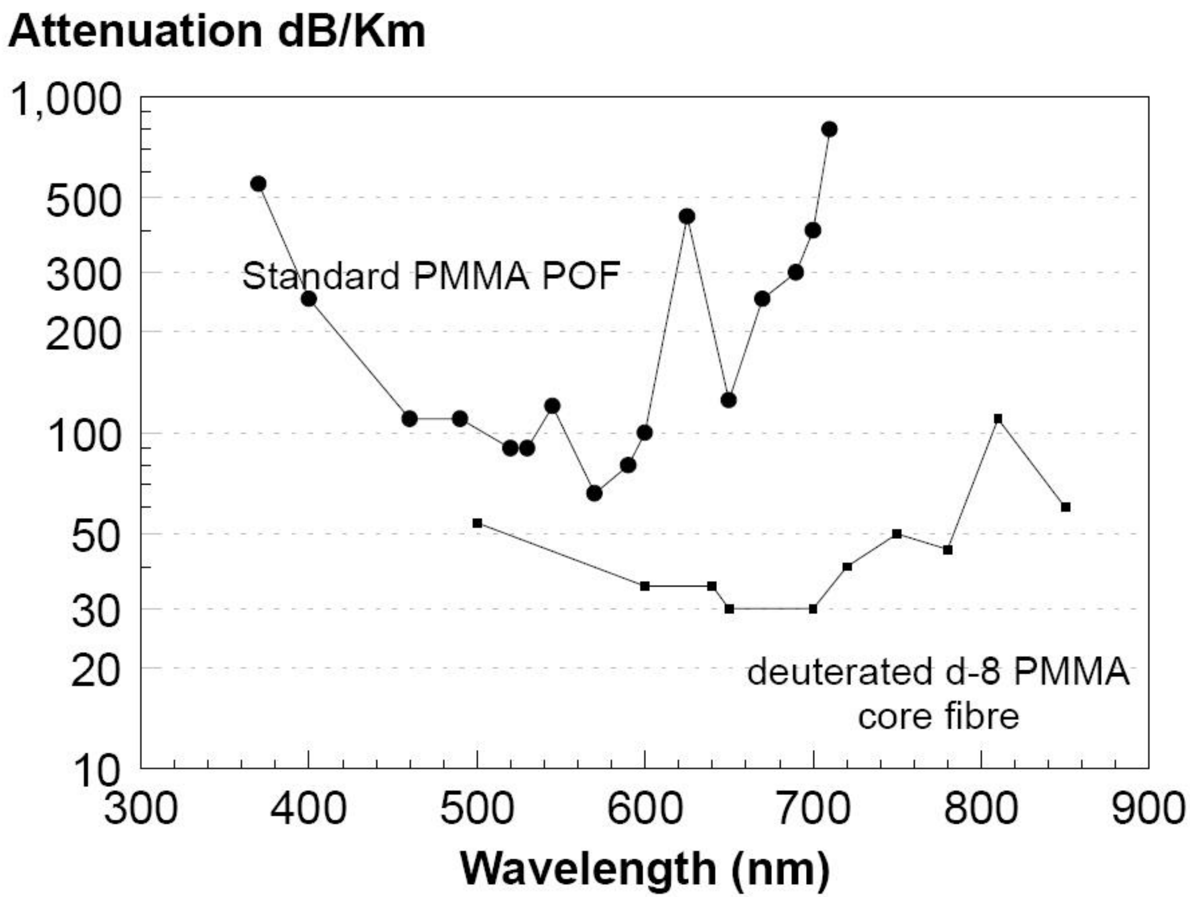
Other bandwidth cells available upon request.

Fibra standard ITU G.652

- Diametru teaca = 125 μm
- MFD = 9÷10 μm la 1300 nm
- λ_C = 1100÷1280 nm
- Pierderi de curbura (la 1550 nm) mai mici de 1 dB pentru 100 spire de fibra rulata pe un mosor cu 7.5 cm diametru
- Dispersia in banda 1300 nm (1285–1330 nm) mai mica de 3.5 ps/nm/km. La 1550 nm dispersia trebuie sa fie mai mica de 20 ps/nm/km
- Viteza de variatie a dispersiei (panta dispersiei S_0) mai mica de 0.095 ps/nm^2/km

ITU (International Telecommunication Union) is the United Nations specialized agency for information and communication technologies – ICTs

Fibra optica din plastic (POF)



- Atenuare 180 dB/km
- NA = 0.3
- Diametru 1 mm
- Banda 125MHz (100m)

Contact

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