

# Optoelectronică

Curs 12  
2022/2023

# Disciplina 2022/2023

- ▶ 2C/1L Optoelectronicaă **OPTO**
- ▶ **Minim 7 prezente curs + laborator**
- ▶ Curs – conf. Radu Damian
  - an IV μE
  - Joi 08(:10)–10:00, C1
  - E – 70% din nota (50%+20%)
    - **20% test (VP) la curs**, saptamana 4–6?
  - probleme + (2p prez. curs)
  - **toate materialele permise**
- ▶ Laborator – sl. Daniel Matasaru
  - an IV μE
    - Luni 18–20, Miercuri 11–15 par
    - Max. 7 prezente
  - L – 30% din nota (+Caiet de laborator)

# Cuprins

- ▶ **Lumina ca undă electromagnetică\*** (ecuațiile lui Maxwell, ecuația undelor, parametrii de propagare)
- ▶ **Elemente de fotometrie și radiometrie\*** (mărimi energetice/luminoase)
- ▶ **Fibra optică** (realizare, principiu de funcționare, atenuare, dispersie, banda de frecvență)
- ▶ **Cabluri optice** (tehnologie, conectori, lipire – splice)
- ▶ **Proiectare sistemică a legăturii pe fibra optică** (bandă de frecvență, balanță puterilor)
- ▶ **Emitătoare optice** (LED și dioda laser – realizare fizică și funcționare)
- ▶ **Receptoare optice** (dioda PIN, dioda cu avalanșă – realizare fizică și funcționare)
- ▶ **Amplificatoare transimpedanță** (parametri, scheme tipice, TIA în buclă deschisă, cu reacție, diferențiale, control automat al câștigului)
- ▶ **Realizarea circuitelor pentru controlul emitătoarelor optice** (parametri, scheme tipice, controlul puterii, multiplexoare)
- ▶ **Dispozitive de captare a energiei solare** (principiu de funcționare, utilizare, proiectare )

\* – VP

# Bibliografie

- ▶ <http://rf-opto.eti.tuiasi.ro>
- ▶ Irinel Casian-Botez, "Structuri Optoelectronice", Ed. "CANOVA", Iasi 2001, ISBN 973-96099-2-9
- ▶ Behzad Razavi – Design of Integrated Circuits for Optical Communications, Mc Graw Hill
- ▶ John Powers – An Introduction to Fiber Optic Systems
- ▶ IBM – Understanding Optical Communications: on-line <http://www.redbooks.ibm.com>
- ▶ Radu Damian, I Casian, D Matăsaru – „Comunicatii Optice” , Indrumar de laborator, 2005
- ▶ MIT Course – Fundamentals of Photovoltaics, <https://ocw.mit.edu>

# Bonus

**Disciplina:** Optoelectronica, structuri, tehnologii, circuite

**An:** 2015/2016

Bonus-uri care se aplica la nota de la teza obtinute prin:

- prezenta la curs (0.5p / 3pr)
- 3 miniteste aplicate la curs (max. 3 X 1.5p)
- contributie la site rf-opto (foto <C5=1p, >C5=0.5p)

| Nr. | Student                             | Grupa | Prezente curs | Bonus prezenta | Bonus foto | Bonus T1 | Bonus T2 | Bonus T3 | Total Bonus | Obs. |
|-----|-------------------------------------|-------|---------------|----------------|------------|----------|----------|----------|-------------|------|
| 1   | <a href="#">CIOLPAN OCTAVIAN</a>    | 5306  | 3             | 0.5            |            |          |          |          | 0.5         | -    |
| 2   | <a href="#">NITA COSTEL-CATALIN</a> | 5307  | 4             | 0.5            | 1          |          |          |          | 1.5         | -    |
| 3   | <a href="#">BARON BOGDAN-IONUT</a>  | 5405  | 12            | 2              | 1          | 0.5      |          | 0.75     | 4.25        | -    |

## Prezenta

[Curs](#)  
[Laborator](#)

## Liste

[Studenti care nu pot intra in examen](#)  
[Bonus-uri acumulate](#)

- **Minim 7 prezente**
- **0.5p/3(2)prez**
- **3 teste**
- **foto <C3/<C5**

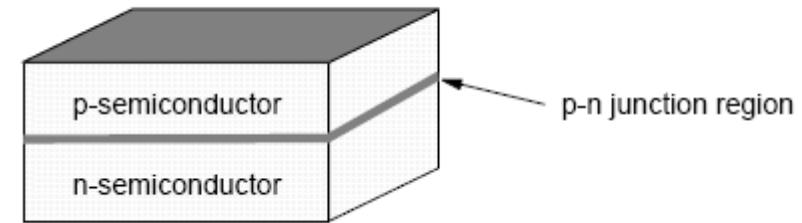
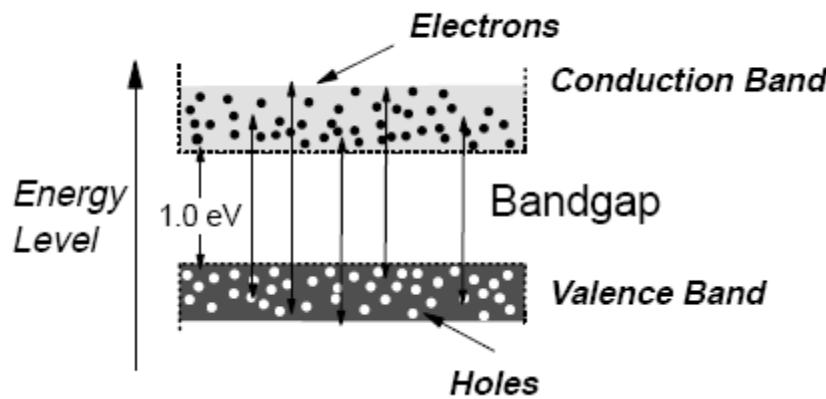
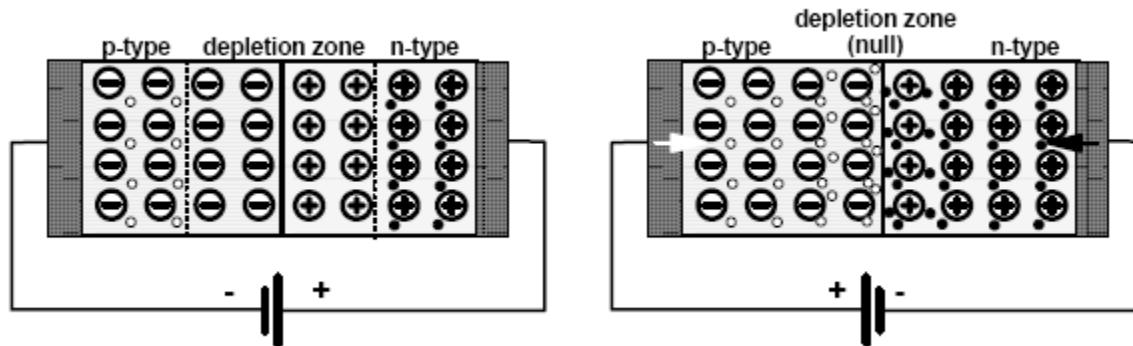
# LED

Dioda electroluminescentă  
Capitolul 7

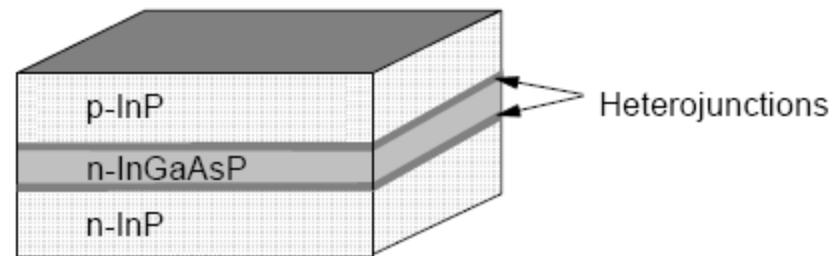
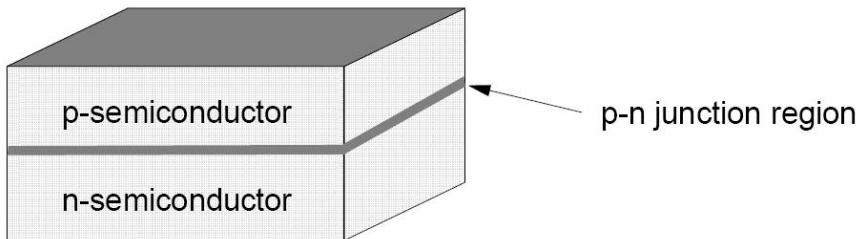
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- ▶ Dispozitive de captare a energiei solare (principiu de funcționare, utilizare, proiectare )

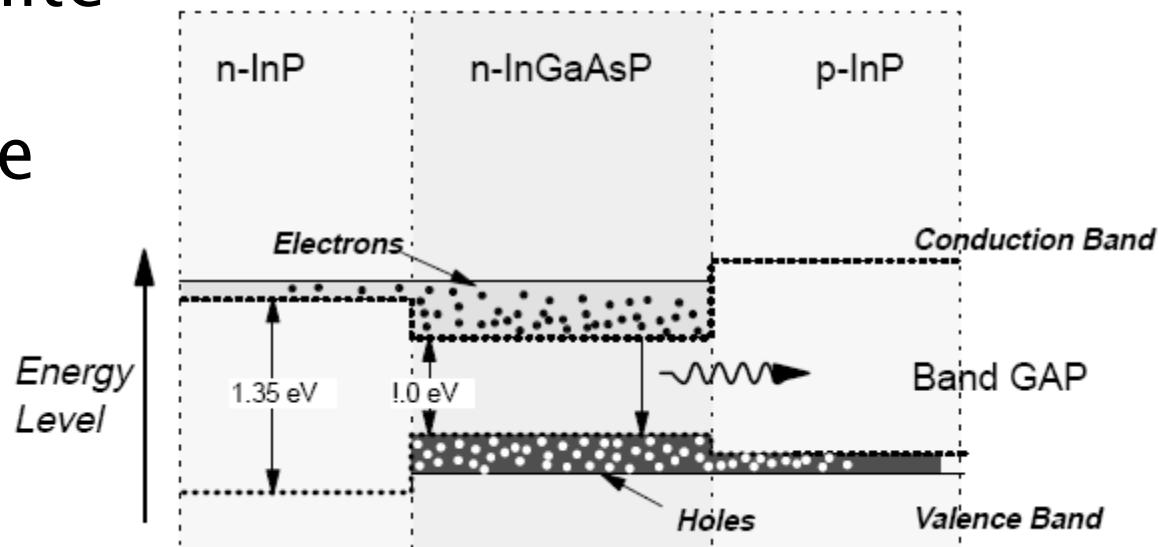
# LED – Principiul de operare



# LED cu heterojunctiuni – principiu



- ▶ Structura de nivele energetice permite capturarea purtatorilor intre cele doua heterojonctiuni

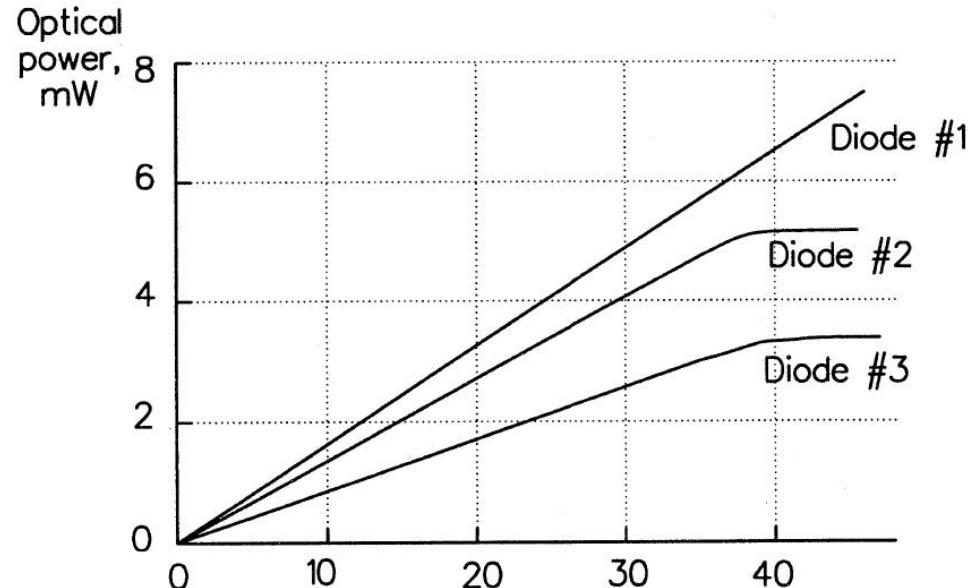


# Caracteristica de raspuns a LED-urilor

- ▶ Caracteristica putere optica emisa functie de curentul direct prin LED este liniara la nivele mici ale curentului.
- ▶ Nu exista curent de prag
- ▶ La nivele foarte mari puterea optica se satureaza
- ▶ Rezonabilitatea

$$r = \frac{P_o}{I} \quad \left[ \frac{W}{A} \right]$$

- ▶ Tipic  $r=50\mu W/mA$



# Diода Laser

Capitolul 8

# Cuprins

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# Caracteristici dioda laser

## ▶ Avantaje

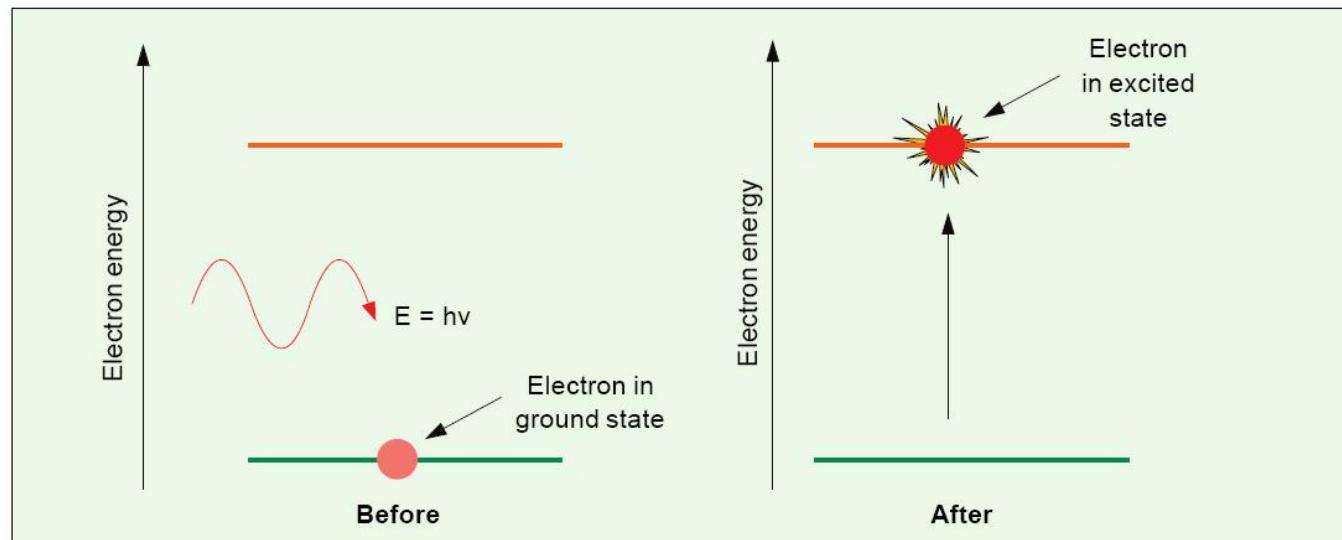
- Putere optica ridicata (50mW functionare continua, 4W functionare in impulsuri)
- Precizie ridicata a controlului (impulsuri cu latimea de ordinul fs – femtosecunde) – viteza mare de lucru
- Spectru ingust, teoretic LASER ofera o singura linie spectrala
- Lumina coerenta si directiva (~80% poate fi cuplata in fibra)

## ▶ Dezavantaje

- Cost (dispozitiv si circuit de comanda: controlul puterii si al temperaturii)
- Durata de viata
- Senzitivitate crescuta cu temperatura
- Modulatie analogica dificila (de obicei cu dispozitive externe)
- Lungime de unda fixa

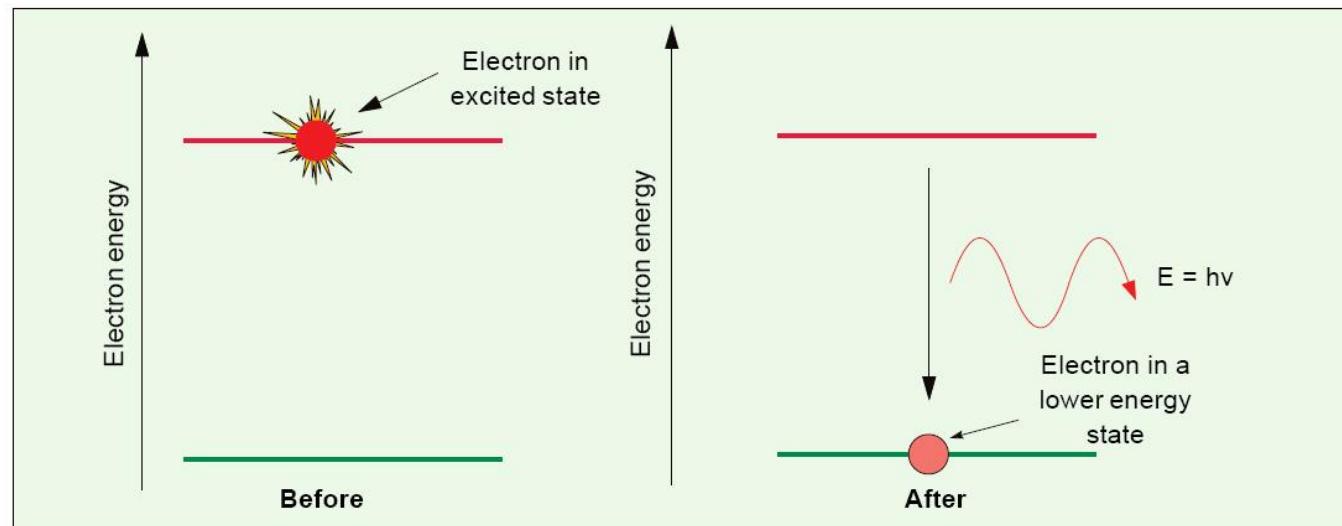
# Diода LASER – Prințipiu de operare

- ▶ LASER = Light Amplification by the Stimulated Emission of Radiation = Amplificarea Luminii prin Emisie Stimulata
- ▶ Un foton incident poate cauza prin absorbtie tranzitia unui electron pe un nivel energetic superior



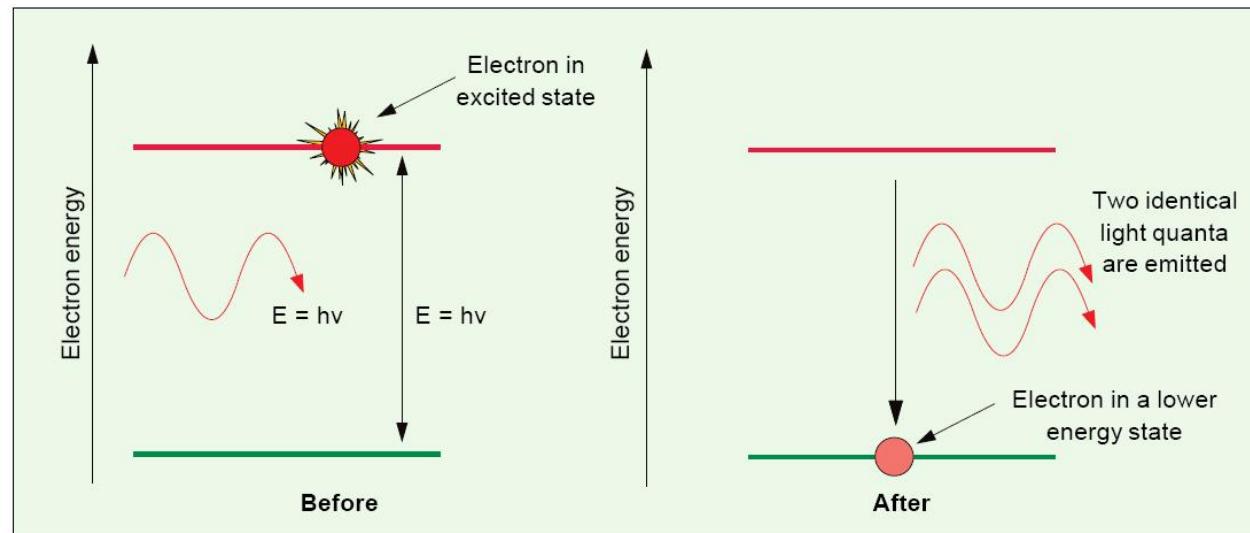
# Diода LASER – Principiu de operare

- ▶ Emisia spontana – electronul trece in starea energetica de echilibru emitand un foton
- ▶ Trecerea se realizeaza prin recombinarea unei perechi electron–gol
- ▶ Directia si faza radiatiei emise sunt aleatoare



# Diода LASER – Prințipiu de operare

- ▶ Emisia stimulată – un foton incident cu energie corespunzătoare poate stimula emisia unui alt doilea foton **fără a fi absorbit**
- ▶ Noul foton are aceeași direcție și fază cu fotonul incident, Lumina rezultată e coerentă



# Caracteristici curent tensiune

- ▶ Amorsarea emisiei stimulate necesita pomparea unei anumite cantitati de energie – curent de prag

$I < I_{th}$  regim LED

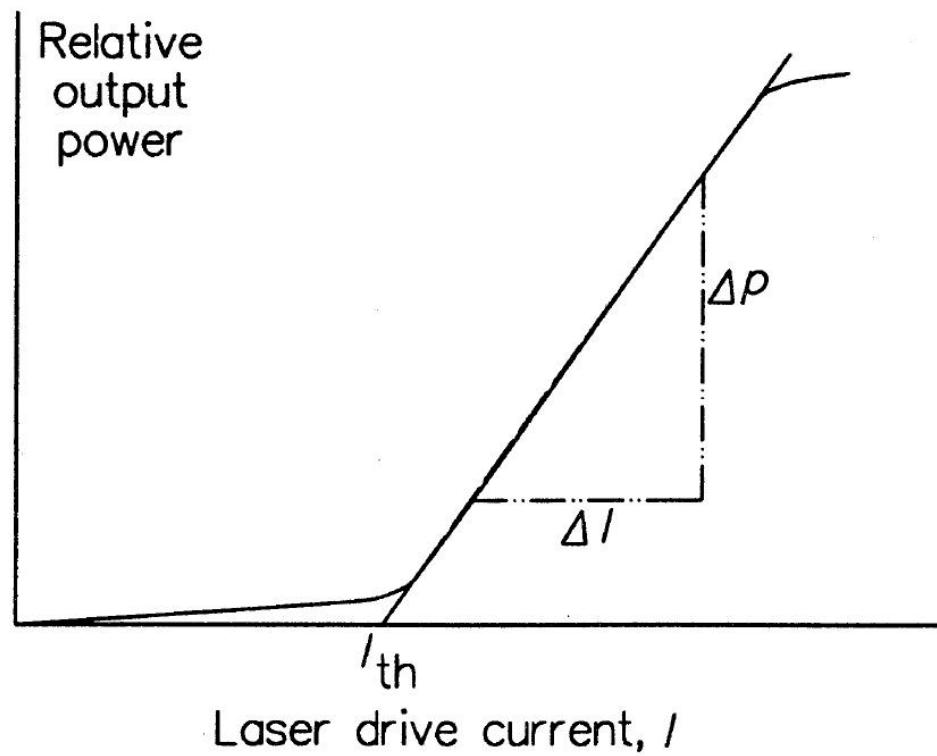
ineficient!,  $P_o \approx 0$

$I > I_{th}$  regim LASER

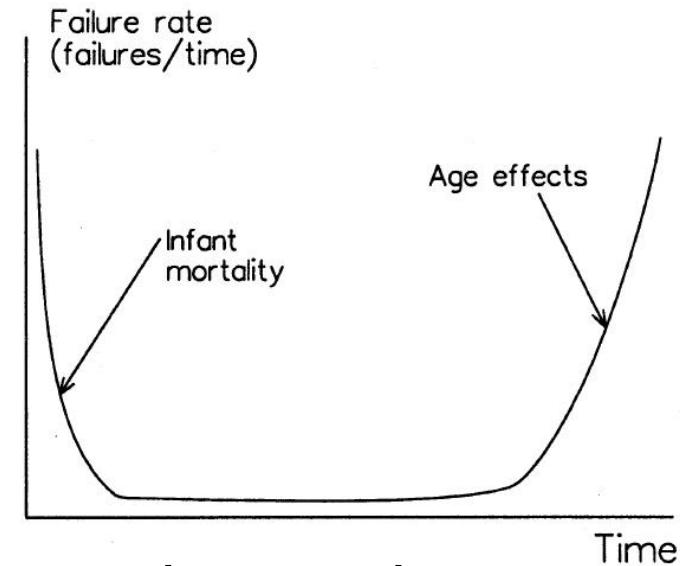
$$r = \frac{\Delta P_o}{\Delta I} \left[ \frac{W}{A} \right]$$

$$P_o = r \cdot (I - I_{th})$$

Apare saturare la nivele mari de curent



# Degradare in timp



- ▶ Cresterea curentului duce la scaderea duratei de viata
$$\tau_m \sim J^{-n}$$
  - $n = 1.5 \div 2$  (empiric)
  - dublarea curentului duce la scaderea de 3–4 ori a duratei de viata
- ▶ Cresterea temperaturii duce la scaderea duratei de viata

$$\tau_m \sim e^{E/kT}$$

- $E = 0.3 \div 0.95 \text{ eV}$  (valoarea tipica in teste  $0.7 \text{ eV}$ )
- cresterea temperaturii cu 10 grade injumatatestă durata de viata

# Parametri

- ▶ Coerenta radiatiei emise
  - LED:  $t_c \approx 0.5\text{ps}$ ,  $L_c \approx 15\mu\text{m}$
  - LASER :  $t_c \approx 0.5\text{ns}$ ,  $L_c \approx 15\text{cm}$

$$L_c = c \cdot t_c = \frac{\lambda_0^2}{\Delta\lambda}$$

- ▶ Stabilitatea frecventei
  - detectie necoerenta (modulatie in amplitudine)
  - mai ales in sistemele multicanal
- ▶ Timpul de raspuns
- ▶ Viteza, interval de reglaj

# Eficienta

- ▶ eficienta de conversie electro-optic  
(randament)

$$\eta = \frac{P_{out}(\text{optic})}{P_{in}(\text{electric})} = \frac{P_o}{V_f \cdot I_f} \approx \frac{r \cdot (I_f - I_{th})}{V_f \cdot I_f}$$

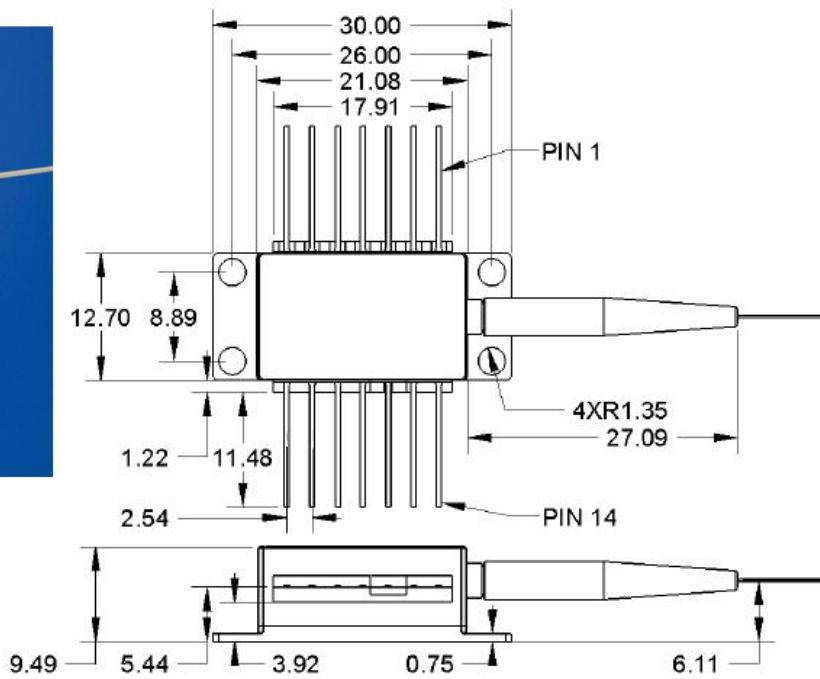
- ▶ tipic, randamente sub 10% sunt intalnite
- ▶ eficienta cuantica
  - interna
  - externa

$$\eta = \frac{n_f}{n_e} \quad \eta = \frac{\Delta P/h\nu}{\Delta I/e} = r \cdot \frac{e}{h\nu}$$

# 1550nm DFB Laser

## Mechanical Drawing

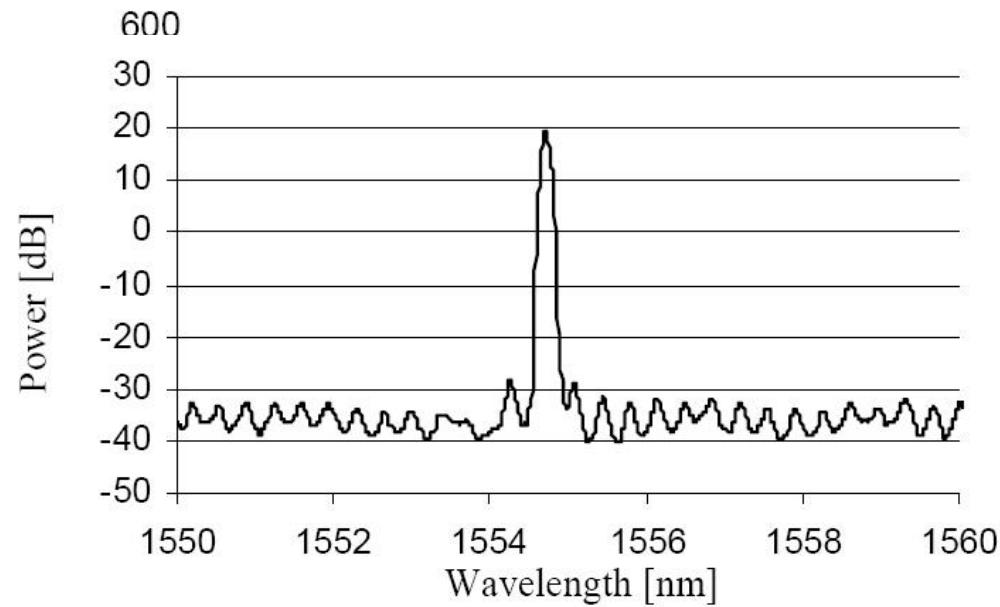
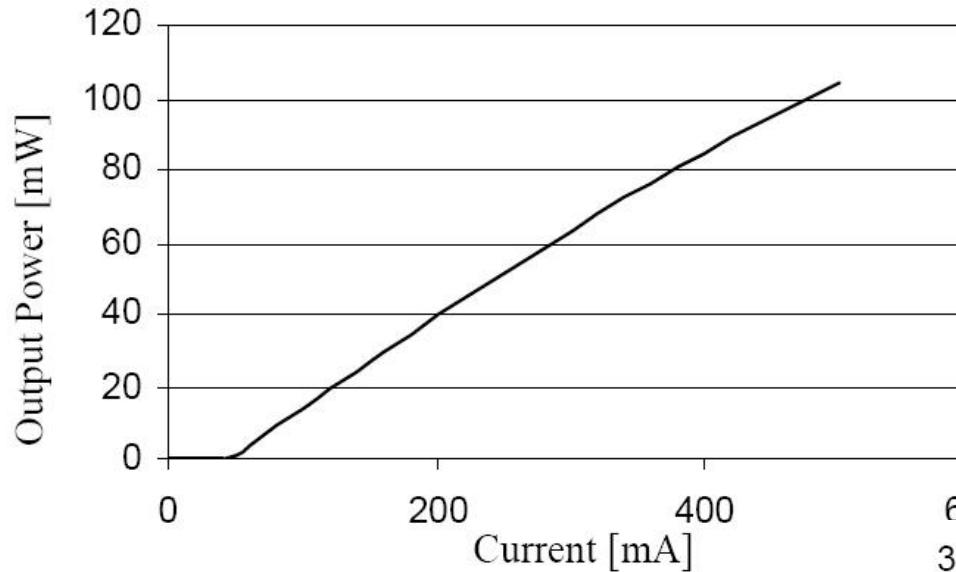
All units in mm



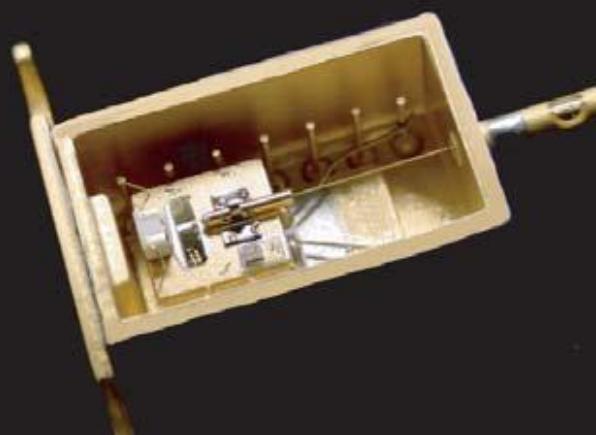
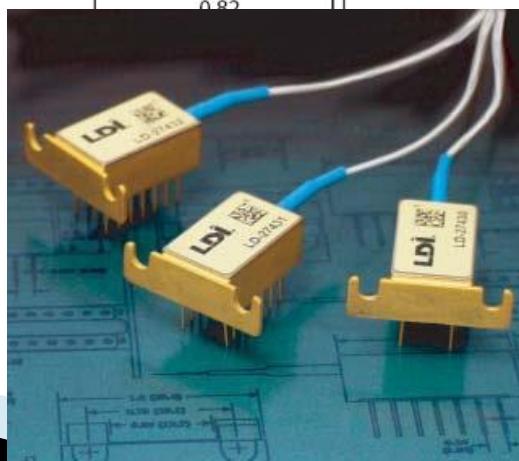
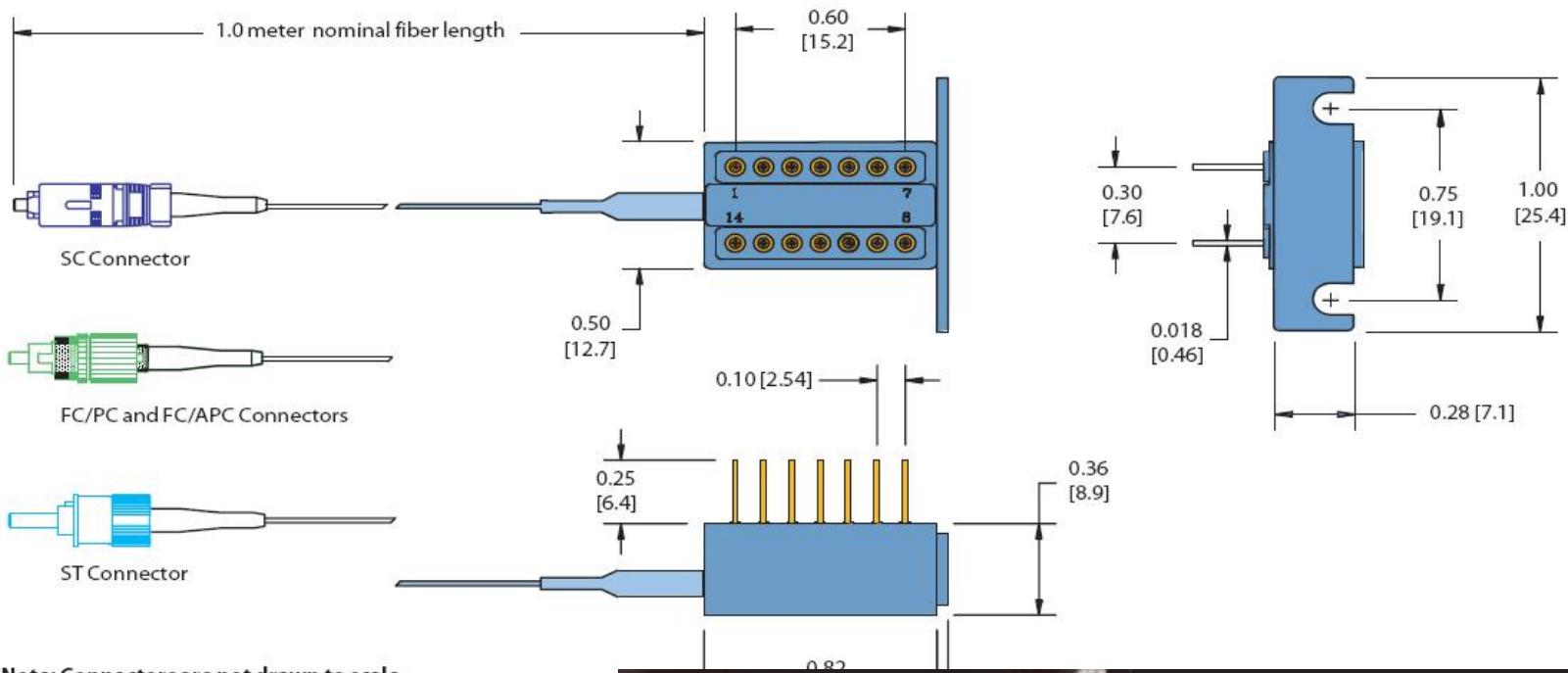
## Pin out

| Pin | Description                |
|-----|----------------------------|
| 1   | Thermistor                 |
| 2   | Thermistor                 |
| 3   | Laser Cathode (Bias)       |
| 4   | Monitor PD Anode           |
| 5   | Monitor PD Cathode         |
| 6   | TEC +                      |
| 7   | TEC -                      |
| 8   | Case GND, Laser Anode      |
| 9   | Case GND, Laser Anode      |
| 10  | Case GND, Laser Anode      |
| 11  | Case GND, Laser Anode      |
| 12  | Laser Cathode (modulation) |
| 13  | Case GND, Laser Anode      |
| 14  | Case GND, Laser Anode      |

# 1550nm DFB Laser

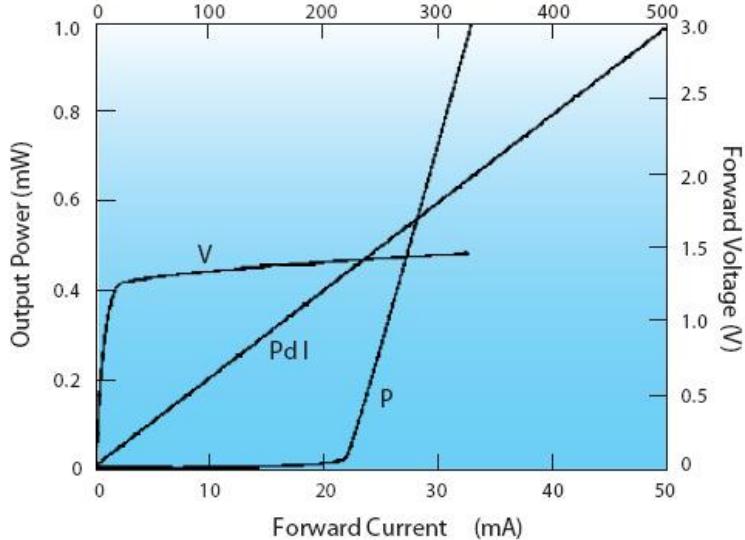


# 1550nm MQW Laser

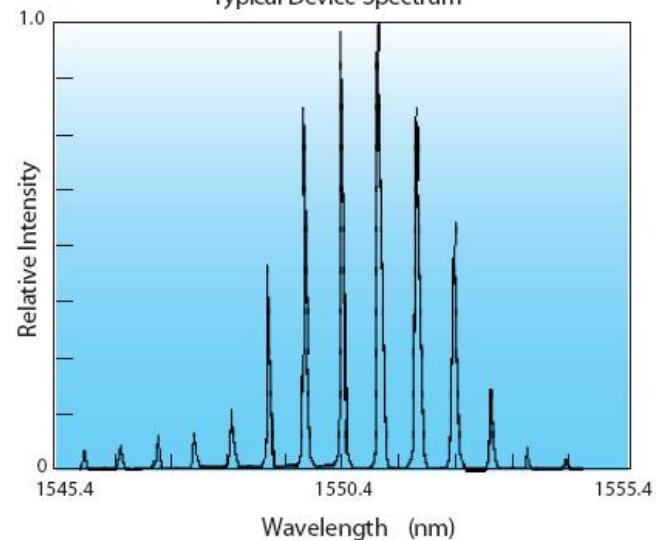


# 1550nm MQW Laser

Typical Laser Characteristics  
Photodiode Current ( $\mu$ A)

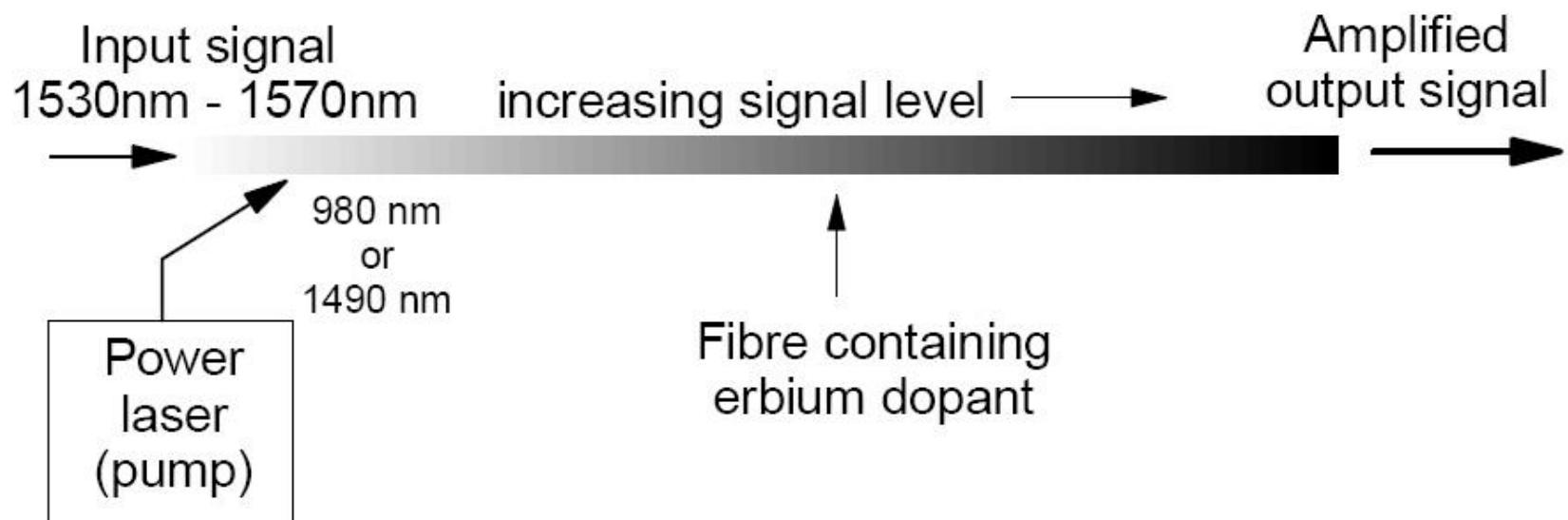


Typical Device Spectrum

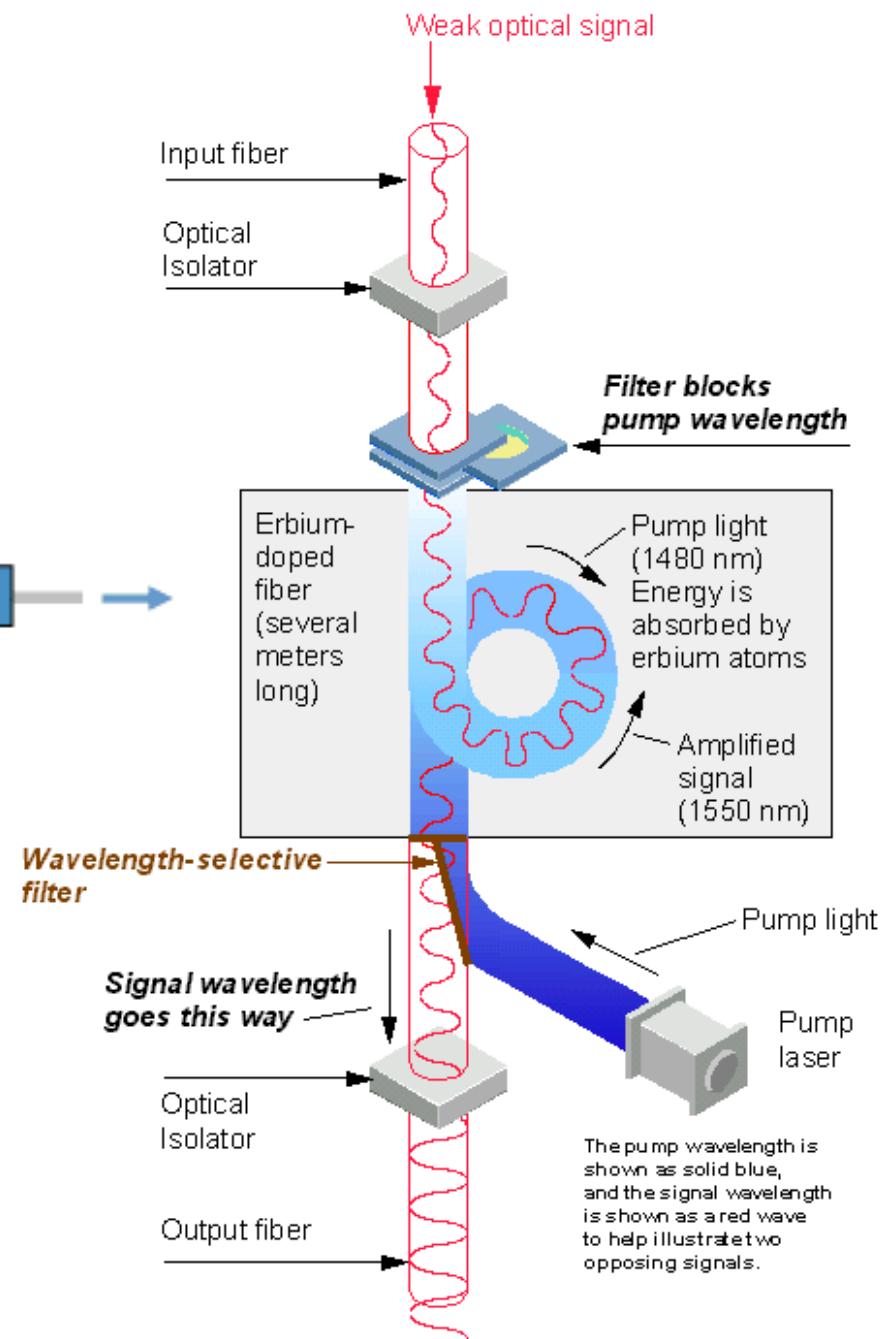
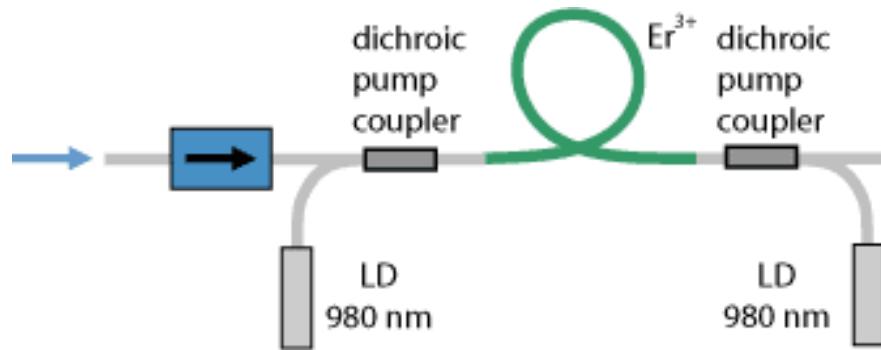


# EDFA

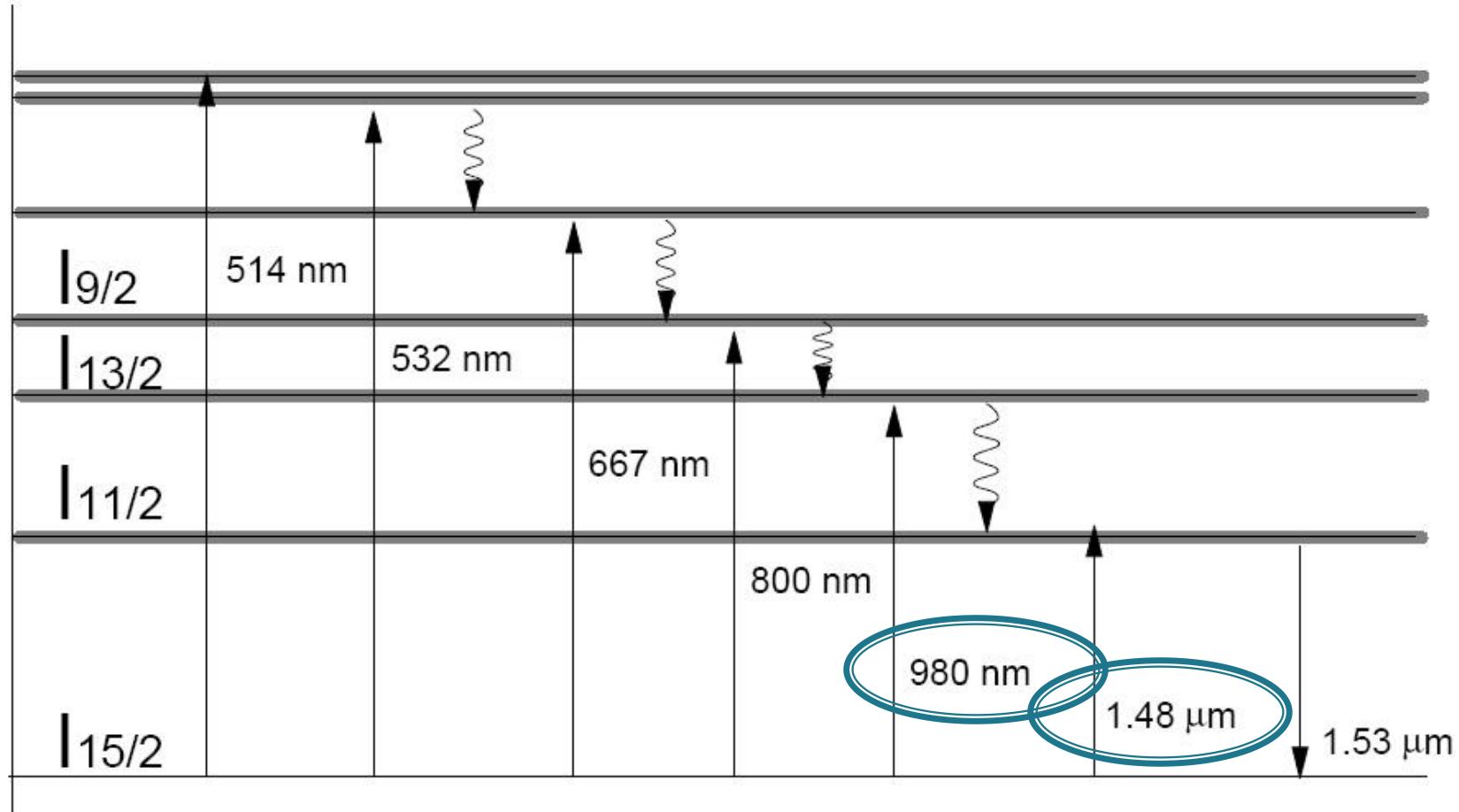
## ► Erbium Dopped Fiber Amplifier



# EDFA

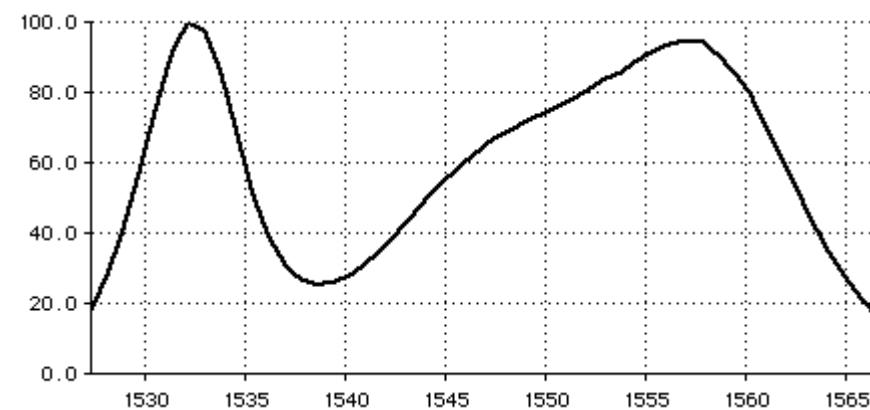
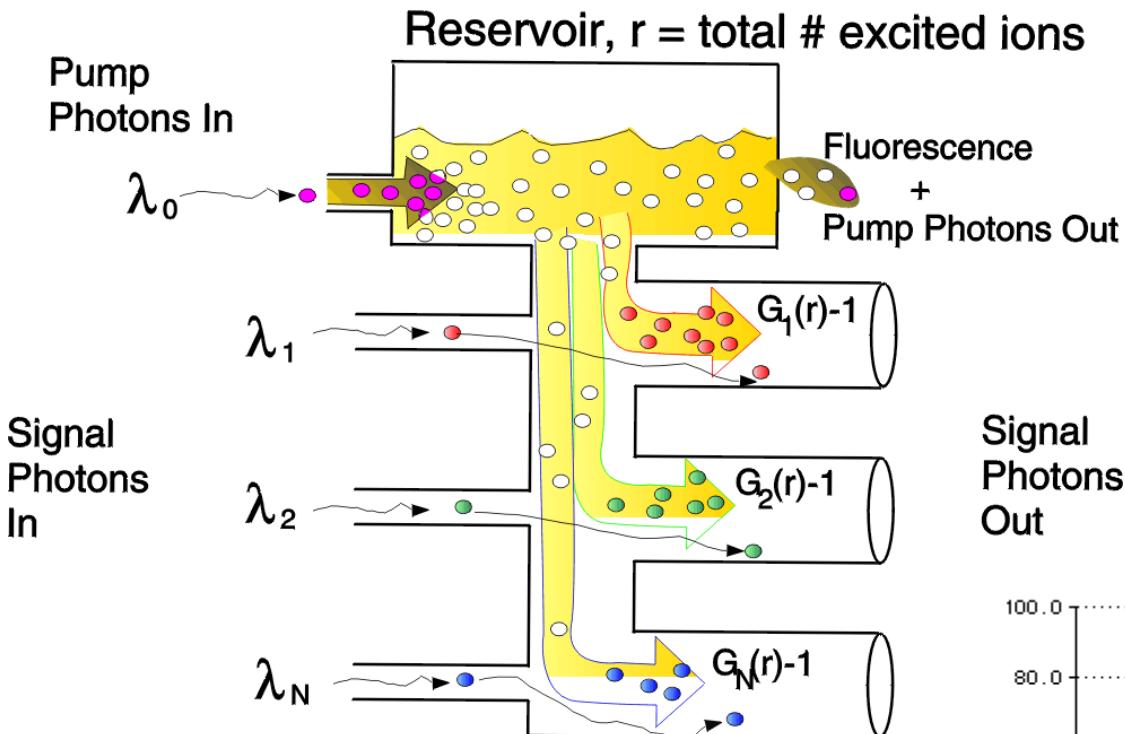


# EDFA



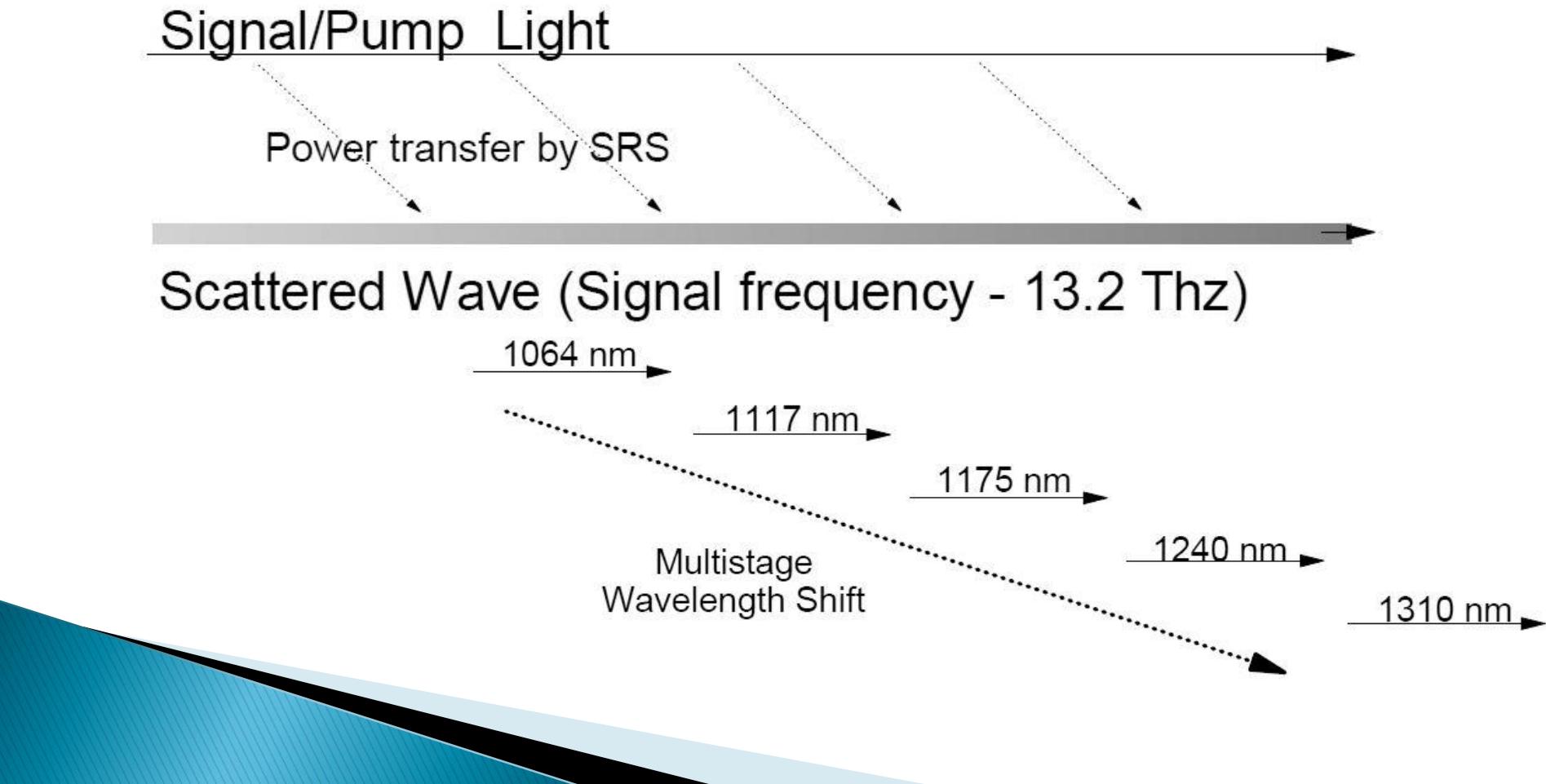
# EDFA

## How to think of an EDFA

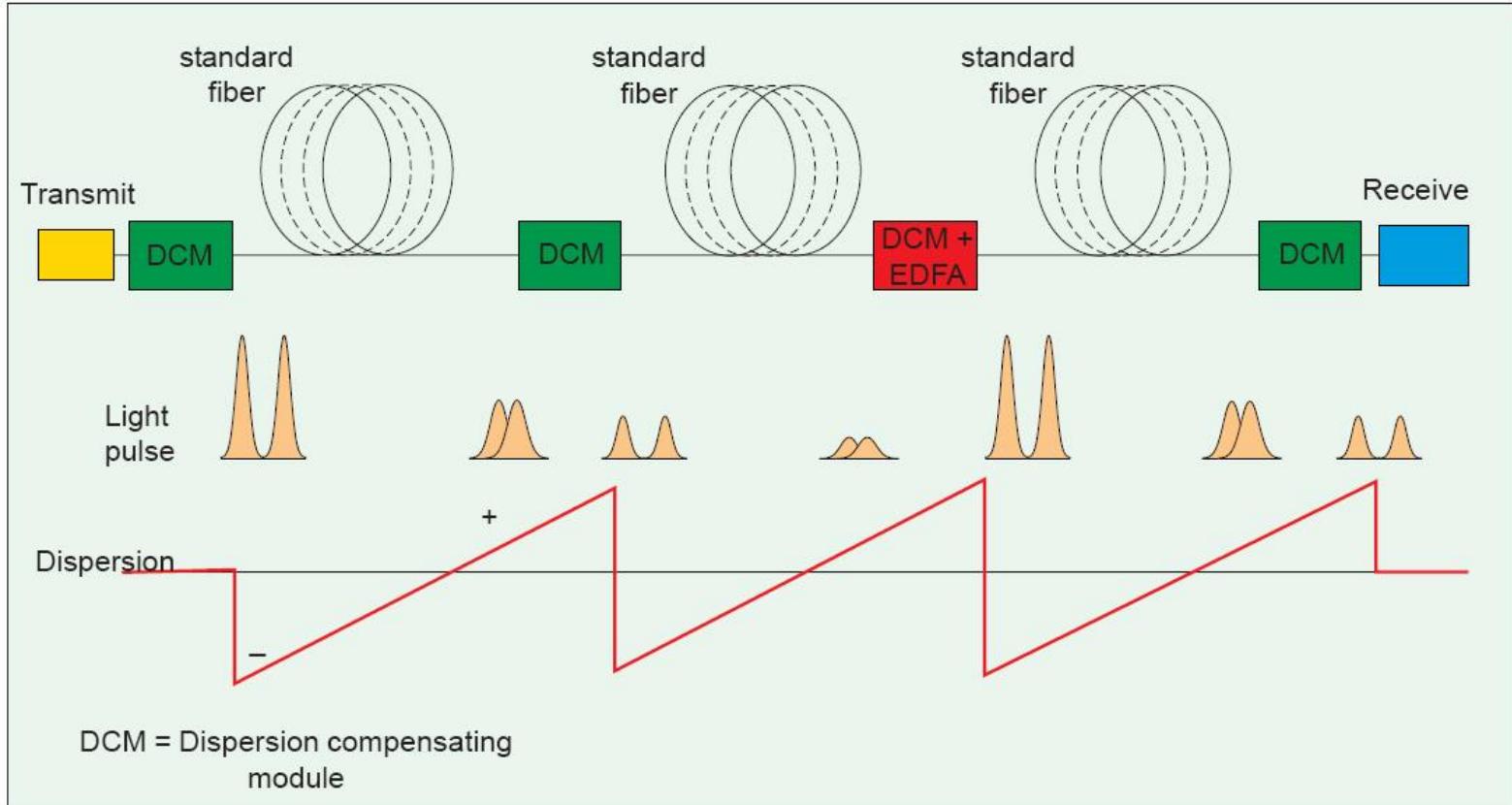


# Amplificator cu efect Raman

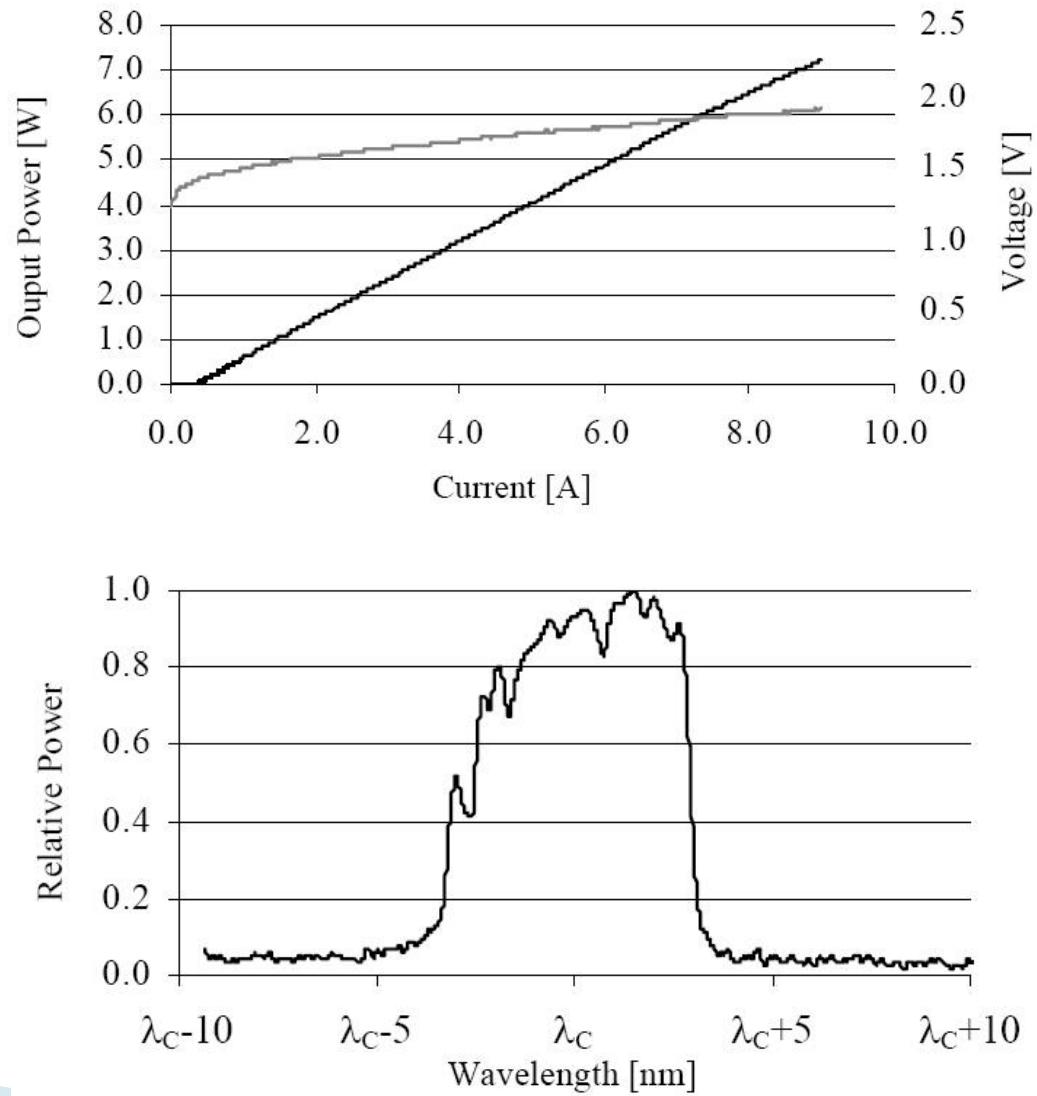
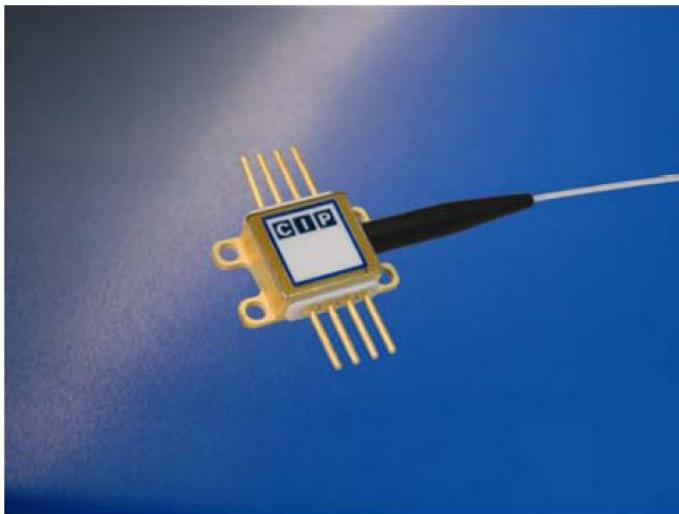
## ▶ Bazat pe efect Raman



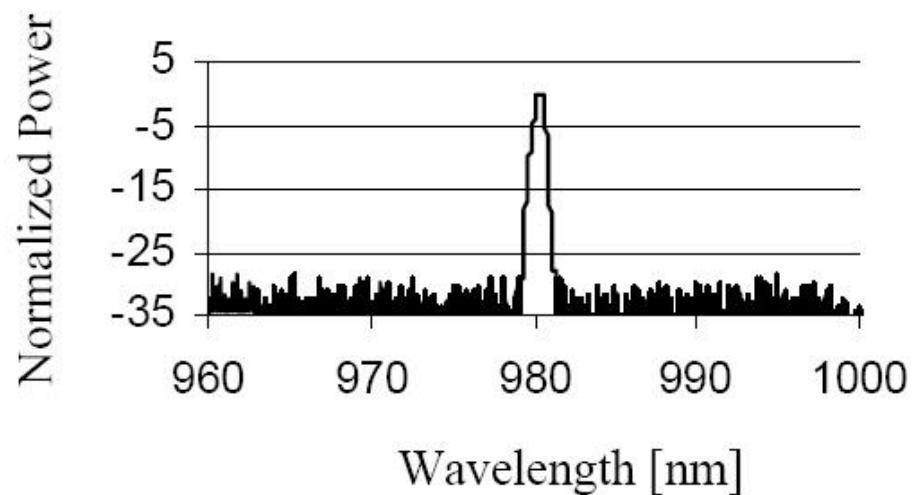
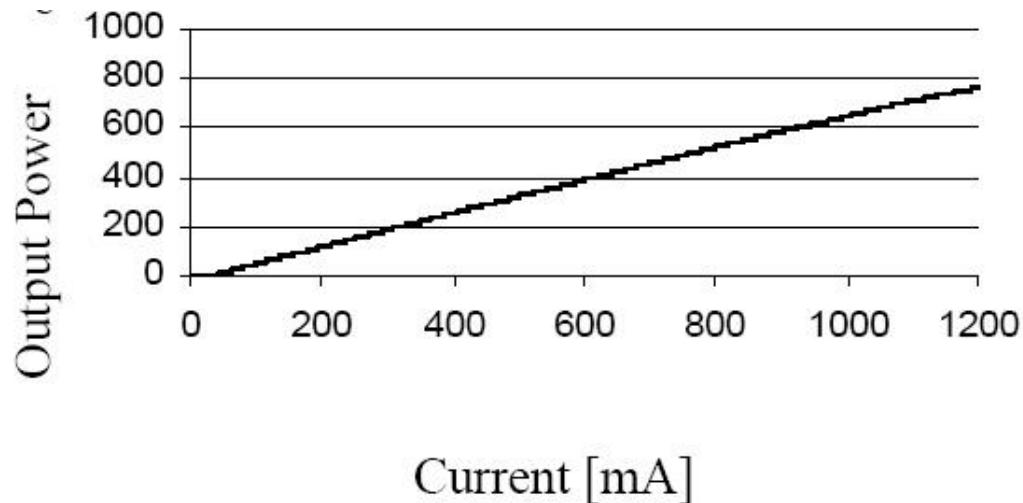
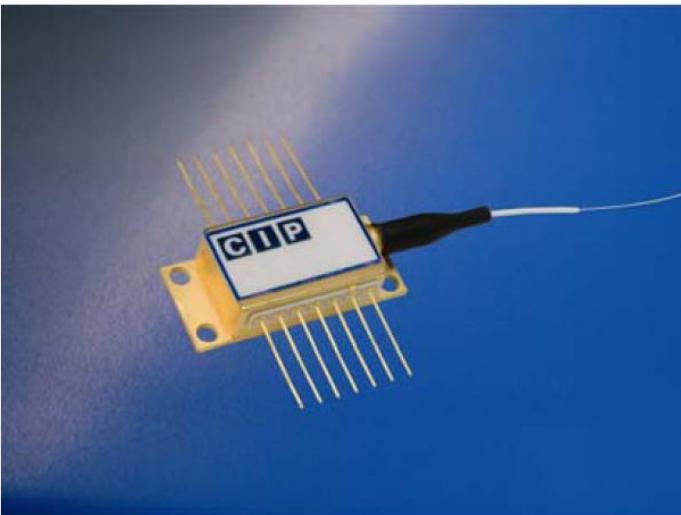
# Utilizare amplificatoare optice



# 7W 980 nm Multimode Pump Laser

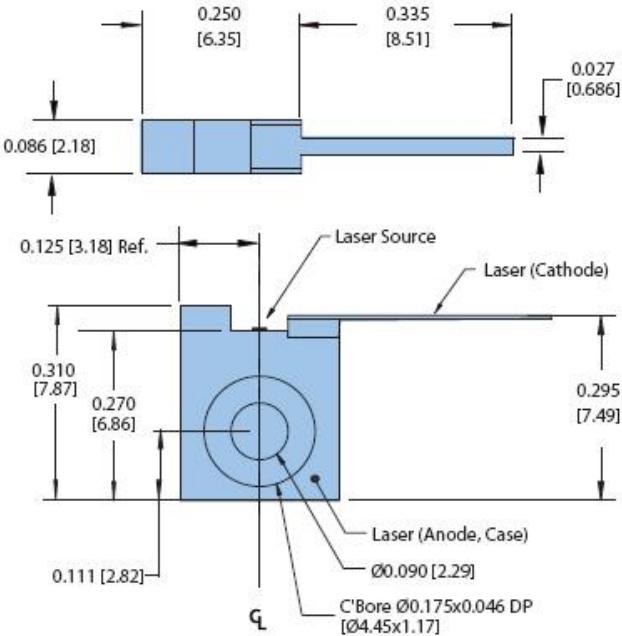


# 600mW 980 nm Singlemode Pump Laser

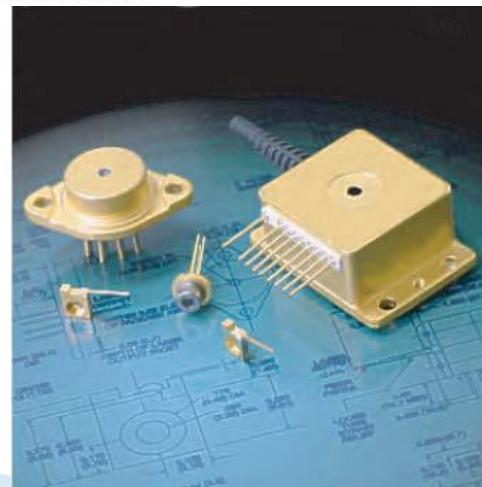
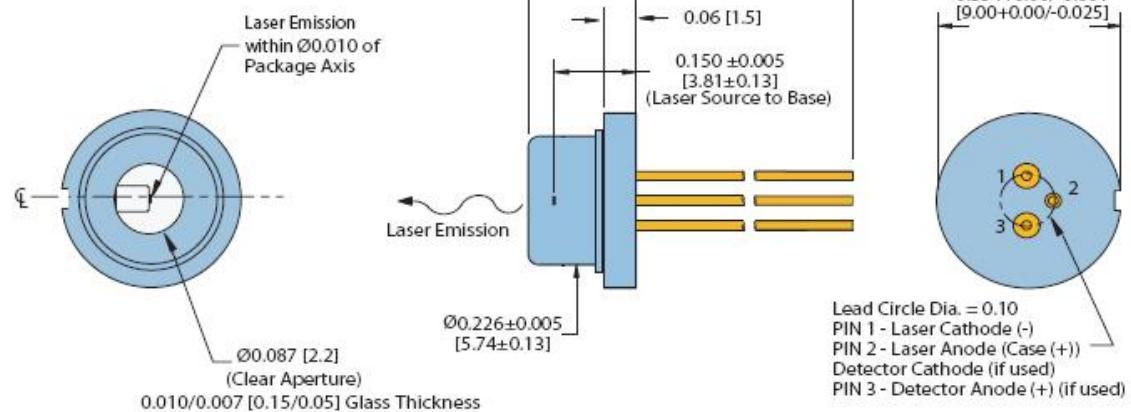


# 6 W, CW, 800nm

**C-Mount Package**

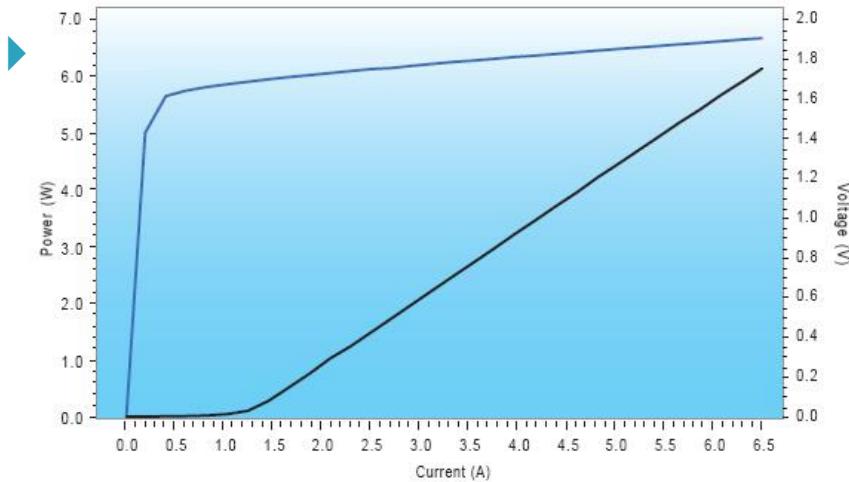


**9mm Package**

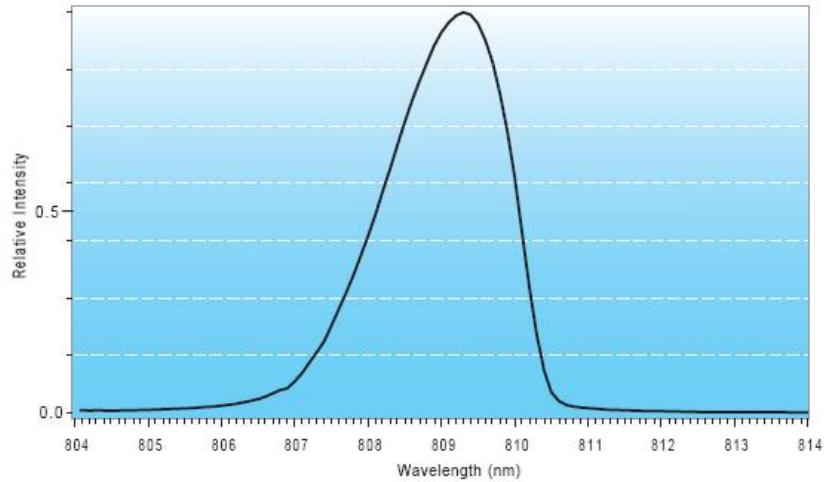


# 6 W, CW, 800nm

Typical L/I, V/I Graph

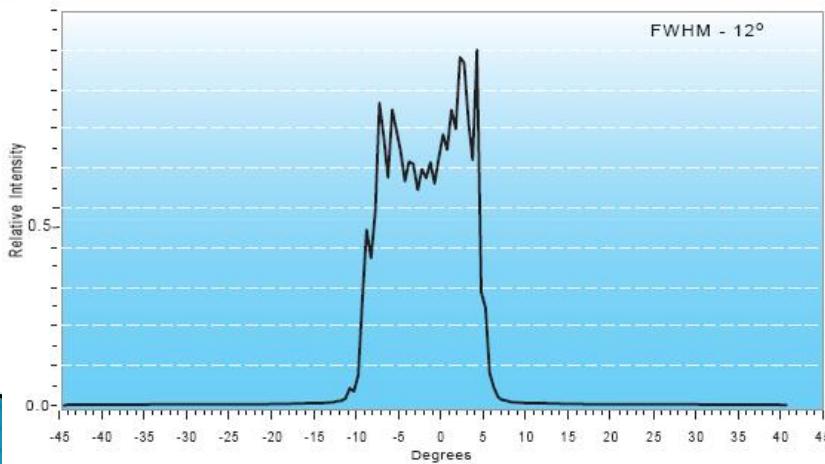


Wavelength Distribution



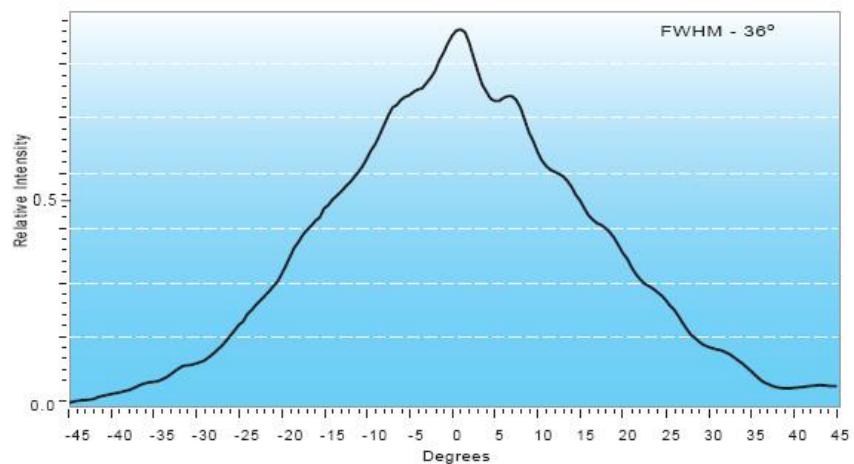
Typical Beam Divergence

Parallel

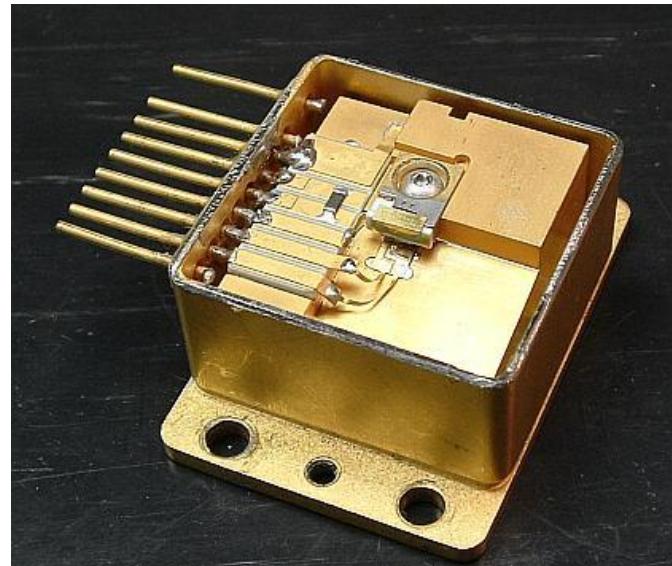
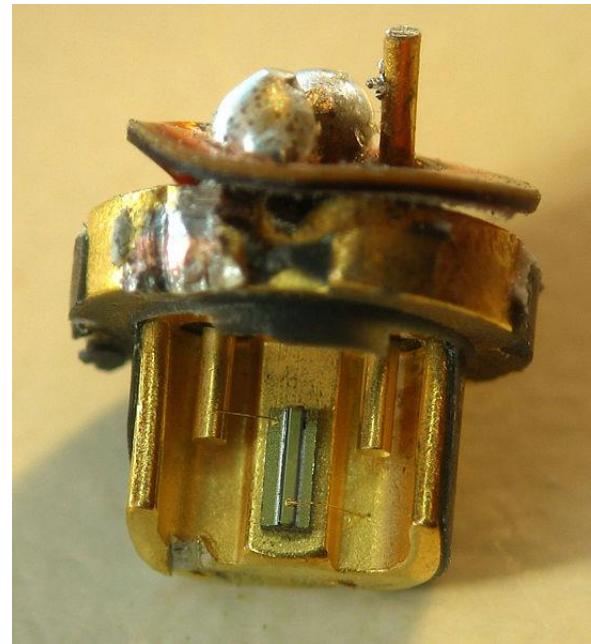
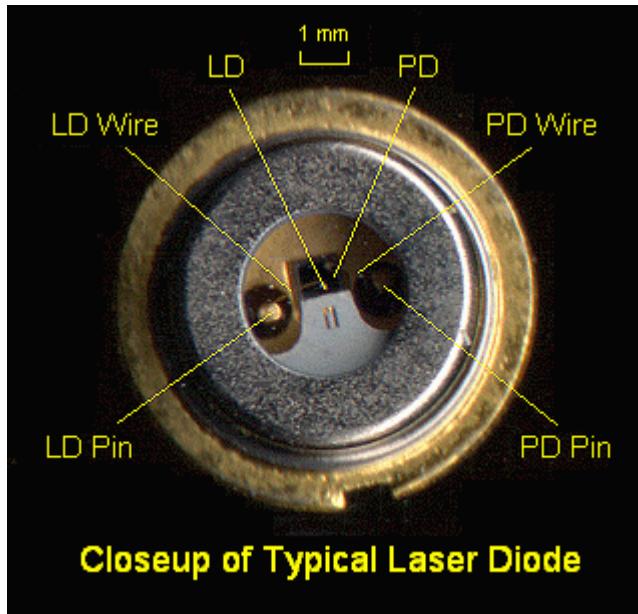


Typical Beam Divergence

Perpendicular



# CW Laser, 650 nm



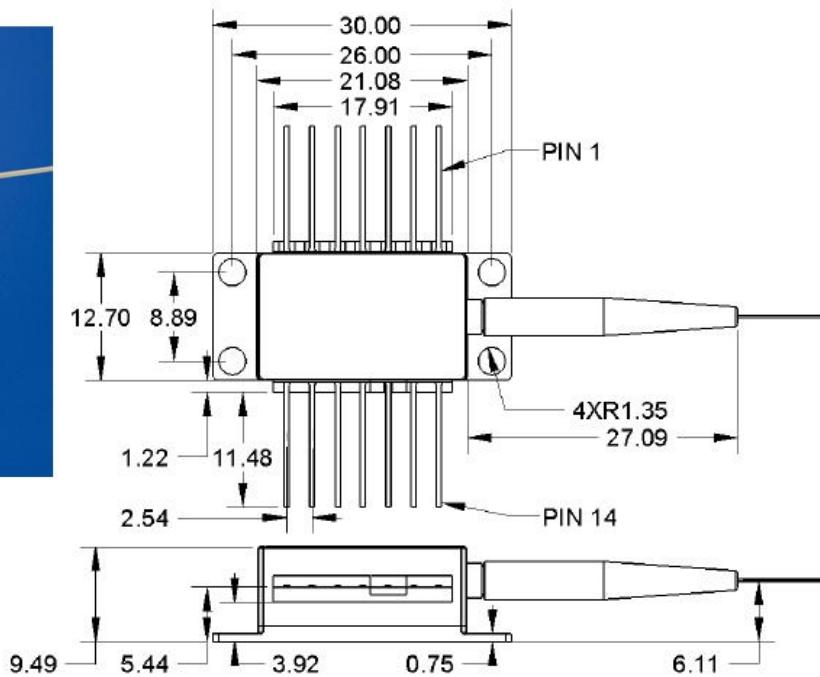
# Lungimi de unda

- ▶ **405 nm** – InGaN blue–violet laser, in Blu–ray Disc and HD DVD drives
- ▶ **445–465 nm** – InGaN blue laser multimode diode recently introduced (2010) for use in mercury–free high–brightness data projectors
- ▶ **510–525 nm** – Green diodes recently (2010) developed by Nichia and OSRAM for laser projectors.
- ▶ **635 nm** – AlGaInP better red laser pointers, same power subjectively twice as bright as 650 nm
- ▶ **650–660 nm** – GaInP/AlGaInP CDDVD, cheap red laser pointers
- ▶ **670 nm** – AlGaInP bar code readers, first diode laser pointers (now obsolete, replaced by brighter 650 nm and 671 nm DPSS)
- ▶ **760 nm** – AlGaInP gas sensing: O<sub>2</sub>
- ▶ **785 nm** – GaAlAs Compact Disc drives
- ▶ **808 nm** – GaAlAs pumps in DPSS Nd:YAG lasers (e.g., in green laser pointers or as arrays in higher–powered lasers)
- ▶ **848 nm** – laser mice
- ▶ **980 nm** – InGaAs pump for optical amplifiers, for Yb:YAG DPSS lasers
- ▶ **1,064 nm** – AlGaAs fiber–optic communication, DPSS laser pump frequency
- ▶ **1,310 nm** – InGaAsP, InGaAsN fiber–optic communication
- ▶ **1,480 nm** – InGaAsP pump for optical amplifiers
- ▶ **1,512 nm** – InGaAsP gas sensing: NH<sub>3</sub>
- ▶ **1,550 nm** – InGaAsP, InGaAsNSb fiber–optic communication
- ▶ **1,625 nm** – InGaAsP fiber–optic communication, service channel
- ▶ **1,654 nm** – InGaAsP gas sensing: CH<sub>4</sub>
- ▶ **1,877 nm** – GaInAsSb gas sensing: H<sub>2</sub>O
- ▶ **2,004 nm** – GaInAsSb gas sensing: CO<sub>2</sub>
- ▶ **2,330 nm** – GaInAsSb gas sensing: CO
- ▶ **2,680 nm** – GaInAsSb gas sensing: CO<sub>2</sub>
- ▶ **3,030 nm** – GaInAsSb gas sensing: C<sub>2</sub>H<sub>2</sub>
- ▶ **3,330 nm** – GaInAsSb gas sensing: CH<sub>4</sub>

# 1550nm DFB Laser

## Mechanical Drawing

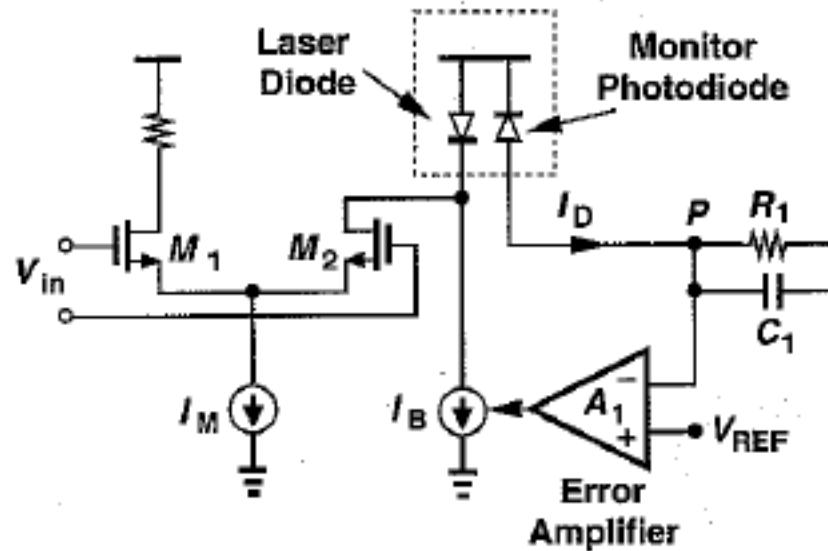
All units in mm



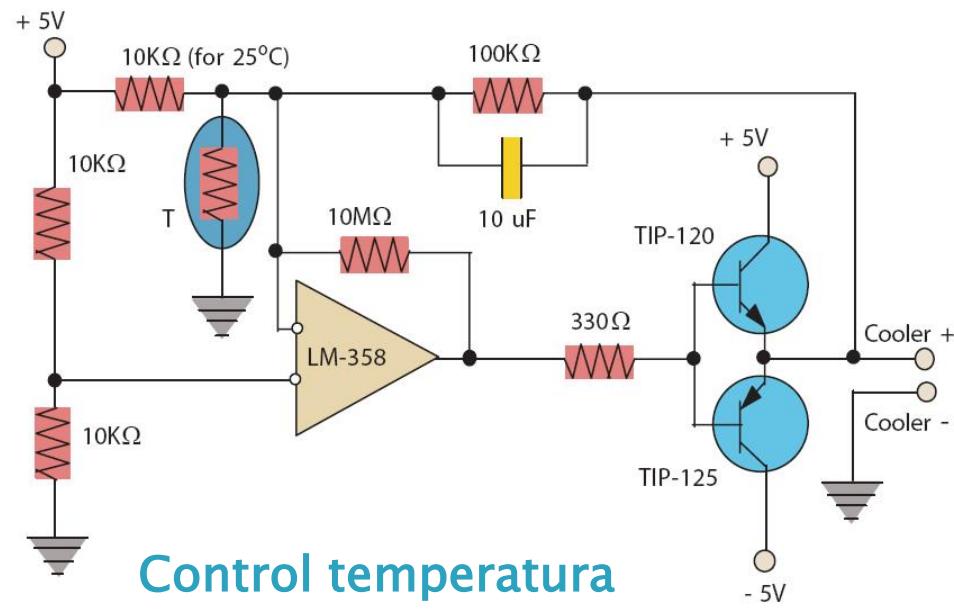
## Pin out

| Pin | Description                |
|-----|----------------------------|
| 1   | Thermistor                 |
| 2   | Thermistor                 |
| 3   | Laser Cathode (Bias)       |
| 4   | Monitor PD Anode           |
| 5   | Monitor PD Cathode         |
| 6   | TEC +                      |
| 7   | TEC -                      |
| 8   | Case GND, Laser Anode      |
| 9   | Case GND, Laser Anode      |
| 10  | Case GND, Laser Anode      |
| 11  | Case GND, Laser Anode      |
| 12  | Laser Cathode (modulation) |
| 13  | Case GND, Laser Anode      |
| 14  | Case GND, Laser Anode      |

# Control dioda LASER



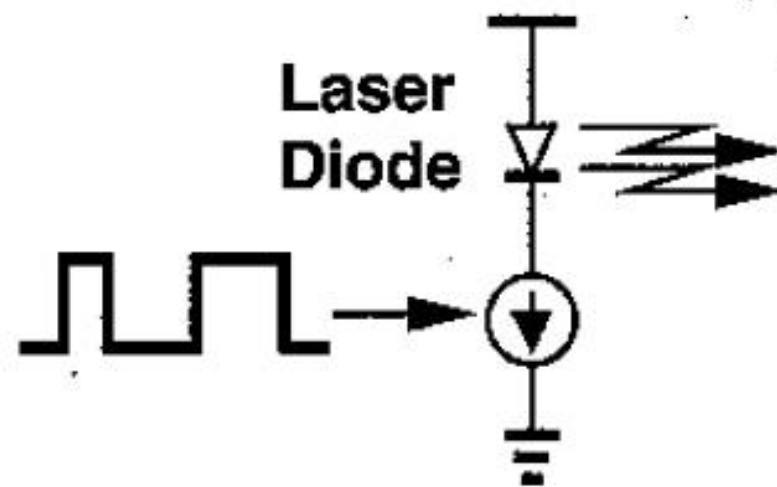
Control putere optica



Control temperatura

# Dioda LASER

- ▶ Ca si in cazul LED, pentru DL intensitatea luminoasa emisa este o functie de curentul prin dioda
  - aproape exclusiv, DL sunt controlate in curent
  - controlul in curent are avantajul unei viteze mai mari de lucru



# Dioda LASER

- ▶ Cerinte pentru driver-ele de diode laser
  - viteza mare de basculare pentru minimizarea interferentei intersimbol
  - curent mare de iesire
  - capacitatea de a rezista la variatiile de tensiune pe dioda Laser
- ▶ Cerintele sunt dificil de respectat deoarece sunt contradictorii
  - viteza mare presupune micsorarea dimensiunii componentelor
  - micsorarea dimensiunii
    - scade tensiunea de strapungere
    - scade capacitatea de curent/putere disipata

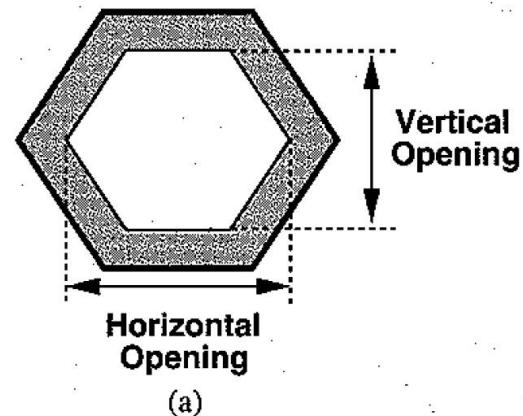
# Caracteristici driver-e DL

## ▶ Viteza

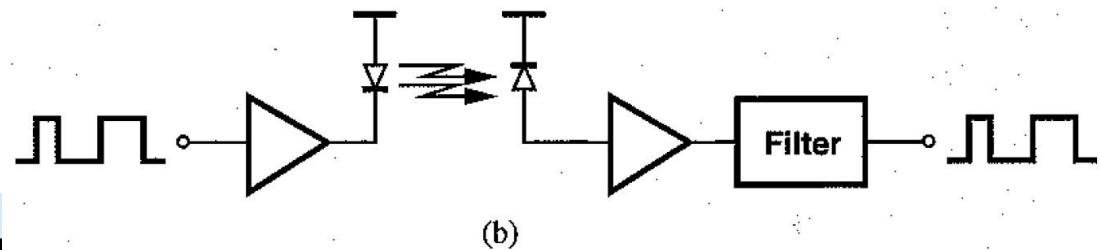
- caracterizata de timpii de crestere si de cadere
- suma acestora trebuie sa fie mult mai mica decat perioada de bit la viteza nominala de lucru

## ▶ Testarea vitezei de lucru

- standardizata
- “eye diagram”



(a)

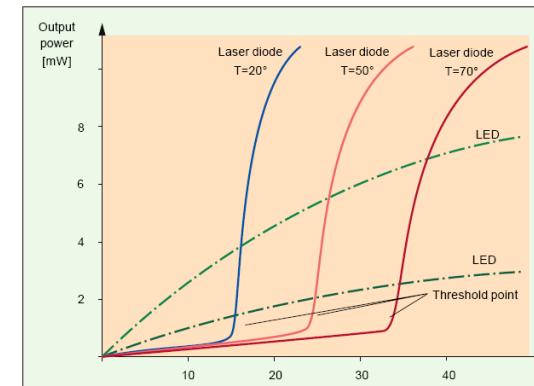


(b)

# Caracteristici driver-e DL

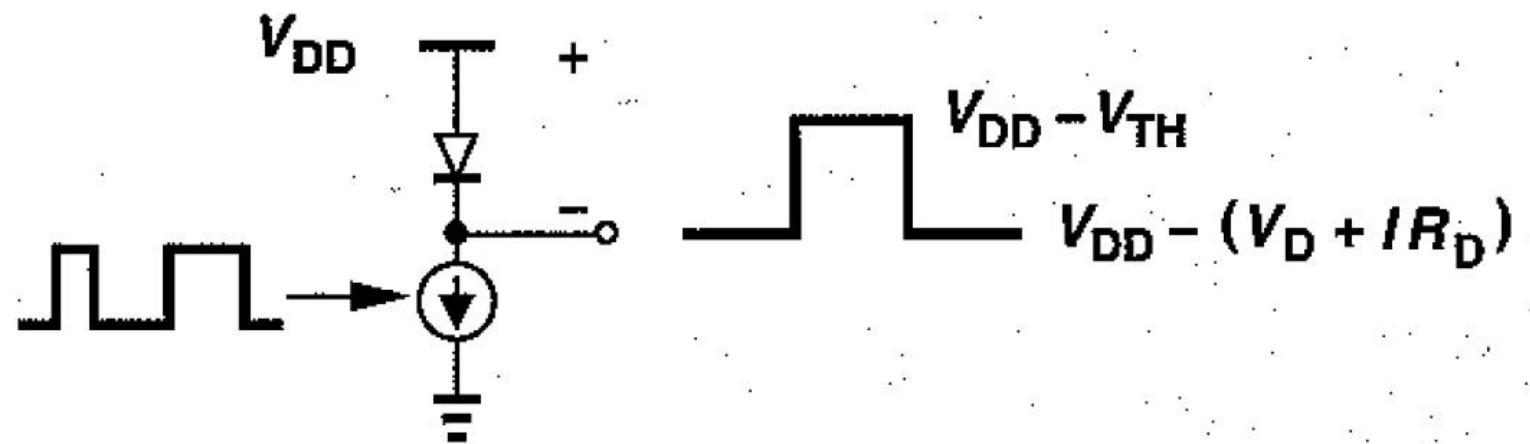
## ▶ Curent de iesire

- laserele trebuie polarizate in vecinatatea pragului, astfel incat o mica variatie de curent sa poata deschide dioda
- driver-ele de DL trebuie sa poata furniza:
  - un curent de “polarizare”
  - un curent de “modulatie”
- Curentul de “polarizare” (~ de prag) variaza cu temperatura si varsta diodei extrem de mult
- Curentul de “modulatie” (semnal) nu depinde de aceste elemente deoarece pentru DL
  - pragul depinde de temperatura si varsta
  - panta este aproximativ constanta



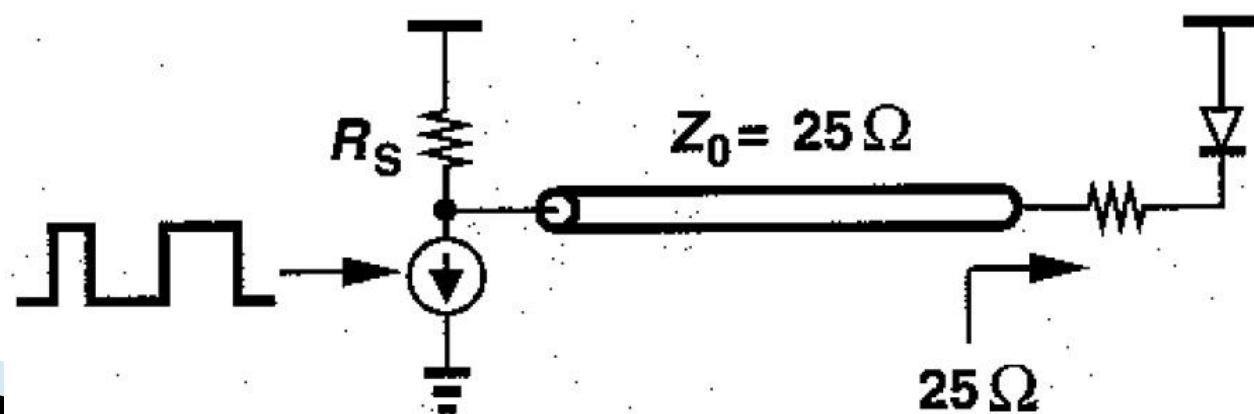
# Caracteristici driver-e DL

- ▶ Variatii de tensiune pe dioda LASER
  - generate de variatiile mari de curent si rezistenta interna a diodei



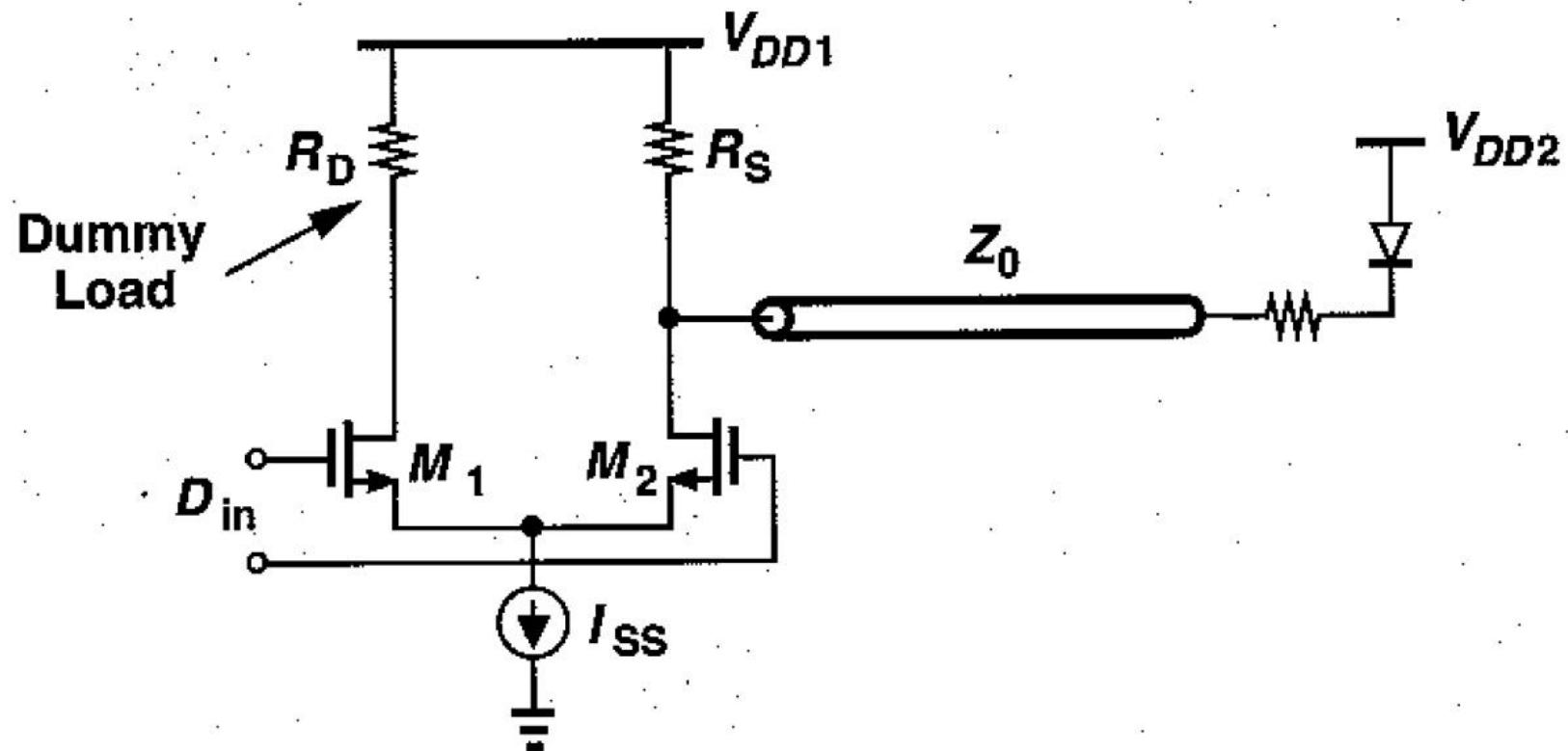
# Caracteristici driver-e DL

- ▶ Impedante de intrare si iesire
- ▶ Se lucreaza la viteze mari (1Gb/s, 10Gb/s)
  - se aplica considerente de proiectare a circuitelor de microunde
  - Intrarea in amplificator are tipic o impedanta de  $50\Omega$
  - Iesirea trebuie adaptata la impedanta diodei Laser
    - daca aceasta impedanta e prea mica, se creste la valori adecvate ( $\sim 25\Omega$ ) prin introducerea unui rezistor in serie



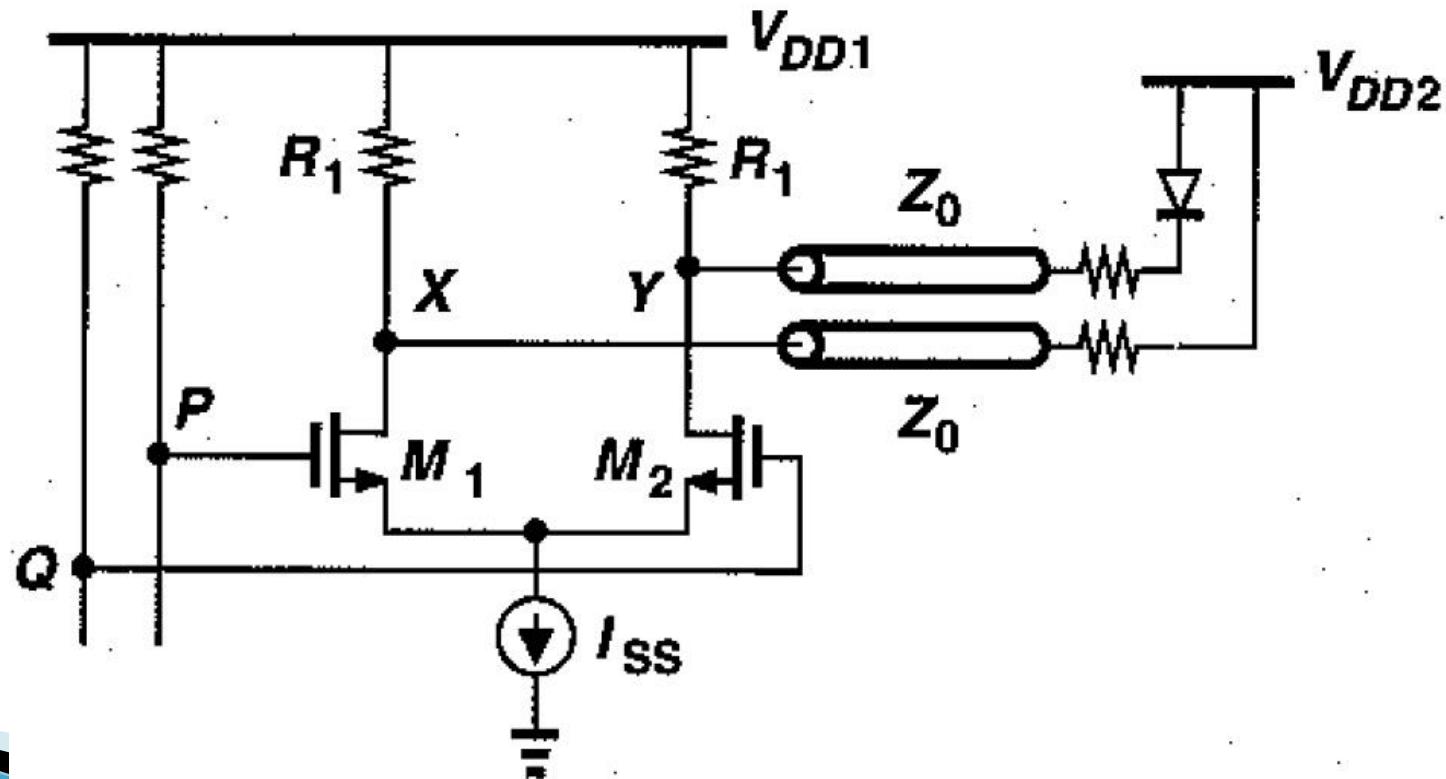
# Principii de proiectare

- ▶ Tipic etajul de ieșire se realizeaza diferential



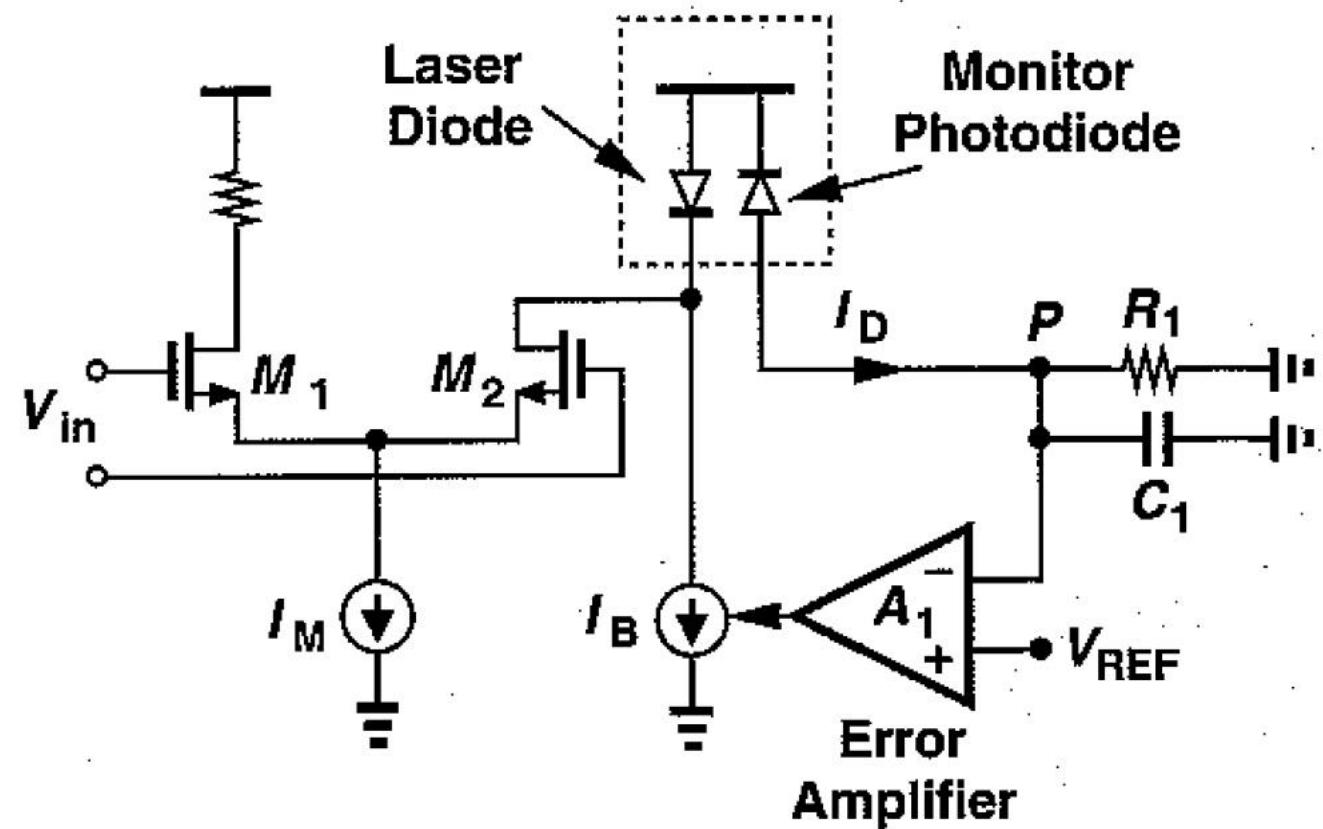
# Principii de proiectare

- ▶ La viteze mari se utilizeaza tipic tranzistoare unipolare si etajul differential se realizeaza simetric



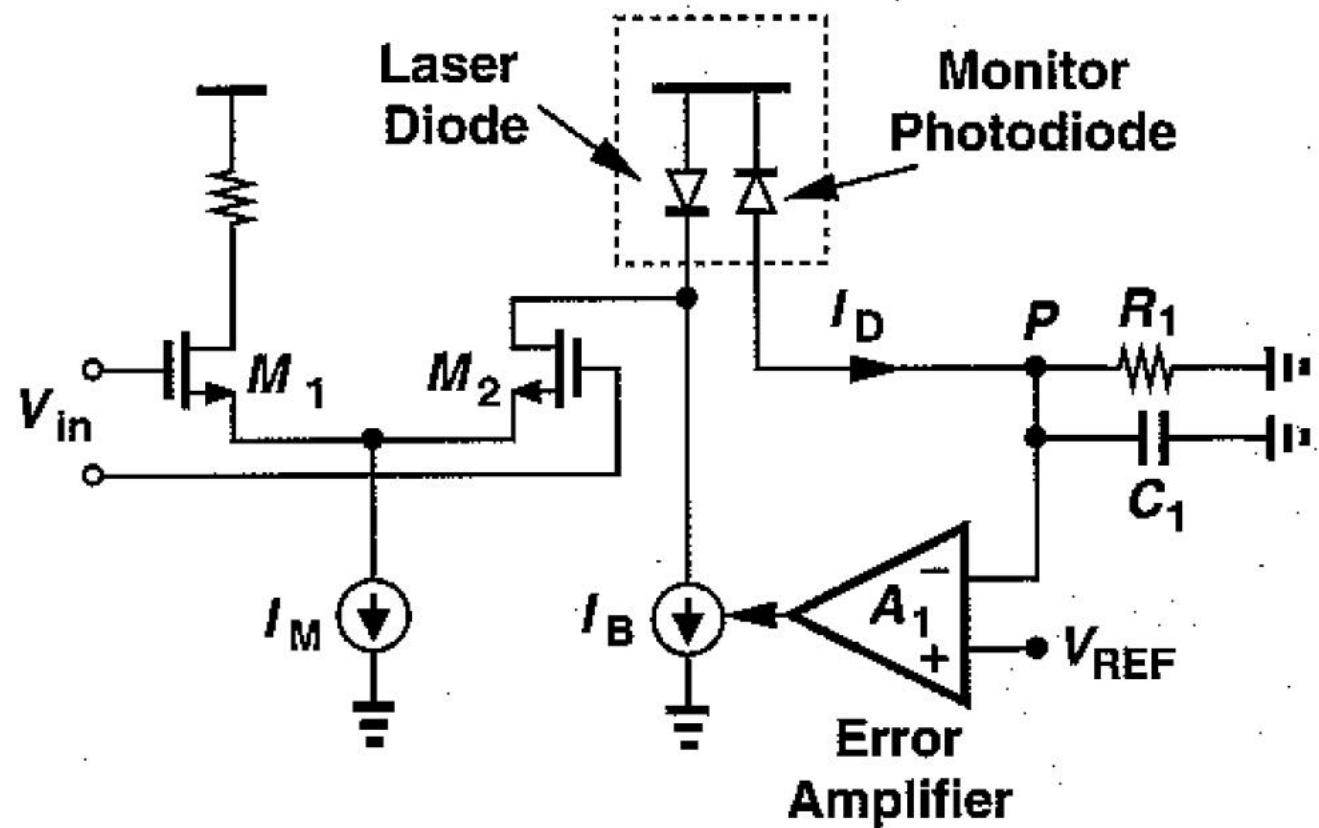
# Controlul puterii în DL

- ▶ Necesar datorita variatiei curentului de “polarizare”



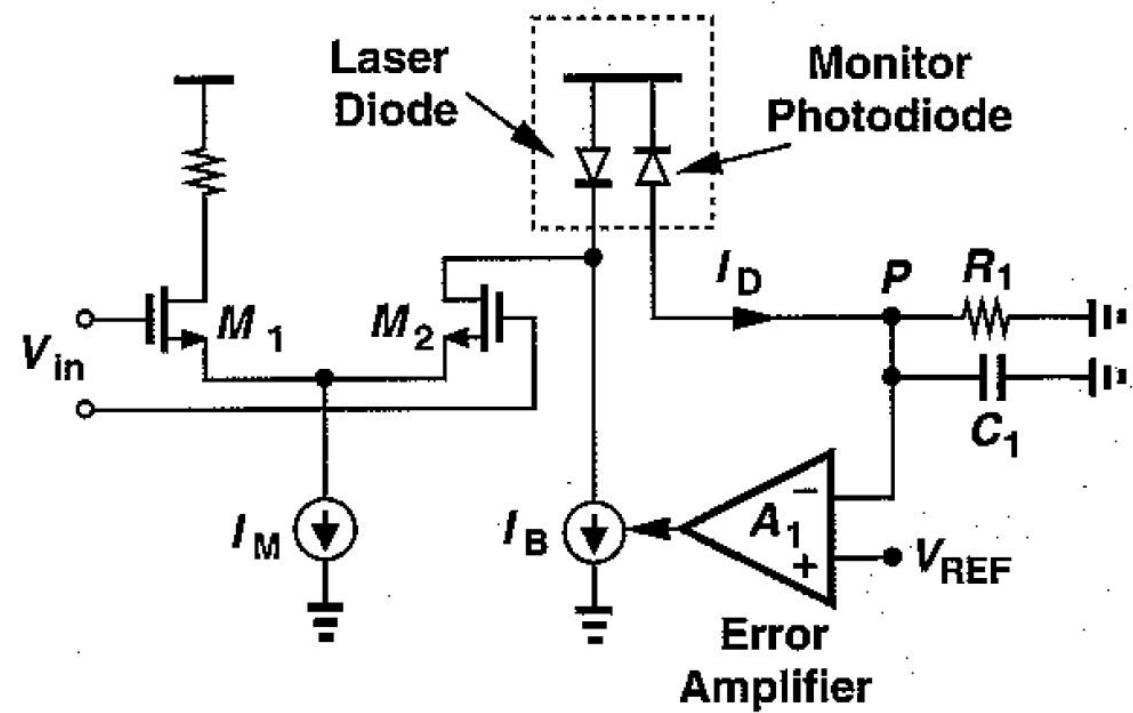
# Controlul puterii în DL

- circuitul RC din schema de reglaj a curentului de polarizare realizează o filtrare trece sus a semnalului



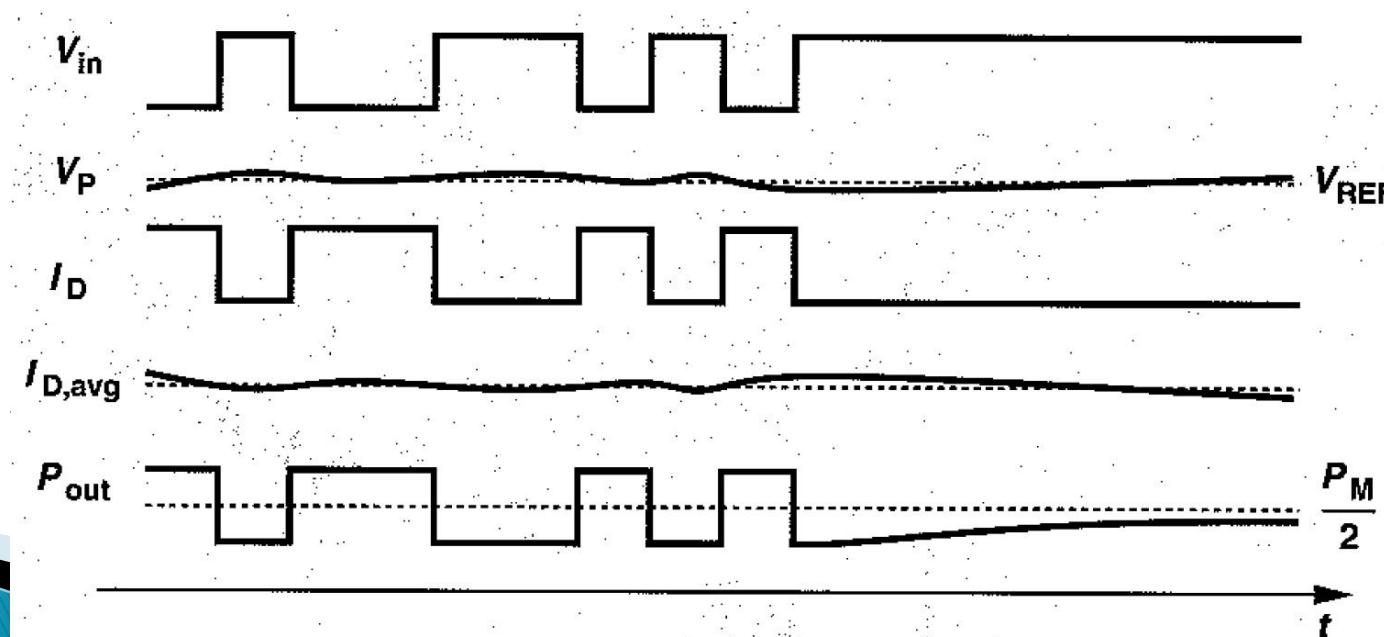
# Controlul puterii in DL

- ▶ La frecvențe prea mici de lucru bucla de reacție e suficient de rapidă pentru a urmări și anula curentul de semnal



# Controlul puterii in DL

- ▶ Bucla de reactie are efect si in cazul unei suite lungi de biti 1 transmisi
  - In acest caz, la limita curentul emis de dioda laser in starea OFF ajunge jumata din curentul corespunzator starii ON
  - Capacitatea de filtrare din bucla trebuie aleasa mare pentru a minimiza acest efect
  - daca valoarea e prea ridicata e necesara o capacitate externa circuitului integrat



# Fotodioda

Capitolul 9

# Cuprins

- ▶ Lumina ca undă electromagnetică (ecuațiile lui Maxwell, ecuația undelor, parametrii de propagare)
- ▶ Elemente de fotometrie și radiometrie (mărimi energetice/luminoase)
- ▶ Fibra optică (realizare, principiu de funcționare, atenuare, dispersie, banda de frecvență)
- ▶ Cabluri optice (tehnologie, conectori, lipire – splice)
- ▶ Proiectare sistemică a legăturii pe fibra optică (bandă de frecvență, balanță puterilor)
- ▶ Emițătoare optice (LED și dioda laser – realizare fizică și funcționare)
- ▶ Receptoare optice (dioda PIN, dioda cu avalanșă – realizare fizică și funcționare)
- ▶ Amplificatoare transimpedanță (parametri, scheme tipice, TIA în buclă deschisă, cu reacție, diferențiale, control automat al câștigului)
- ▶ Realizarea circuitelor pentru controlul emițătoarelor optice (parametri, scheme tipice, controlul puterii, multiplexoare)
- ▶ Dispozitive de captare a energiei solare (principiu de funcționare, utilizare, proiectare )

# Detectori optici

## ▶ Cerinte

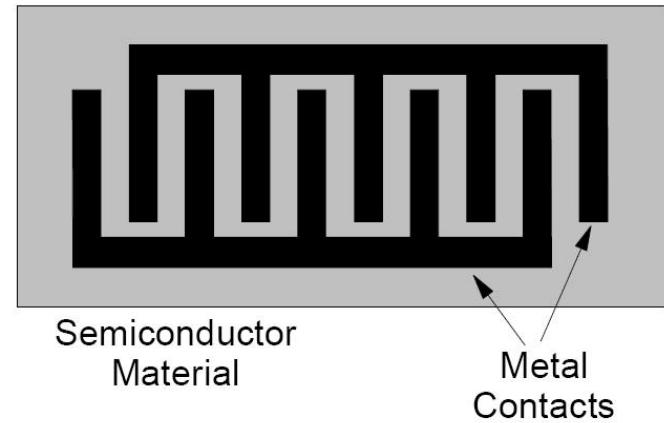
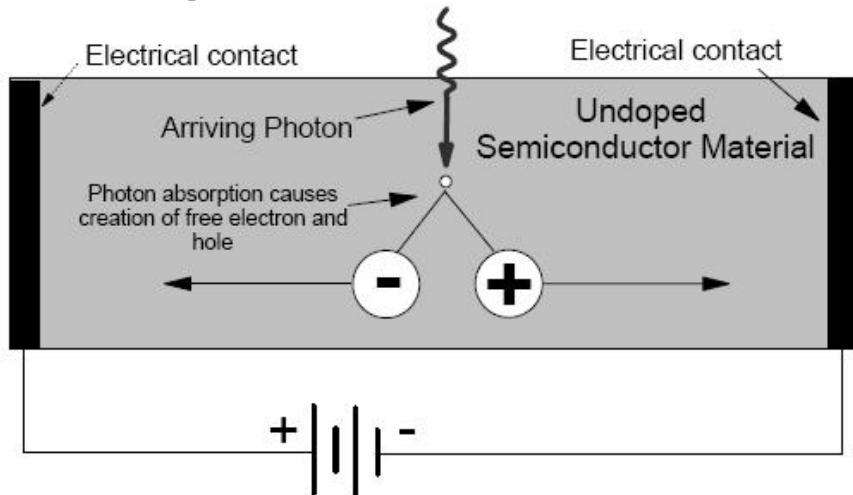
- eficienta crescuta a conversiei optic/electric
- zgomot redus
- raspuns uniform la diferite lungimi de unda
- viteza de raspuns ridicata
- liniaritate

## ▶ Principii de operare

- fotoconductori               $R = R(P_o)$
- fototranzistori               $I_B = I_B(P_o)$
- fotodiode                     $I = I(P_o)$ 
  - pn
  - pin
  - pin cu multiplicare in avalansa
  - Schottky

# Fotoconductori

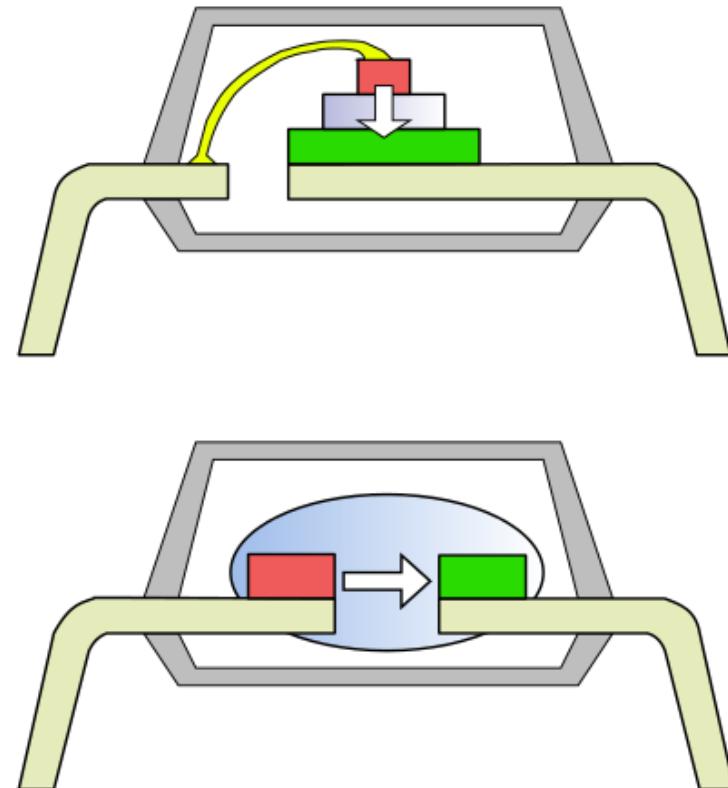
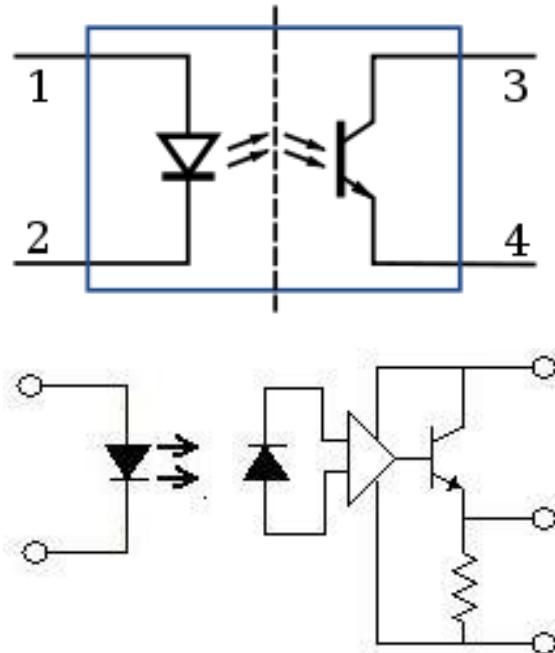
## ▶ Principiu



▶ Recent dispozitive Metal Semiconductor Metal (filtru interdigital) au inceput sa fie utilizate pentru usurinta de fabricare si integrare in aplicatii mai putin pretentioase

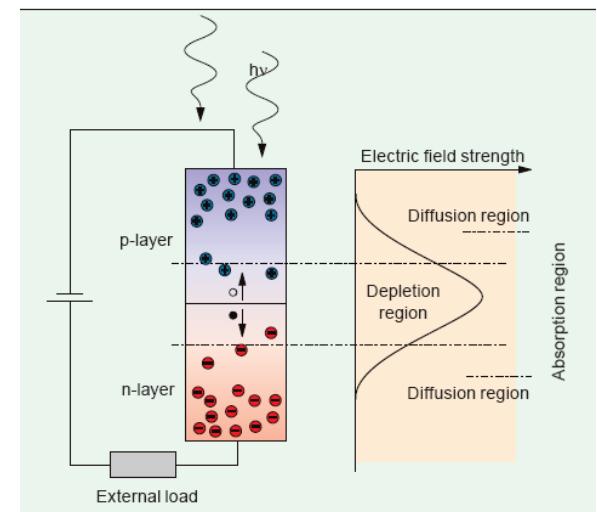
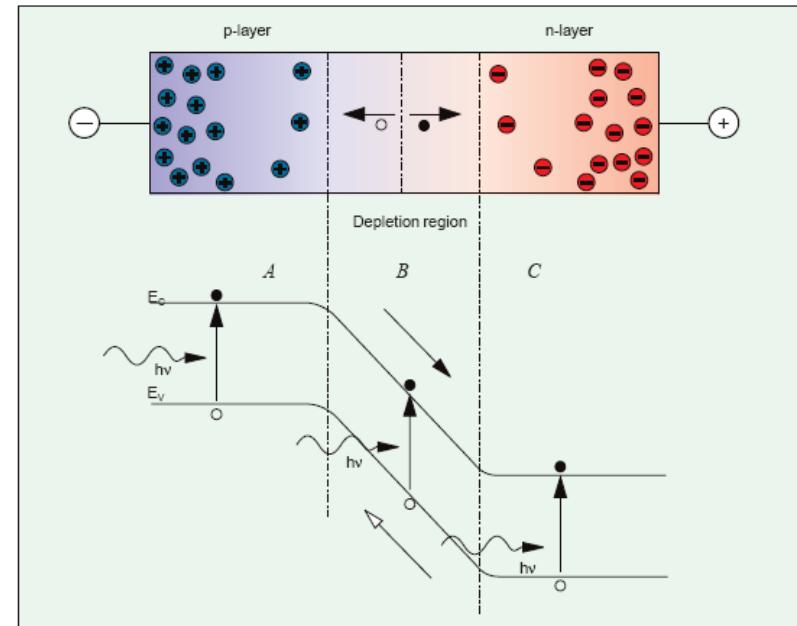
# Optocuploare

- ▶ utilizate pentru a oferi izolare electrica intre doua sectiuni ale unui circuit
  - izolarea portiunii de comanda si/sau masura de partea de “forta” a circuitului



# Fotodioda – Principiul de operare

- ▶ Jonctiunea pn este polarizata invers
- ▶ Lumina este absorbita in regiunea golita de purtatori, un foton absorbit generand o pereche electron-gol
- ▶ Sarcinile sunt separate de campul electric existent in regiunea golita si genereaza un curent in circuitul exterior



# Fotodioda – Principiul de operare

- ▶ Energia necesara pentru eliberarea unei perechi electron gol

$$h\nu = \frac{hc}{\lambda} \geq E_g$$

- ▶ Lungime de unda de taiere

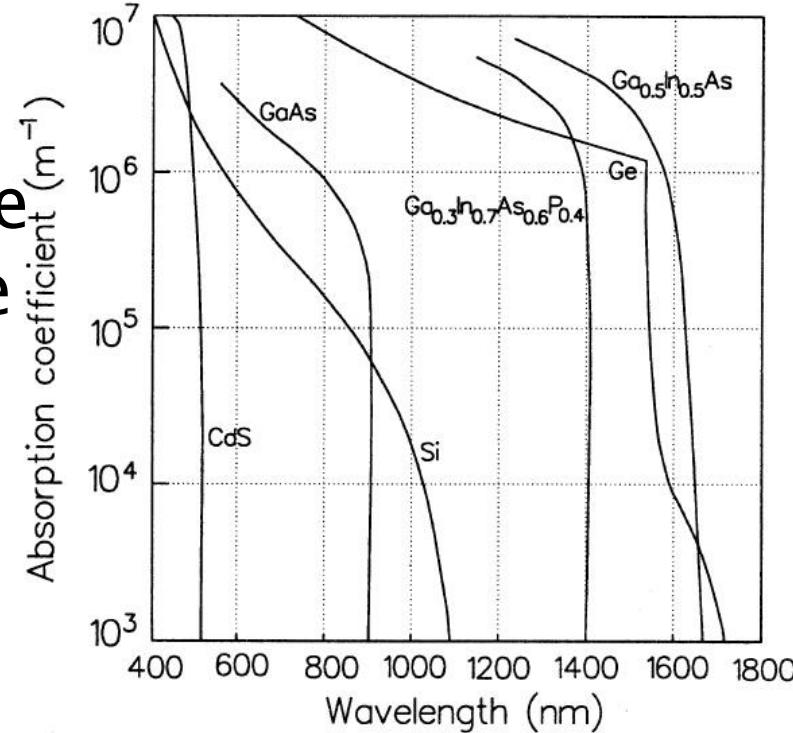
$$\lambda_{\max} = \frac{hc}{E_g}$$

- ▶ Puterea optica absorbita in zona golita de purtatori (w) aflata la o adincime d in interiorul dispozitivului

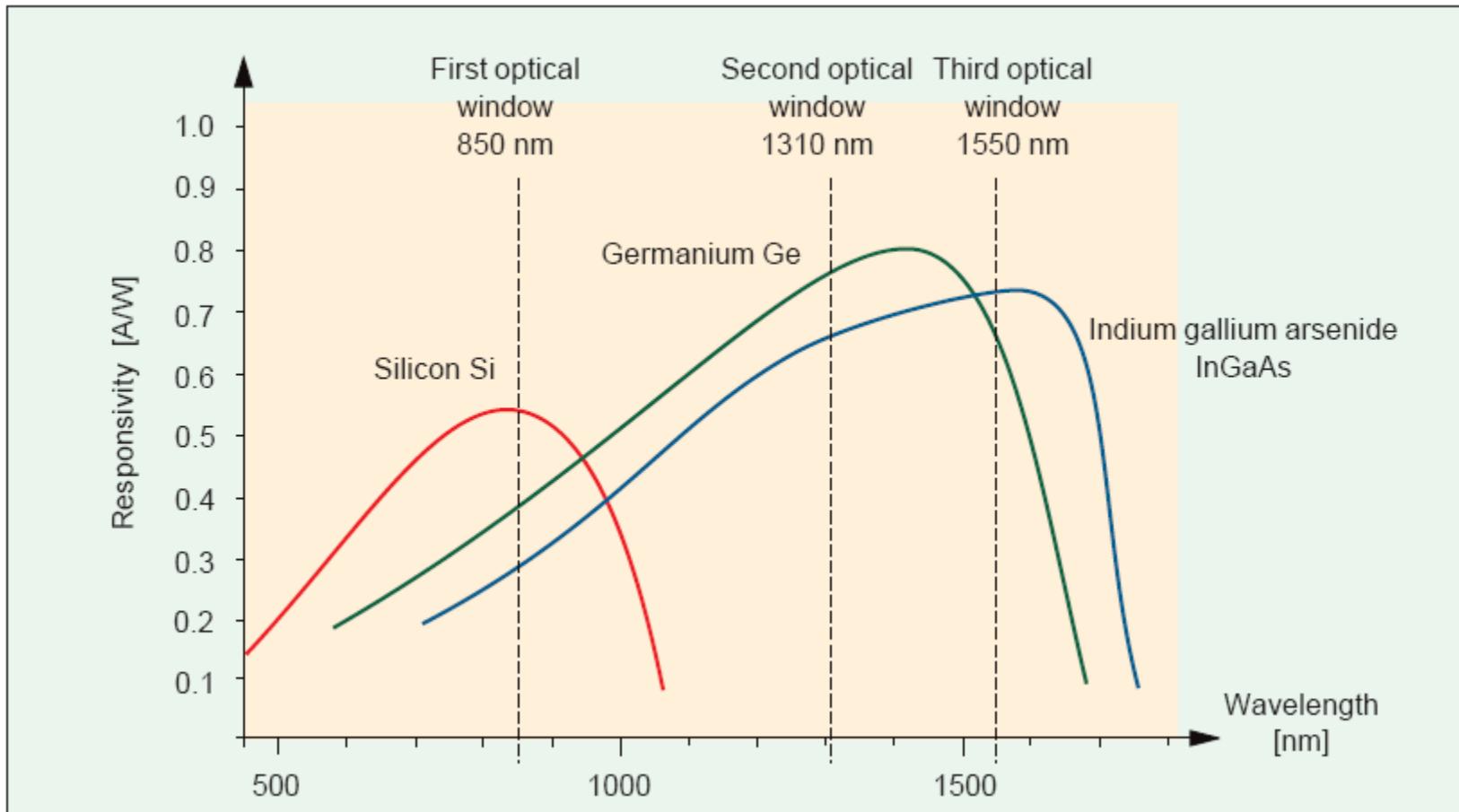
$$P(w) = P_i \cdot e^{-\alpha \cdot d} \cdot (1 - e^{-\alpha \cdot w}) \cdot (1 - R_f)$$

# Fotodioda – Principiul de operare

- ▶ Coeficientul de absorbtie pentru materialele uzuale
- ▶ Valoarea mare a coeficientului de absorbtie la lungimi de unda reduse implica scaderea rezponsivitatii
- ▶ Ca urmare comportarea **tuturor** materialelor este de tip trece banda



# Materiale utilizate pentru fotodiode



# Fotodioda – Marimi caracteristice

- ▶ Eficiența cuantica – raportul dintre numărul de perechi electron–gol generate și numărul de fotoni incidenti

$$\eta = \frac{n_e}{n_f}$$

- ▶ În unitatea de timp numărul de fotoni depinde de puterea optică, iar numărul de electroni impune curentul generat

$$\eta = \frac{I/e}{P/h\nu}$$

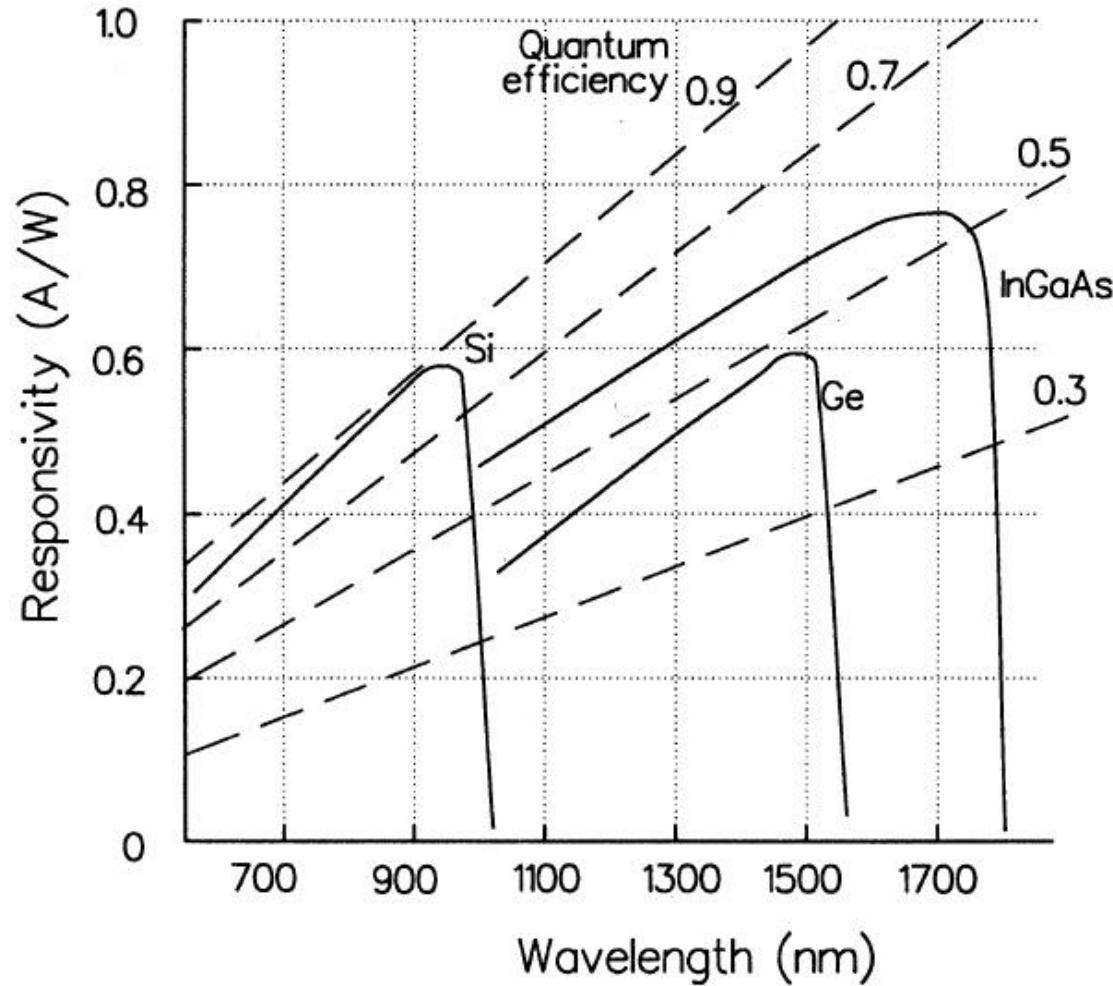
- ▶ Rezonanța

$$R = \frac{I}{P_o} = \frac{\eta \cdot e \cdot \lambda}{hc}$$

$$R = 0.8 \cdot \eta \cdot \lambda [\mu m] \quad \left[ \frac{A}{W} \right]$$

# Fotodiode - marimi karakteristice

$$R = \frac{I}{P_o} = \eta \cdot \frac{e}{hc} \cdot \lambda$$



# Materiale utilizate pentru fotodiode

| Material | $\lambda$ [ $\mu\text{m}$ ] | Responsivitate [A/W] | Viteza [ns] | Curent de intuneric |
|----------|-----------------------------|----------------------|-------------|---------------------|
| Si       | 0.85                        | 0.55                 | 3           | 1                   |
| Si       | 0.65                        | 0.4                  | 3           | 1                   |
| InGaAs   | 1.3–1.6                     | 0.95                 | 0.2         | 3                   |
| Ge       | 1.55                        | 0.9                  | 3           | 66                  |

- Dezavantajul major pentru Ge este curentul de intuneric mare

| Material                                 | Eg (eV) |
|--|---------|
| GaAs                                     | 1.43    |
| GaSb                                     | 0.73    |
| GaAs <sub>0.88</sub> Sb <sub>0.12</sub>  | 1.15    |
| Ge                                       | 0.67    |
| InAs                                     | 0.35    |
| InP                                      | 1.35    |
| In <sub>0.53</sub> Ga <sub>0.47</sub> As | 0.75    |
| In <sub>0.14</sub> Ga <sub>0.86</sub> As | 1.15    |
| Si                                       | 1.14    |

# Current de intuneric

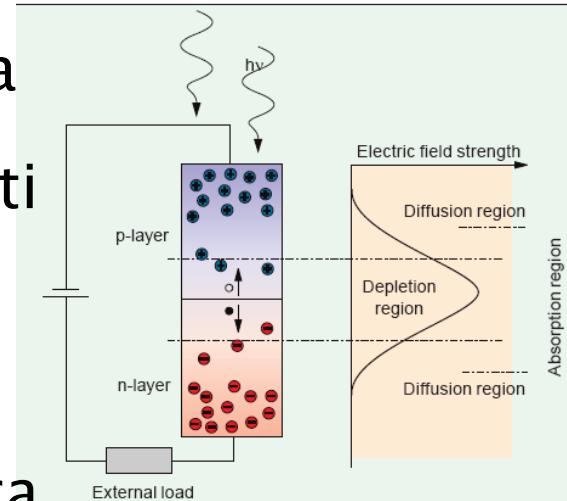
- ▶ Currentul invers al jonctiunii p–n, datorat agitatiei termice, prezent in absenta iluminarii
- ▶ Constituie o importanta sursa de zgomot (limiteaza aplicatiile Ge)

$$I_D = I_S \approx \frac{\beta \cdot kT}{eR_0}$$

- $\beta$  – coeficient de idealitate  $\beta = 1 \div 2$
- $R_0$  – rezistenta la intuneric a diodei (invers proportionala cu aria diodei)

# Fotodioda PIN

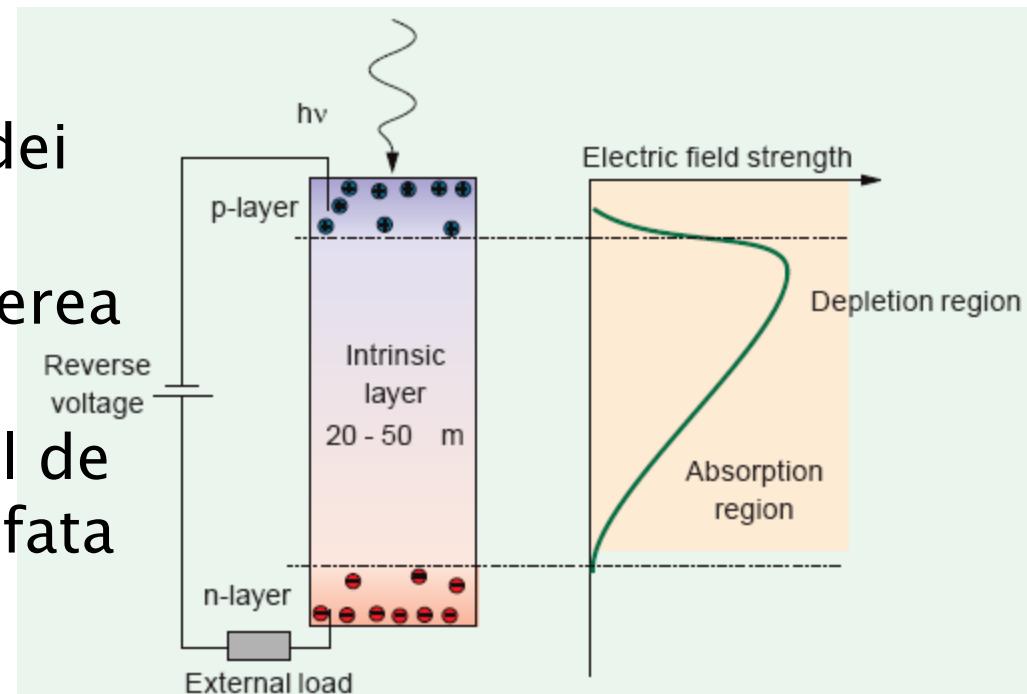
- ▶ Existenta campului electric in regiunea golita de purtatori face ca eventualii purtatori generati optic sa fie accelerati spre terminale pentru constituirea photocurentului
- ▶ Problemele utilizarii diodei pn polarizate invers ca fotodetector sunt generate de adancimea extrem de mica a zonei golite ( $w$ )
- ▶ Puterea optica absorbita in interiorul acestei zone e in consecinta redusa
- ▶ Purtatorii generati inafara zonei de golire ajung eventual in zona golita si vor fi accelerati spre terminale, dar viteza fenomenului este prea redusa pentru aplicatii in comunicatii



$$P(w) = P_i \cdot e^{-\alpha \cdot d} \cdot (1 - e^{-\alpha \cdot w}) \cdot (1 - R_f)$$

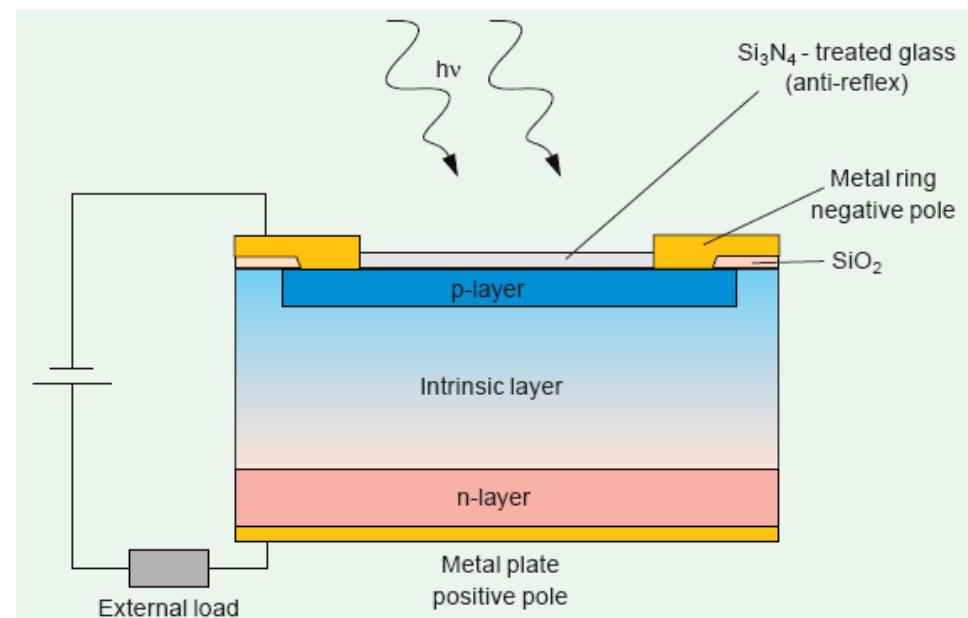
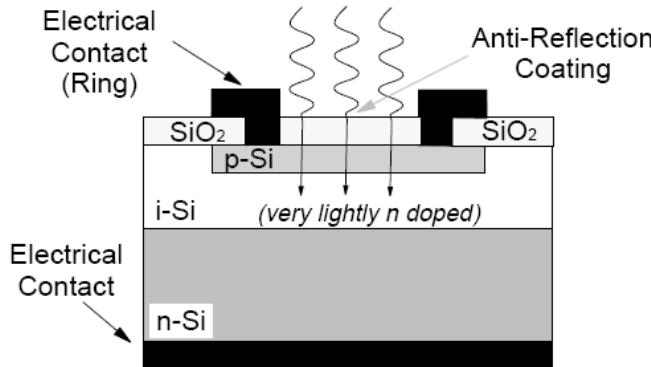
# Fotodioda PIN

- ▶ Solutia consta in introducerea unui strat foarte slab dopat (intrinsec) intre cele doua zone ale diodei
  - creste volumul de absorbtie deci creste sensibilitatea fotodiodei
  - capacitatea jonctiunii scade ducand la cresterea vitezei
  - este favorizat curentul de conductie (mai rapid) fata de cel de difuzie



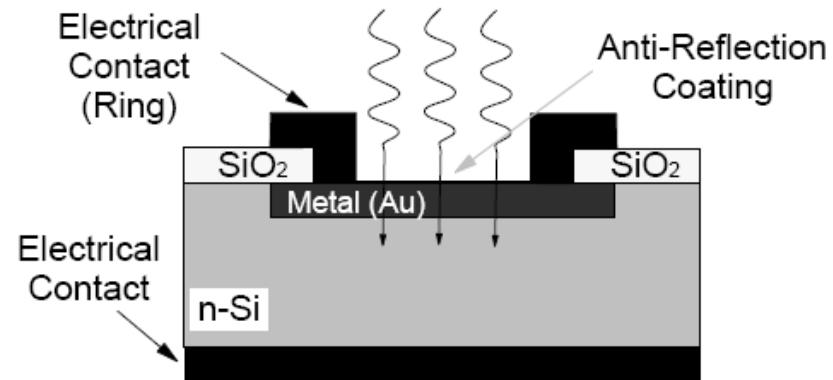
# Structura fotodiodei PIN

- ▶ tipic, adancimea stratului intrinsec este de  $20\text{--}50\mu\text{m}$
- ▶ cresterea suplimentara a adancimii ar duce la cresterea timpului de tranzit
  - $w=20\mu\text{m} \rightarrow T_{tr} \approx 0.2\text{ns}$



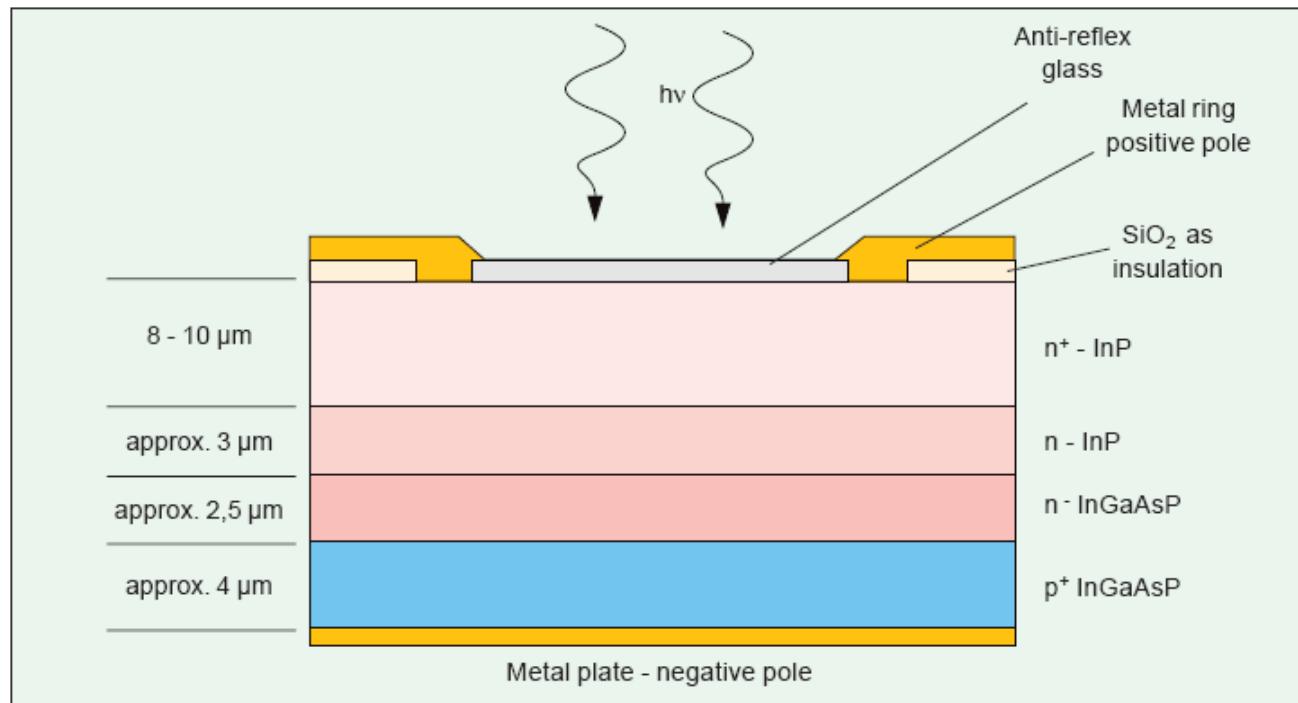
# Structura fotodiodelor Schottky

- ▶ se bazeaza pe jonctiunea metal semiconductor
- ▶ vitezele de lucru sunt mult mai mari, metalul fiind un bun conductor realizeaza evacuarea mult mai rapida a purtatorilor din jonctiune
- ▶ permite utilizarea unor materiale cu eficienta mai mare dar care nu pot fi dopate simultan p  
si n pentru utilizare in PIN
- ▶ modulatie cu 100GHz posibila



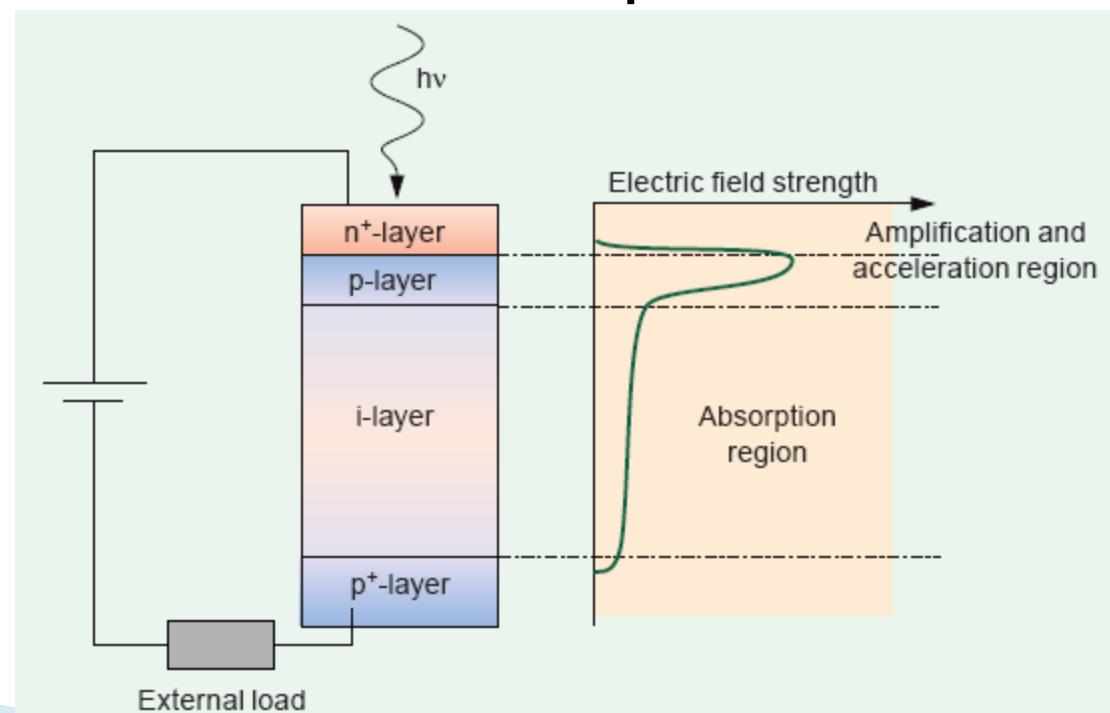
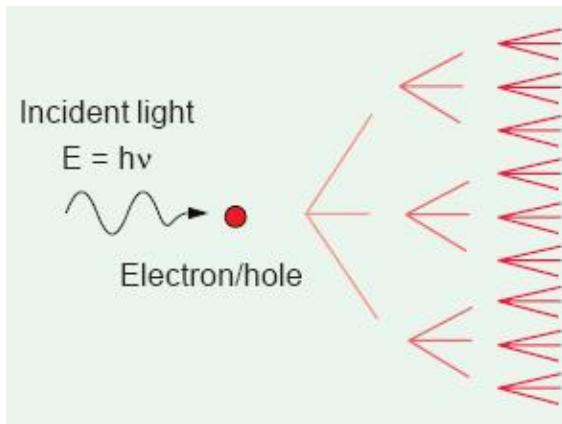
# Fotodioda PIN pentru lungimi de unda crescute (1550nm)

- ▶ se utilizeaza tipic
  - InGaAsP pe substrat InP
  - GaAlAsSb pe substrat GaSb



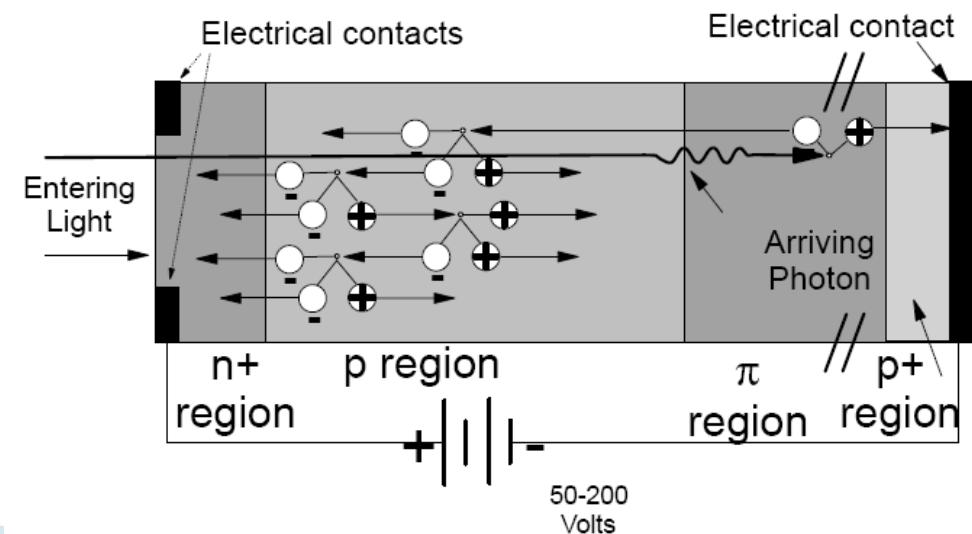
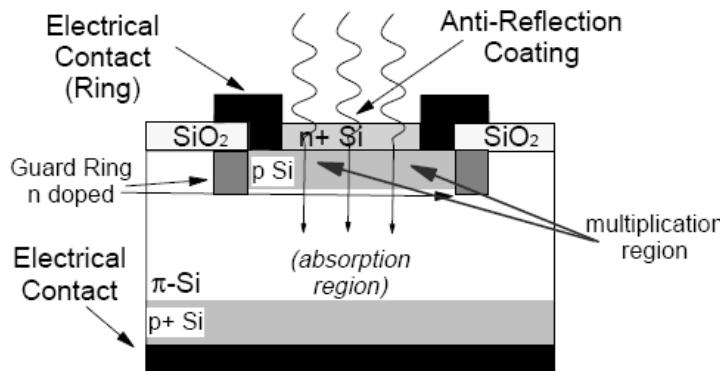
# Fotodioda PIN cu multiplicare in avalansa

- ▶ daca viteza purtatorilor este suficient de mare genereaza noi perechi electron/gol prin ionizare de impact
- ▶ amplificarea are loc in acelasi timp cu detectia

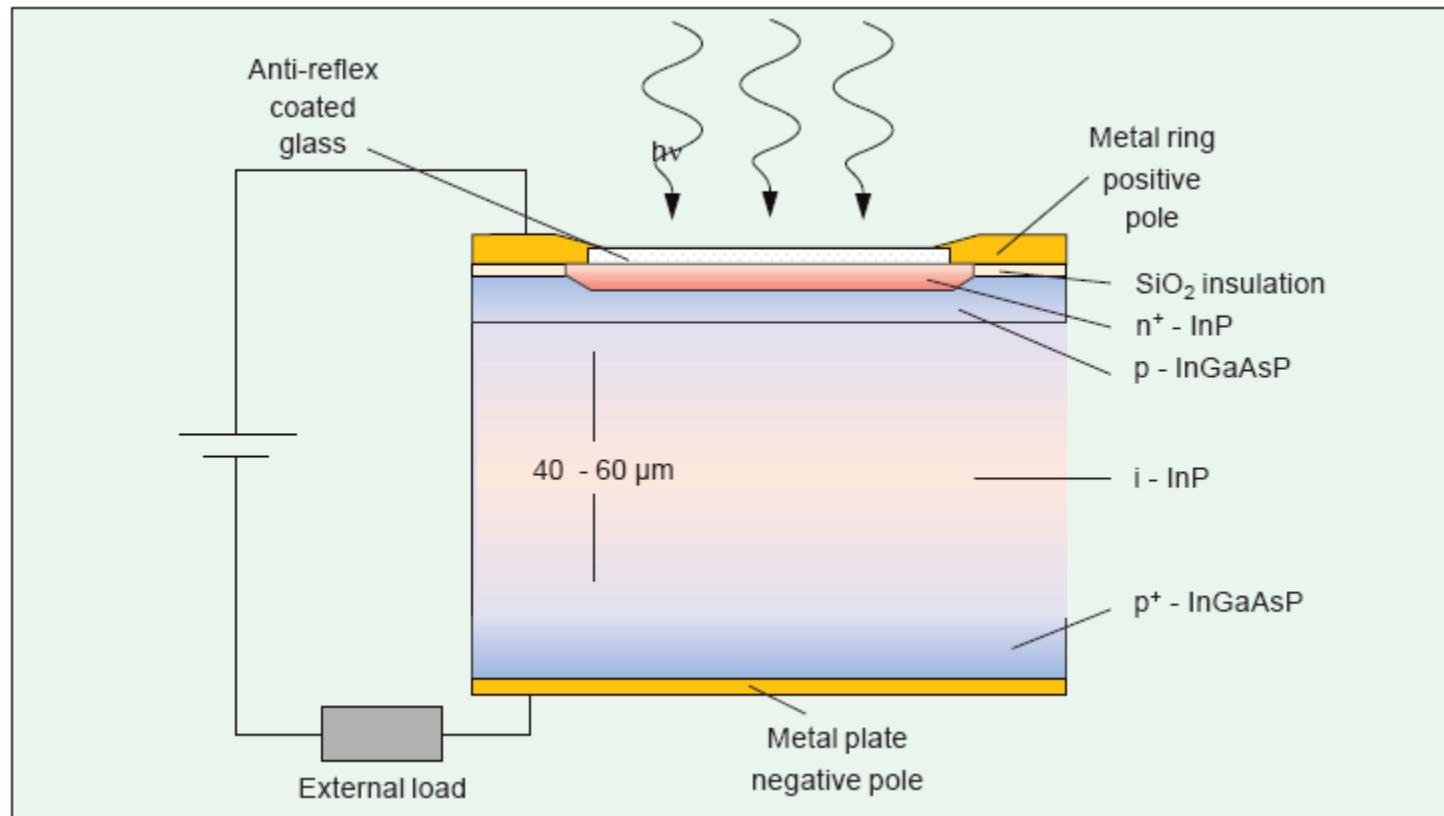


# Functionarea fotodiodei cu multiplicare in avalansa

- ▶ campuri electrice de ordinul minim:  $3 \times 10^5$  V/m, tipic:  $10^6$  V/m sunt necesare
- ▶ aceste campuri sunt generate de tensiuni inverse de polarizare de ordinul 50–300V
- ▶ structura este modificata pentru concentrarea campului in zona de accelerare



# Structura fotodiodei cu multiplicare in avalansa



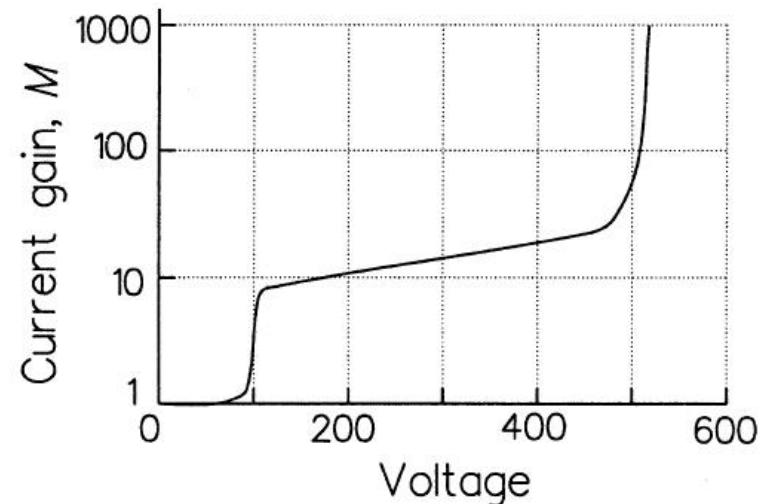
# Caracteristicile fotodiodei cu multiplicare în avalansa

- ▶ factorul de multiplicare caracterizează amplificarea photocurentului generat

$$M = \frac{I_M}{I}$$

- ▶ Rezonabilitatea

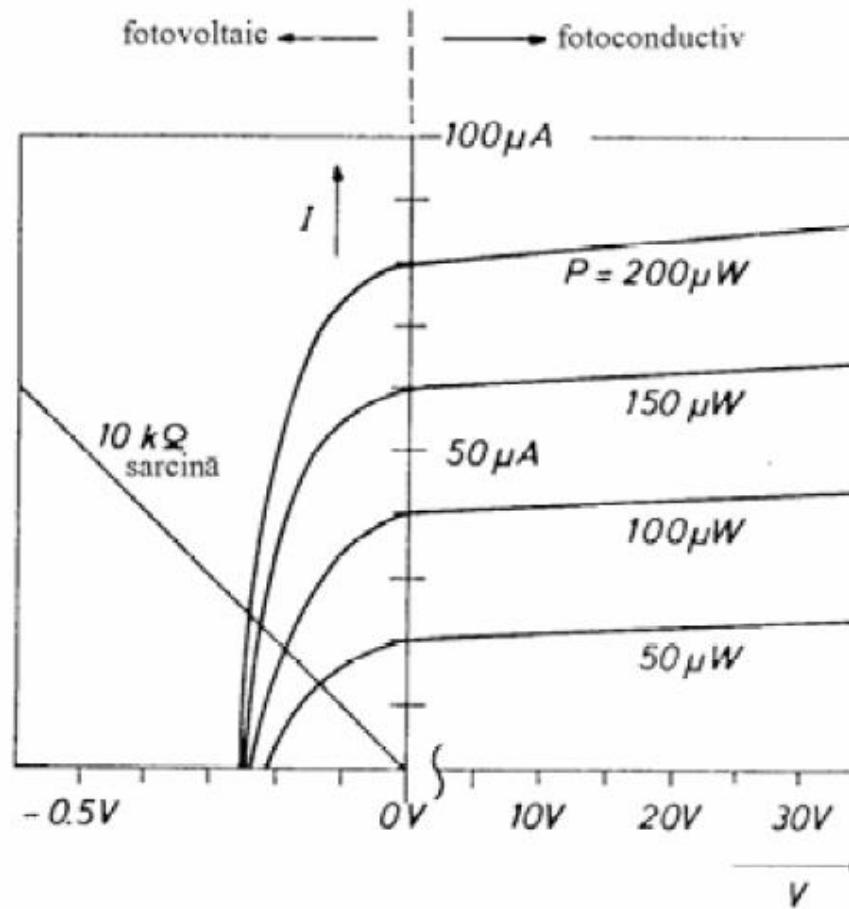
$$R = \frac{I}{P_o} = \frac{\eta \cdot e \cdot \lambda}{hc} \cdot M$$



# Dezavantaje

- ▶ tensiuni inverse de polarizare mari cresc complexitatea circuitului
- ▶ diodele cu multiplicare in avalansa sunt intrinsec mai zgomotoase (currentul de zgomot este amplificat de asemenea)
- ▶ factorul de multiplicitate are o componenta aleatorie (zgomot suplimentar)
- ▶ viteza mai redusa (timp de generare al avalansei)

# Caracteristici curent/tensiune Fotodioda

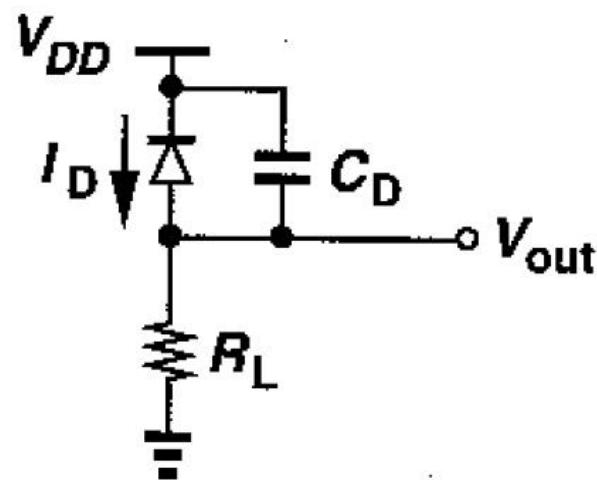


# Amplificatoare transimpedanta

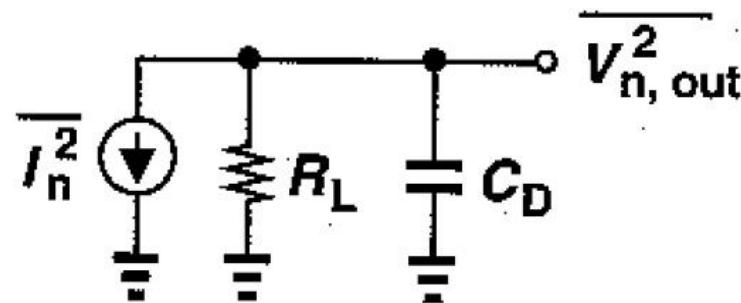
- ▶ Fotodiodele genereaza un curent proportional cu puterea optica receptionata
- ▶ Primul pas necesar este conversia acestui curent la o tensiune
- ▶ Amplificatoarele transimpedanta sunt amplificatoarele atacate in curent si care ofera la iesire o tensiune propotionala cu acesta
- ▶ Amplificarea este masurata in  $\Omega$  ( $k\Omega$ )

# Amplificatoare transimpedanta

- ▶ Cel mai simplu amplificator transimpedanta este un rezistor



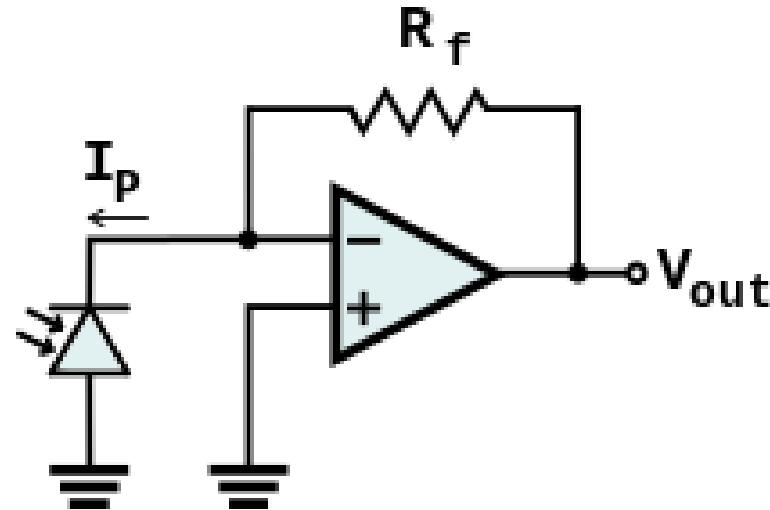
(a)



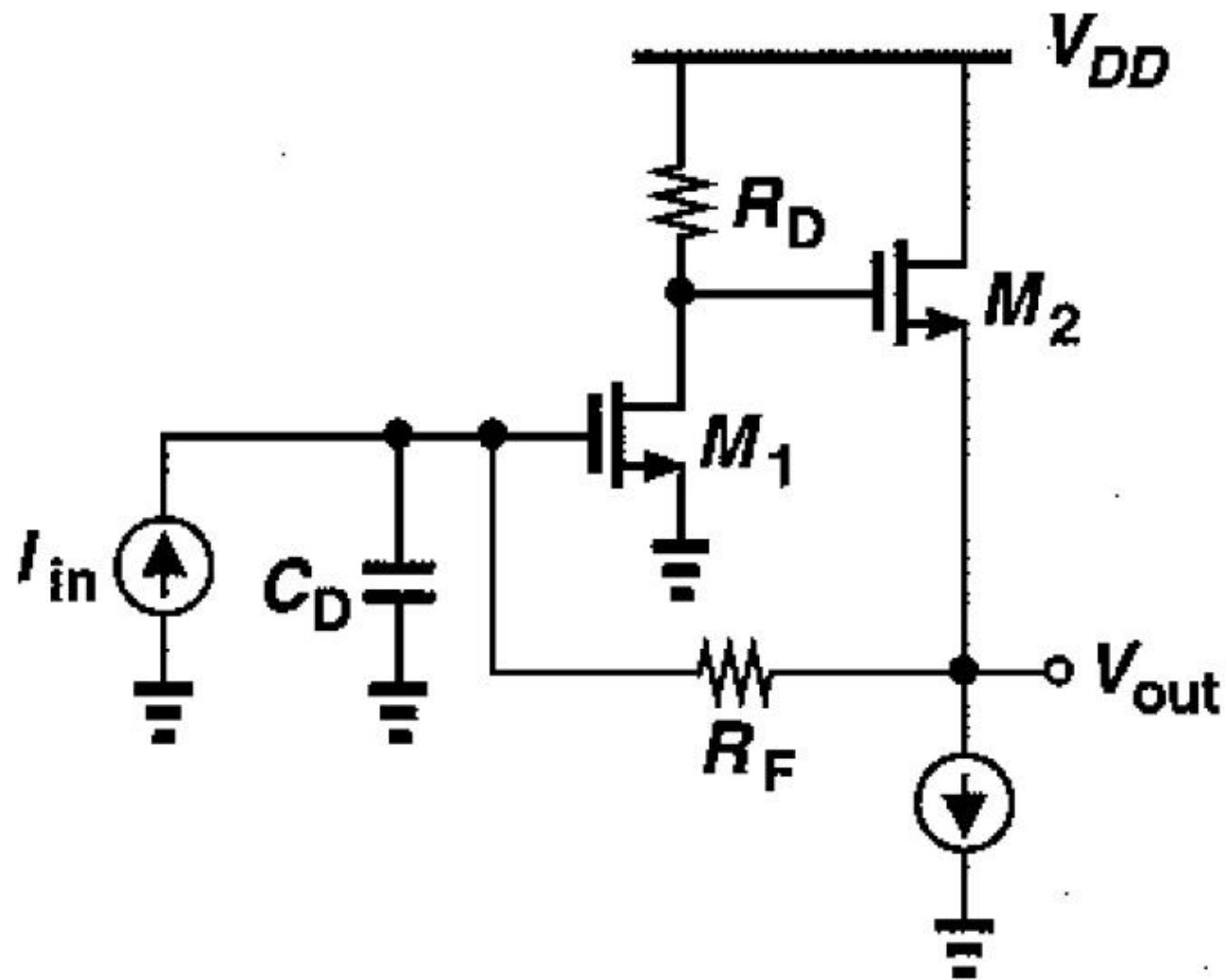
(b)

# Amplificatoare transimpedanta

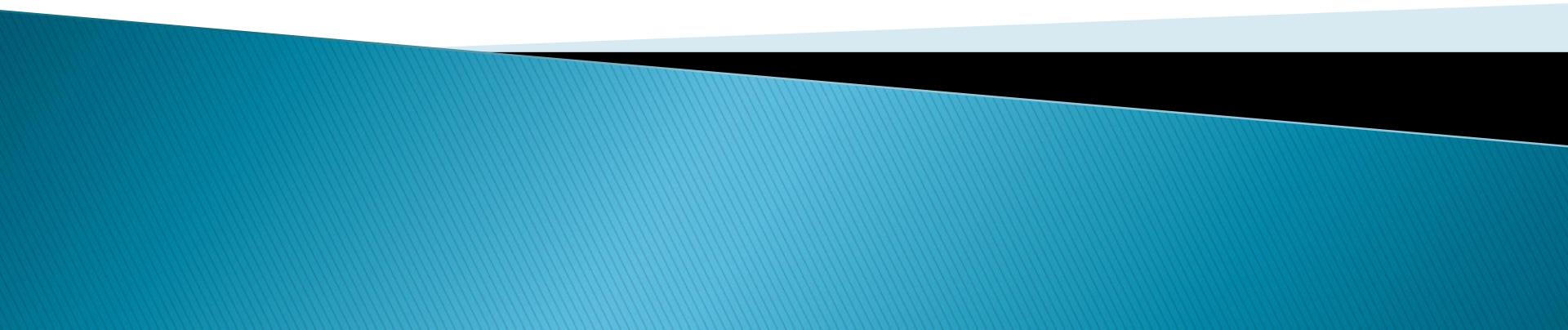
- ▶ Trebuie realizat un compromis intre
  - zgomot
  - castig
  - viteza
- ▶ De obicei sunt realizate cu reactie



# Amplificatoare transimpedanta



# Zgomotul traductorilor electro-optici



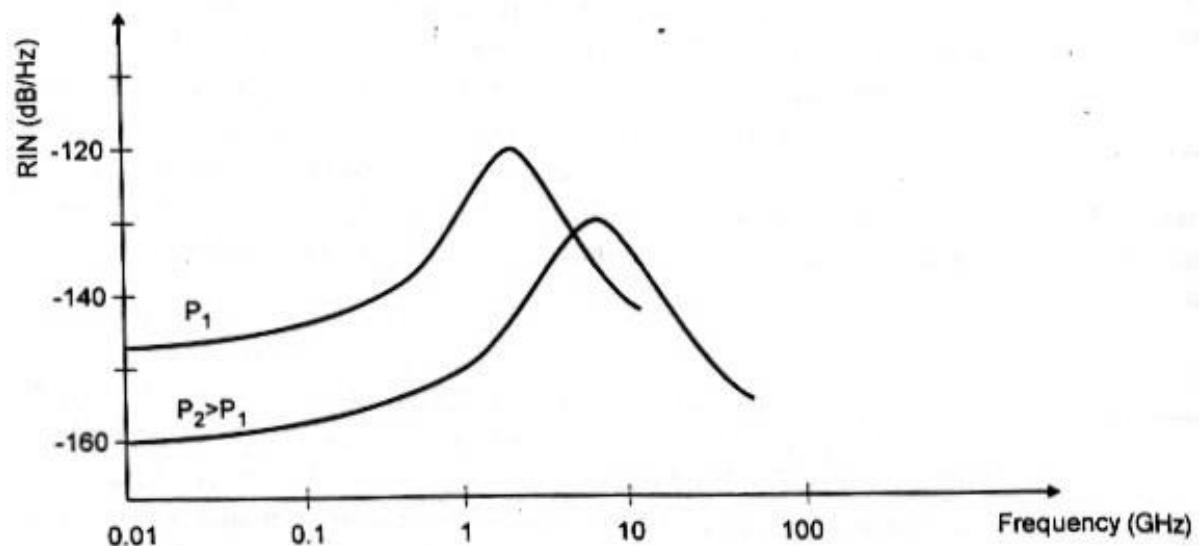
# Zgomotul emitorilor optici

- ▶ LED
  - este considerat o sursa lipsita de zgomot
  - nu contamineaza semnalul cu zgomot suplimentar
- ▶ Dioda LASER
  - fluctuatii de faza, determina o largire a spectrului emis
  - fluctuatii de intensitate, determina zgomotul de intensitate introdus de dioda
  - RIN – Relative Intensity Noise

$$RIN[1/Hz] = \frac{\langle P_n^2 \rangle}{\langle P^2 \rangle \cdot BW}$$

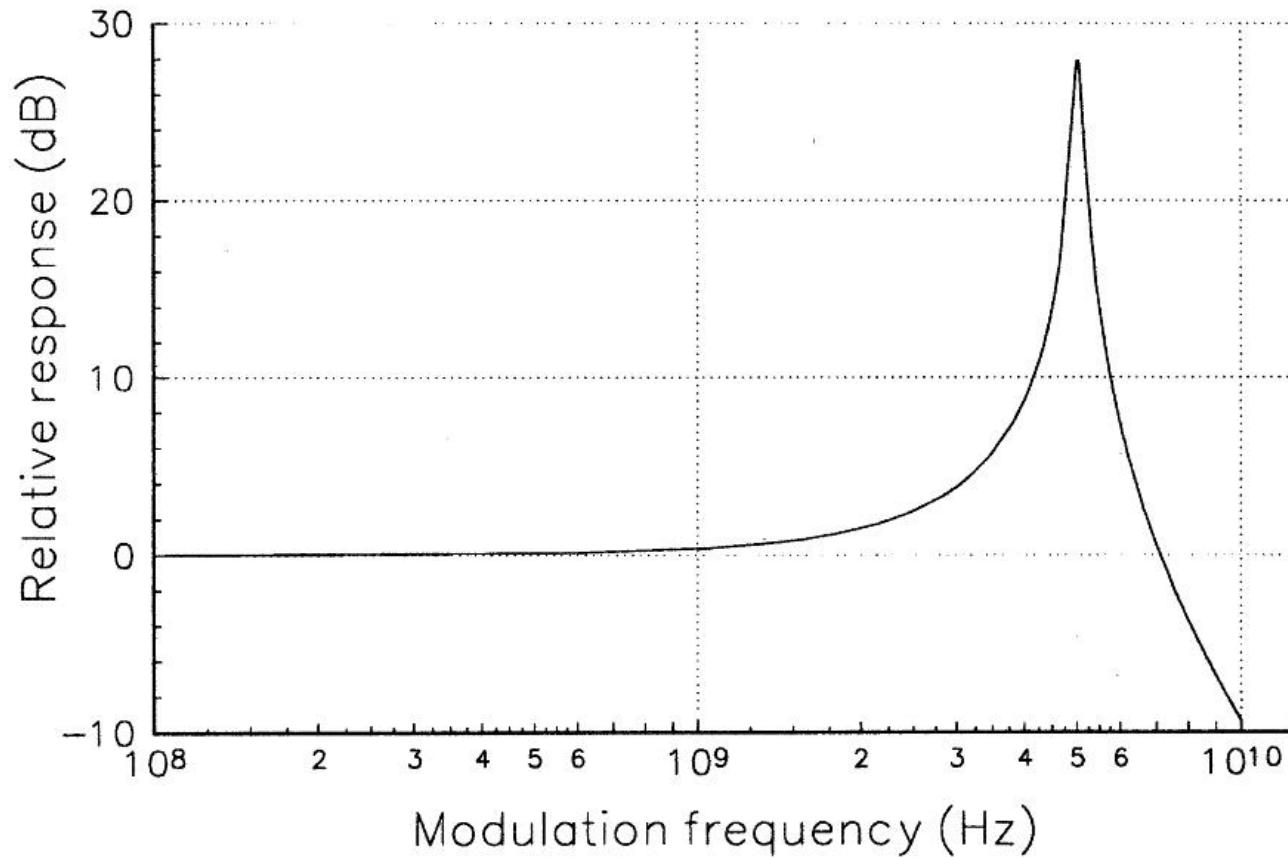
# RIN

- ▶ reprezinta o densitate spectrala de zgomot
  - puterea de zgomot depinde de RIN si de banda semnalului
- ▶ Depinde de puterea semnalului
  - $P^{-3}$  la puteri mici,  $P^{-1}$  la puteri mari



# Raspunsul unei diode laser

- ▶ oscilatii de relaxare - x GHz



# EIN

## ▶ Equivalent Input Noise

- $R_i$  – rezistenta de intrare in circuitul de modulatie a diodei
- Variatiile de putere (zgomot) echivalente unor variatii de curent (zgomot) prin dioda

$$\langle P_n^2 \rangle = r \cdot \langle I_n^2 \rangle$$

$$EIN[W] = R_i \cdot \langle I_n^2 \rangle \quad 1 \text{ Hz banda}$$

$$EIN[W / Hz] = RIN \cdot (I_0 - I_{th})^2 \cdot R_i$$

# Zgomotul fotodiodei

## ▶ NEP

- Noise Equivalent Power
- r – rezonabilitatea diodei

$$NEP[W] = \frac{\int \sqrt{\langle i_n^2 \rangle} df}{r}$$

- r depinde de  $\lambda$ , implica NEP depinde de  $\lambda$
- În cataloge apare de obicei densitatea spectrală

$$NEP[W / \sqrt{Hz}] = \frac{\sqrt{\langle i_n^2 \rangle}}{r} = \frac{NEP}{\sqrt{BW_{PD}}}$$

# Zgomotul fotodiodei

- ▶ NEP
  - cea mai mica putere detectabila

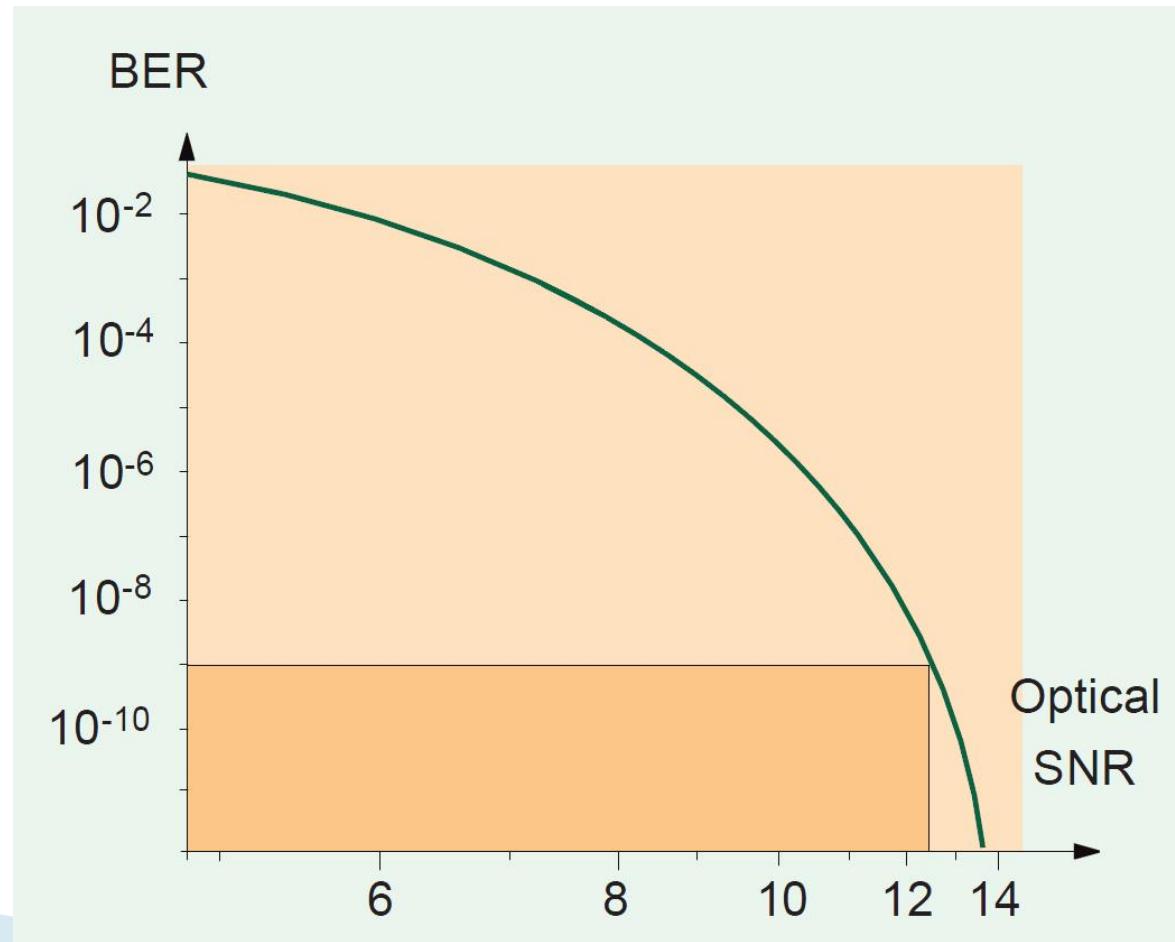
$$\langle i_n^2 \rangle = 2 \cdot e \cdot I \cdot BW_{PD} = 2 \cdot e \cdot (I_S + I_{dark}) \cdot BW_{PD}$$

$$P_{\min} = \frac{\sqrt{\langle i_n^2 \rangle_{\min}}}{r} = \frac{1}{r} \cdot \sqrt{2 \cdot e \cdot I_{dark} \cdot BW_{PD}}$$

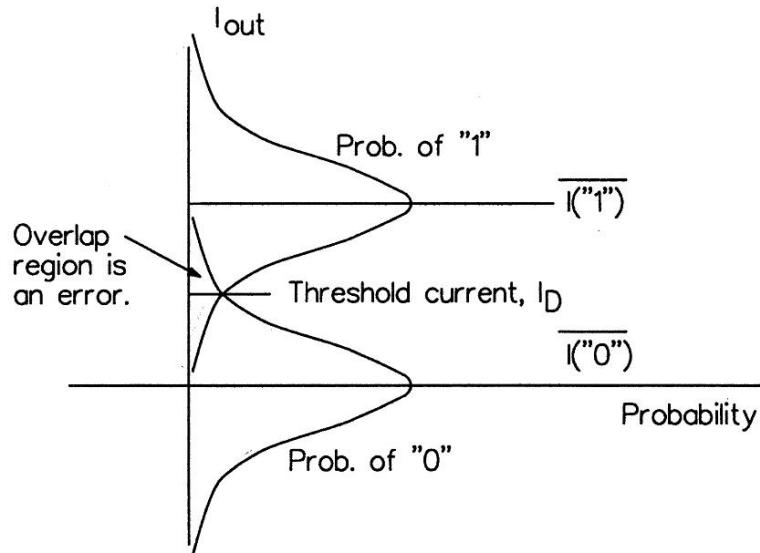
$$NEP[W / \sqrt{Hz}] = \frac{1}{r} \cdot \sqrt{2 \cdot e \cdot I_{dark}}$$

# BER

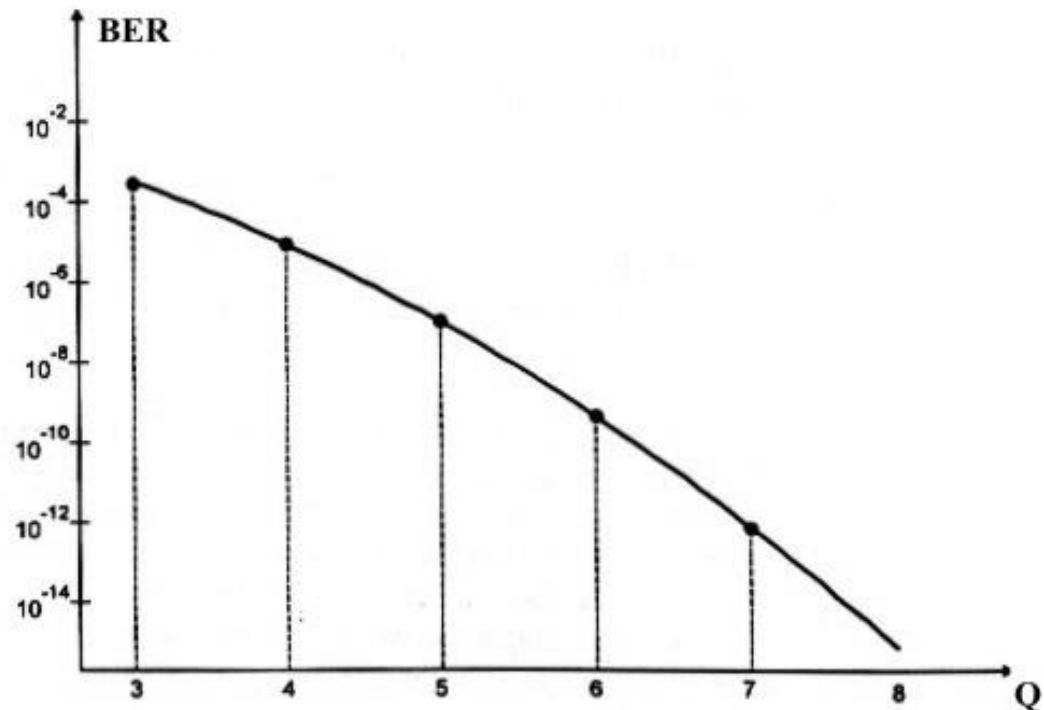
## ▶ Bit Error Rate



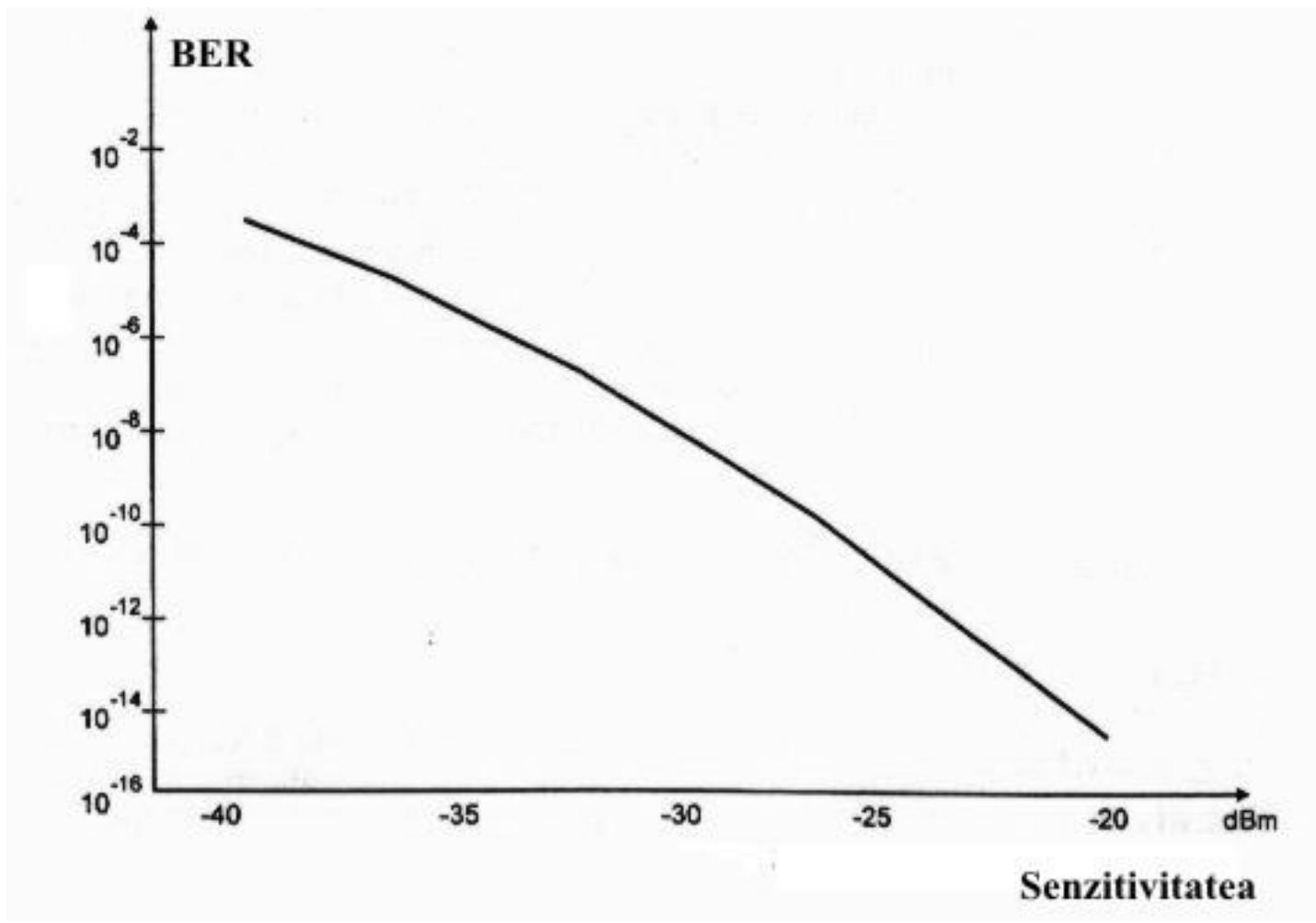
# Probabilitate de eroare



$$Q = \frac{\bar{i}(1) - I_D}{\sigma_1} = \frac{I_D - \bar{i}(0)}{\sigma_0}$$



# Senzitivitatea unei diode



# **Utilizare celule solare**

**Capitolul 10**

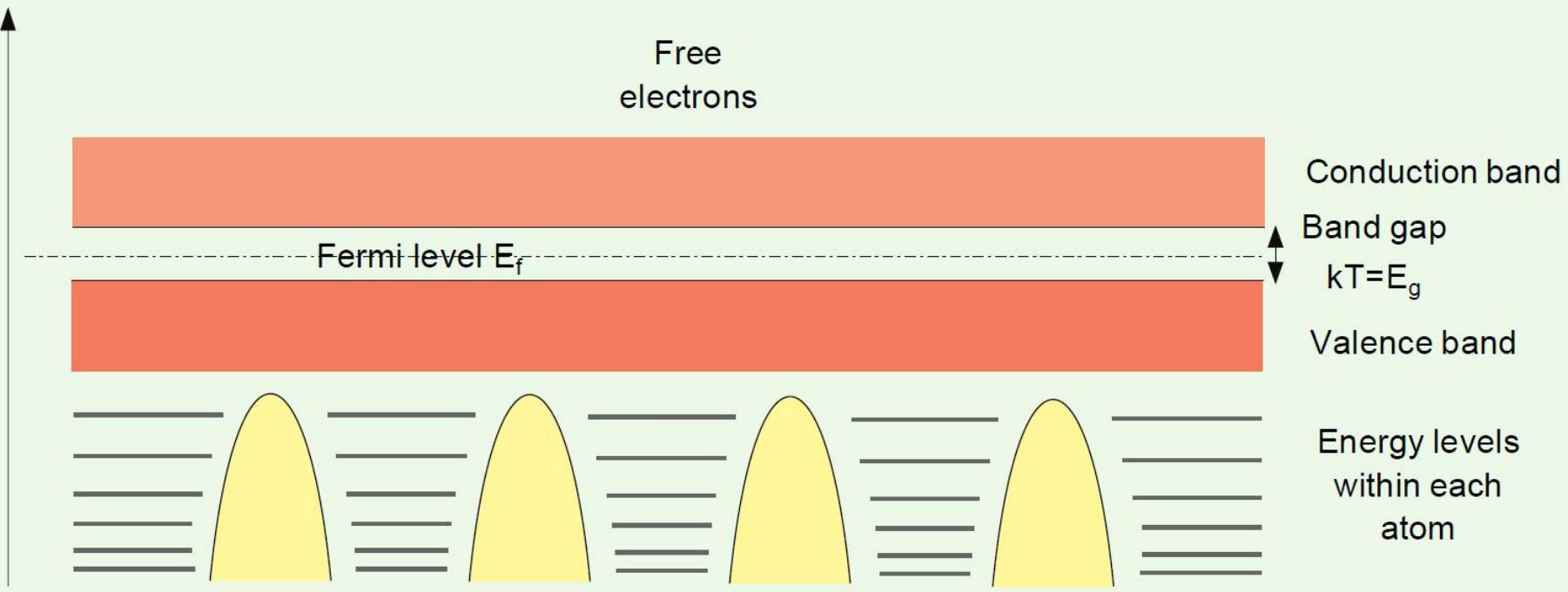
# Cuprins

- ▶ **Lumina ca undă electromagnetică** (ecuațiile lui Maxwell, ecuația undelor, parametrii de propagare)
- ▶ **Elemente de fotometrie și radiometrie** (mărimi energetice/luminoase)
- ▶ **Fibra optică** (realizare, principiu de funcționare, atenuare, dispersie, banda de frecvență)
- ▶ **Cabluri optice** (tehnologie, conectori, lipire – splice)
- ▶ **Proiectare sistemică a legăturii pe fibra optică** (bandă de frecvență, balanță puterilor)
- ▶ **Emițătoare optice** (LED și dioda laser – realizare fizică și funcționare)
- ▶ **Receptoare optice** (dioda PIN, dioda cu avalanșă – realizare fizică și funcționare)
- ▶ **Amplificatoare transimpedanță** (parametri, scheme tipice, TIA în buclă deschisă, cu reacție, diferențiale, control automat al câștigului)
- ▶ **Realizarea circuitelor pentru controlul emițătoarelor optice** (parametri, scheme tipice, controlul puterii, multiplexoare)
- ▶ **Dispozitive de captare a energiei solare** (principiu de funcționare, utilizare, proiectare )

# Efect fotovoltaic

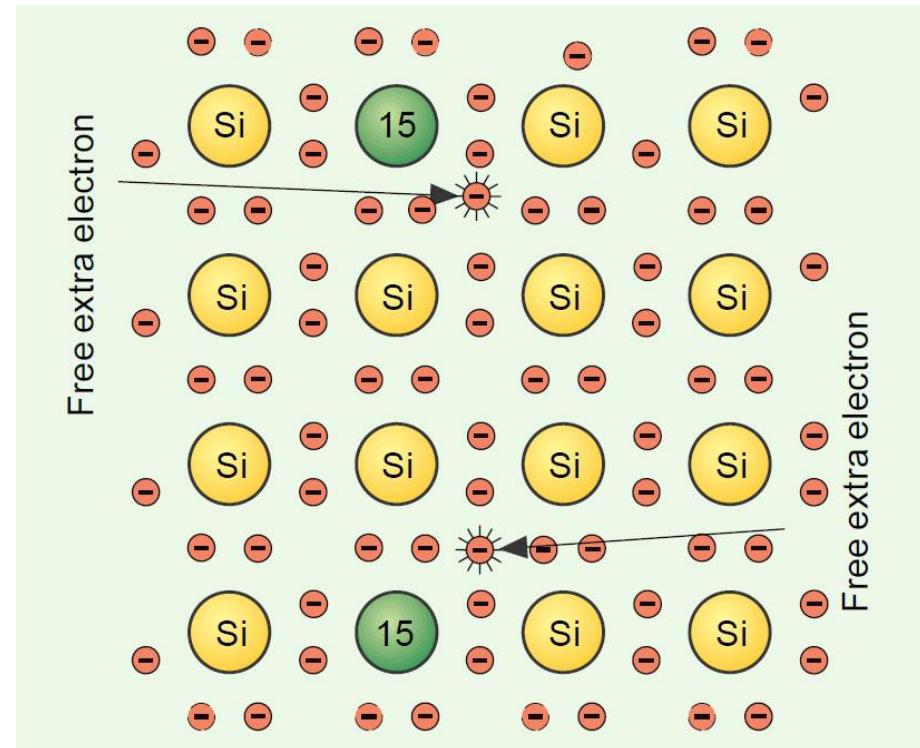
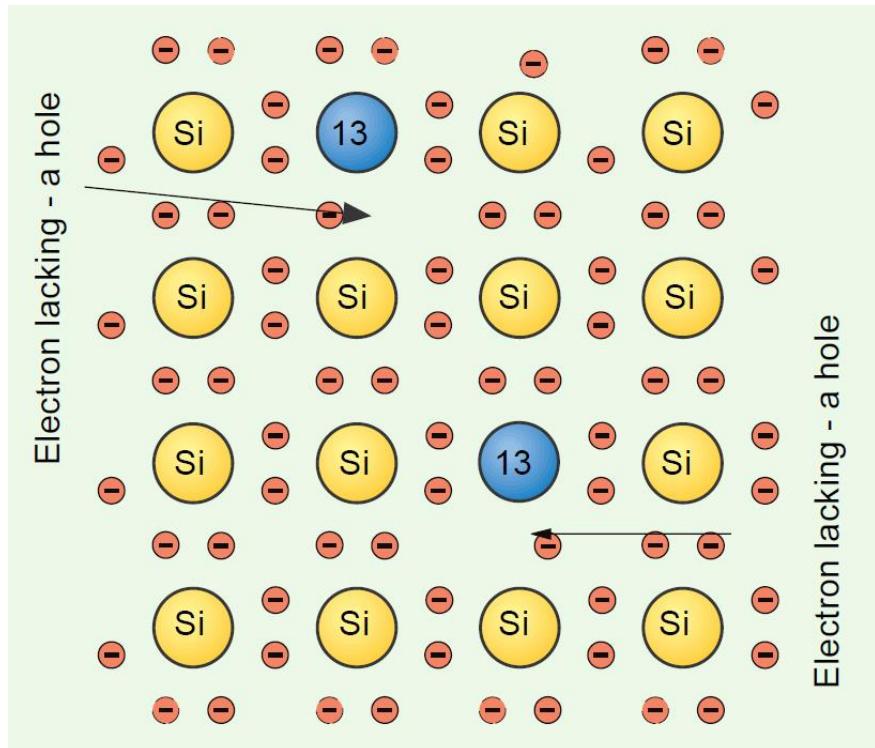
## ▶ joncțiunea pn

Energy level



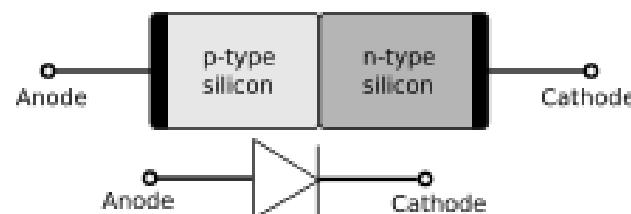
# Efect fotovoltaic

## ► joncțiunea pn

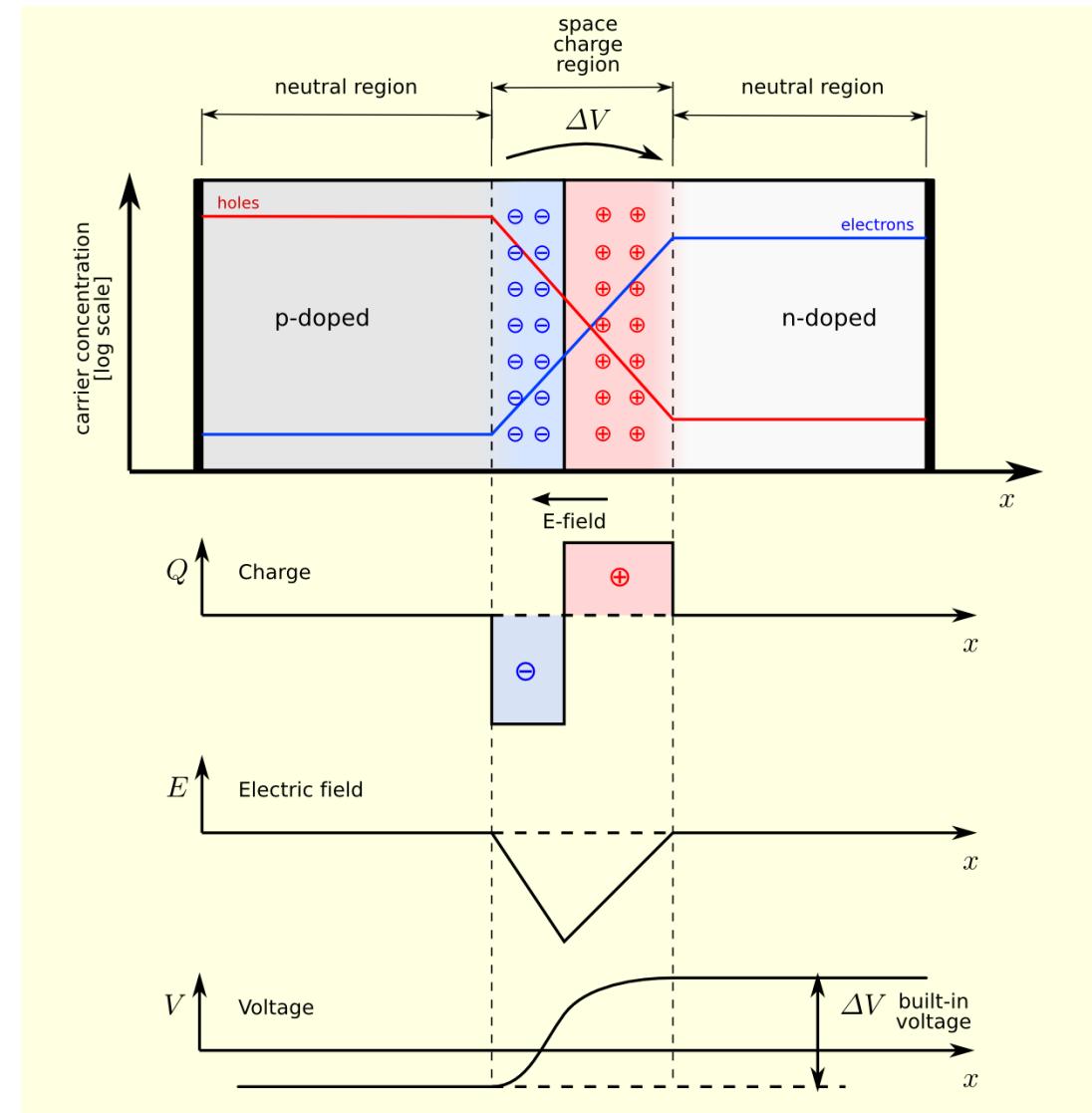


# Efect fotovoltaic

## ▶ joncțiunea pn

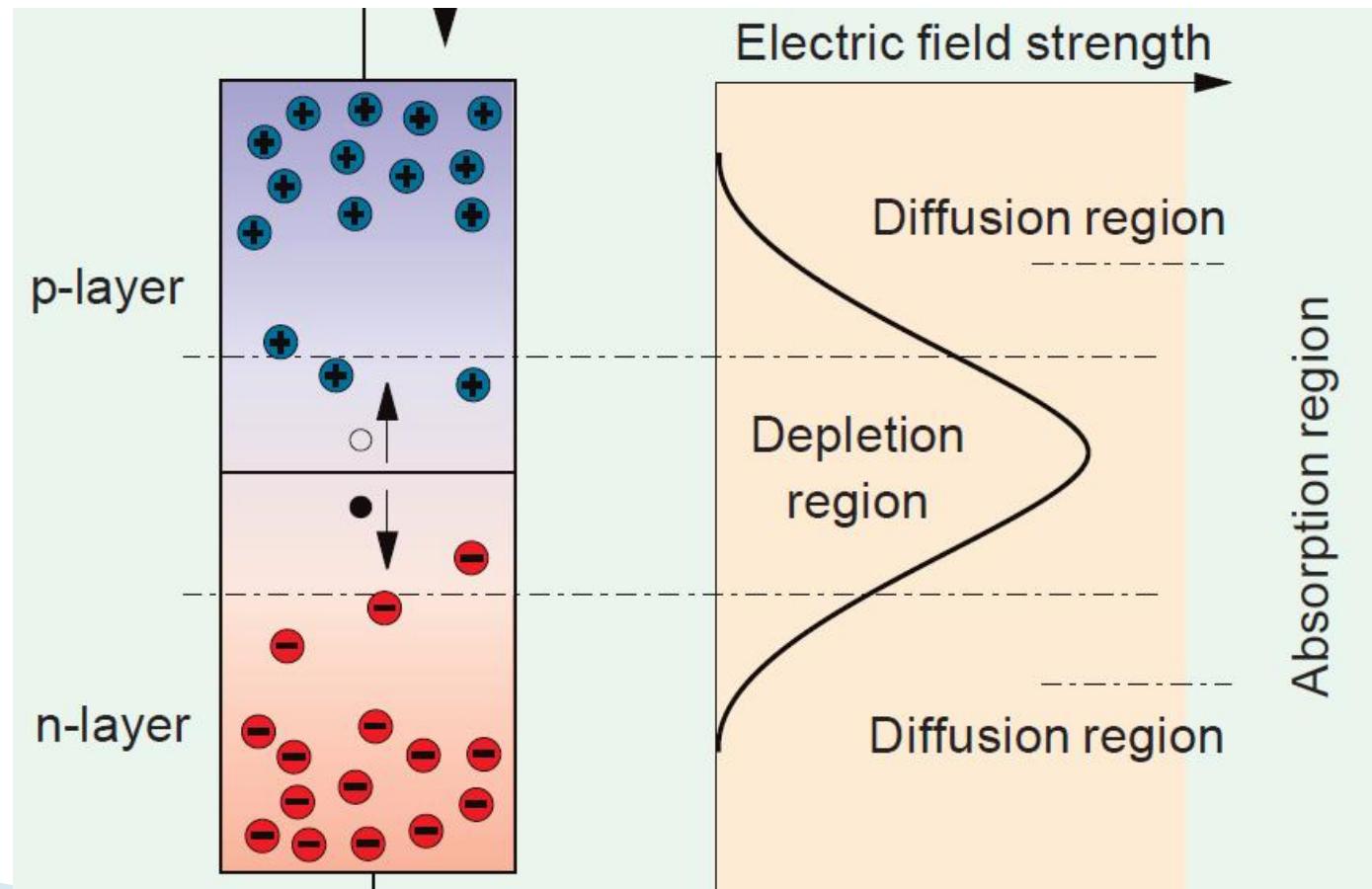


$$V > V_D$$



# Efect fotovoltaic

## ▶ joncțiunea pn / Fotodioda

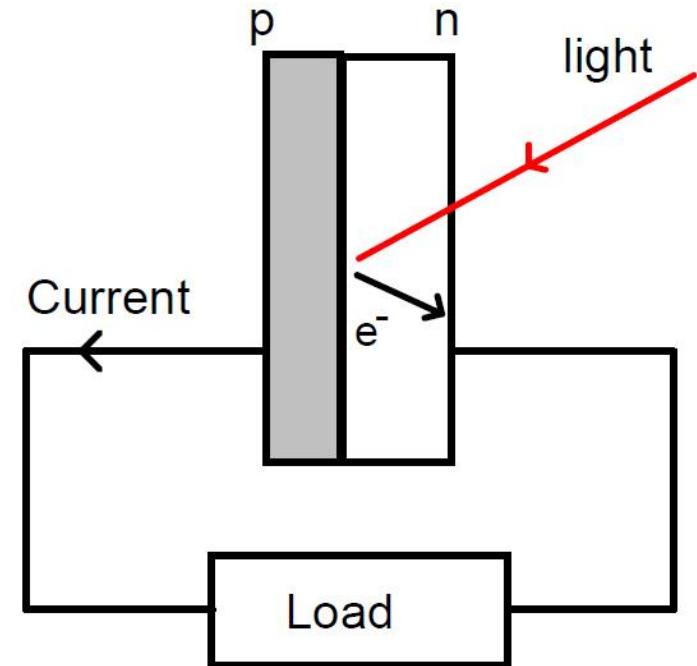
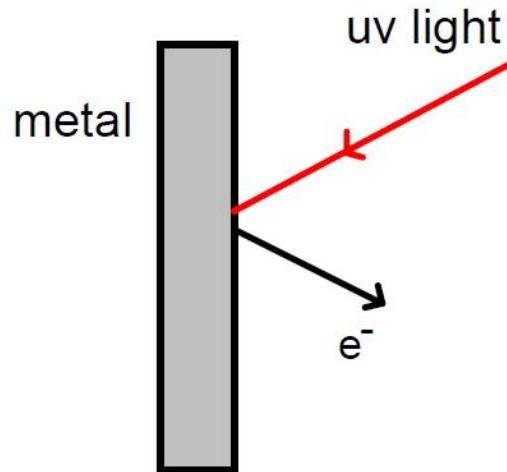


# Efect fotovoltaic

- ▶ generarea unei perechi electron/gol în interiorul unui material prin absorbtia energiei fotonilor incidenti și creșterea energiei potențiale a electronilor
  - urmat de posibilitatea separării sarcinilor
- ▶ deosebit de conversia:
  - fototermica (energia fotonilor este convertită în căldură – energie cinetică a electronilor)
  - fotochimica (fotosinteza energie potențială utilizată chimic)
- ▶ duce la apariția unei tensiuni electromotoare și a unui curent într-un circuit închis

# Efect fotovoltaic

- ▶ diferit de efectul fotoelectric (cu toate ca este asemanator ca principiu)



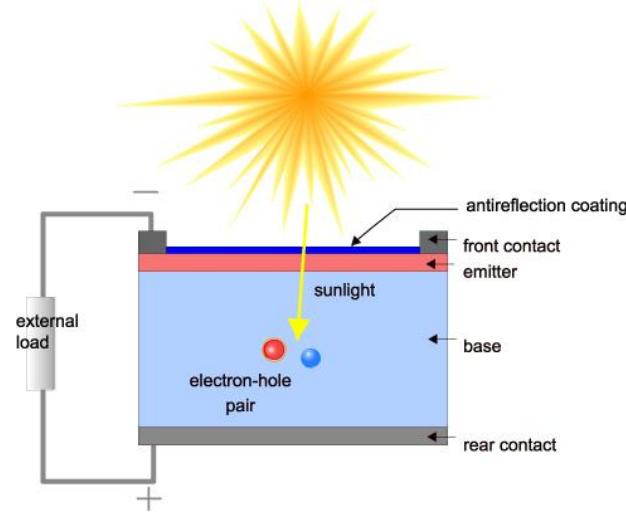
# Efect fotovoltaic

- ▶ Separarea fizica a sarcinilor este de obicei realizata prin utilizarea unei jonctiuni pn:
  - campul electric generat de distributia sarcinilor in zona golita de portatori a jonctiunii
- ▶ In principiu o **celula solară** este o **fotodiode** in care:
  - nivelul de semnal optic este ridicat (fortarea prin polarizare inversa externa a extragerii tuturor electronilor generati nu e necesara)
  - viteza de lucru nu e importanta (accelerarea iesirii din dispozitiv a electronilor generati nu e necesara)

# Celula solară (fotovoltaica)

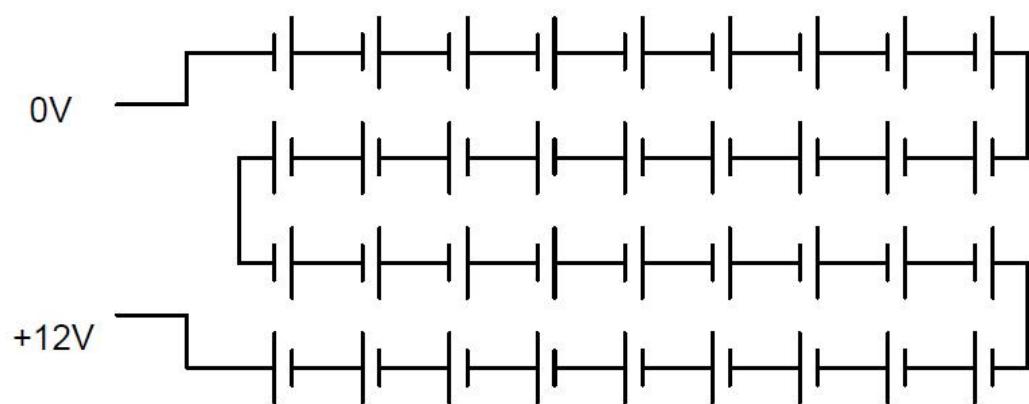
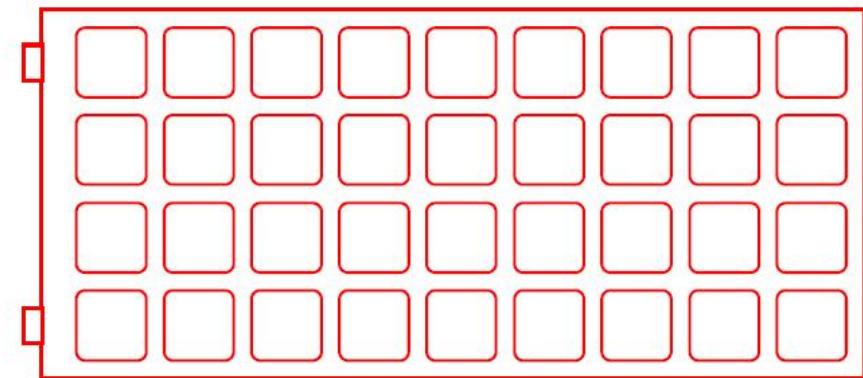
► în principiu o dioda

- cu arie mare ( $\sim 100\text{cm}^2$ )
- cu suprafață tratată antireflectorizant
- generează o tensiune electromotoare de  $0.5\div 1\text{V}$
- generează curenti de scurtcircuit de  $x0 \text{ mA/cm}^2$



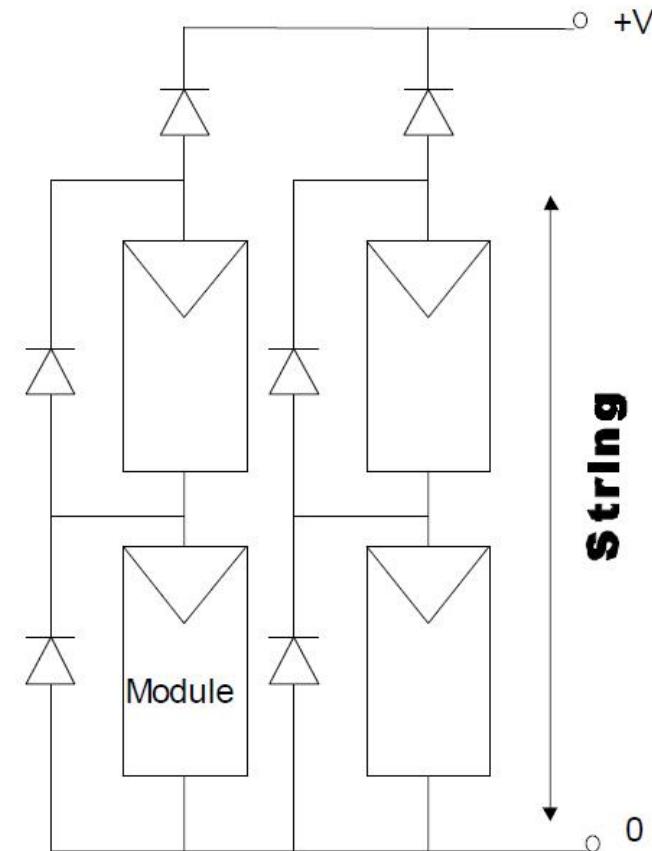
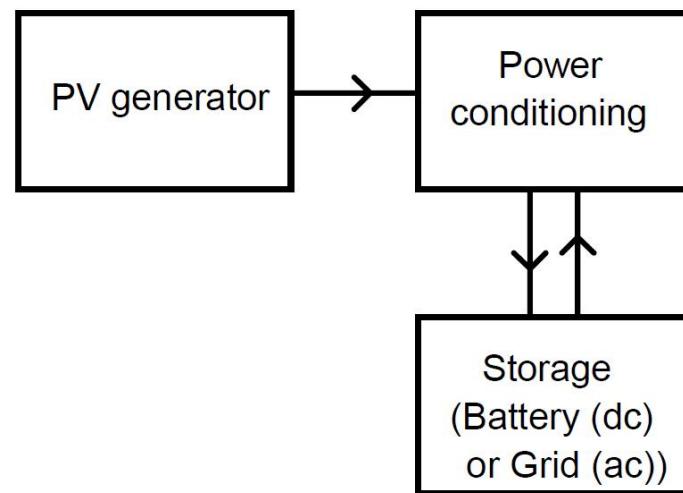
# Celula solară (fotovoltaica)

- ▶ pentru utilizare în practică
  - module de 28 – 36 de celule conectate în serie
  - crește tensiunea la 12V (tipic)



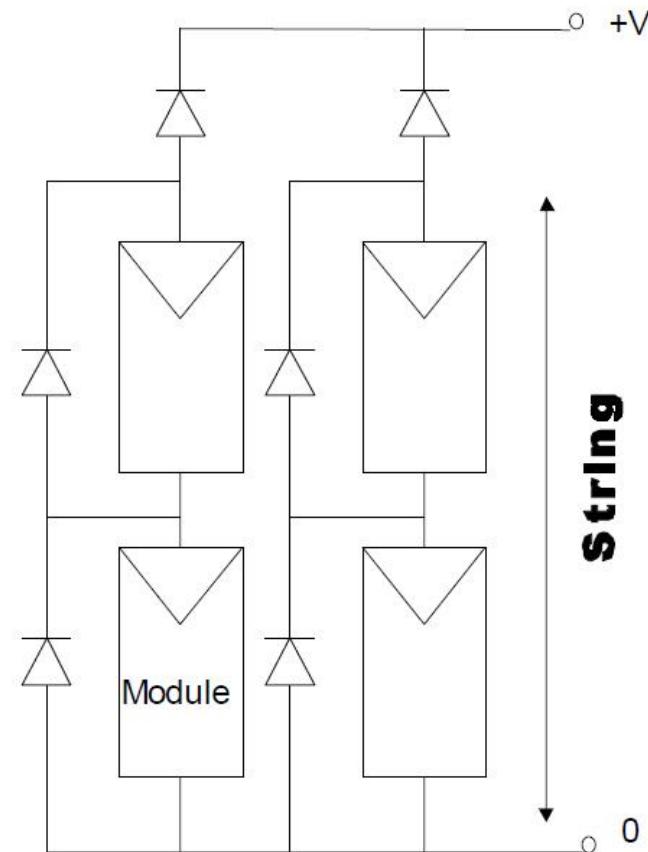
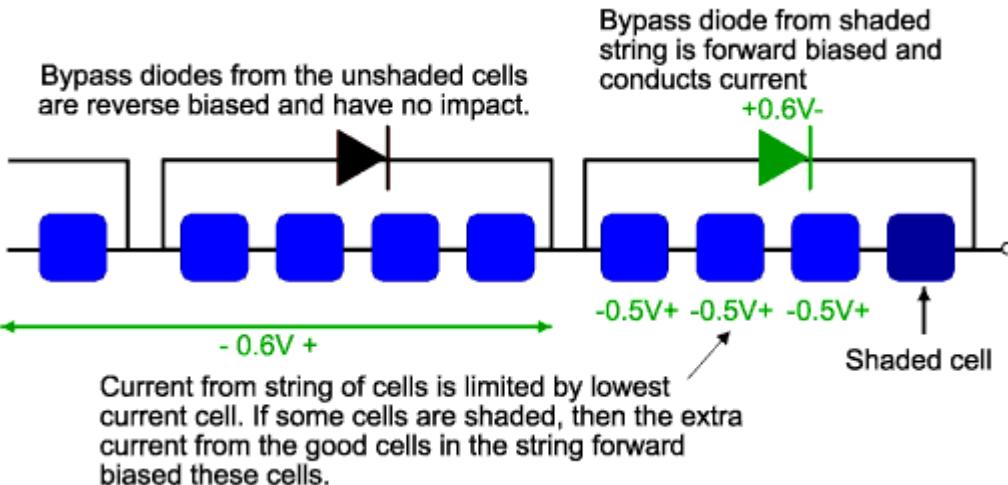
# Celula solara (fotovoltaica)

- ▶ pentru utilizare in practica
  - modulele sunt conectate in serie si/sau paralel pentru obtinerea tensiunilor/urentilor necesari pentru aplicatie



# Celula solara (fotovoltaica)

- ▶ pentru utilizare in practica
  - diode pentru flexibilitate



# Celula solara (fotovoltaica)

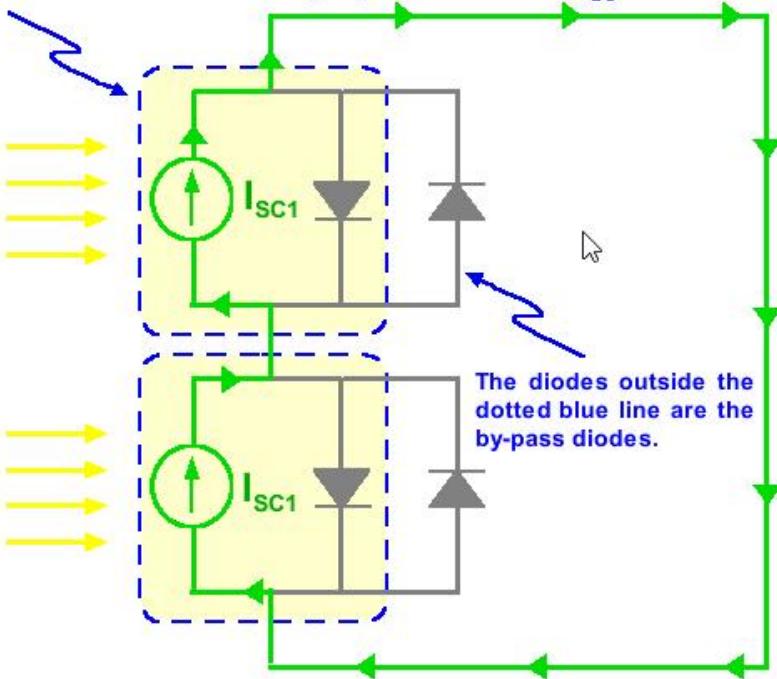
## ▶ Diode bypass

### SERIES CONNECTED SOLAR CELLS WITH BYPASS DIODES

- Matched currents at short circuit
- Mismatched currents at short circuit
- Matched currents at open circuit
- Mismatched currents at open circuit

At short circuit conditions and with matched currents, the voltage across both the solar cells and the bypass diodes is zero. The bypass diodes have no effect.

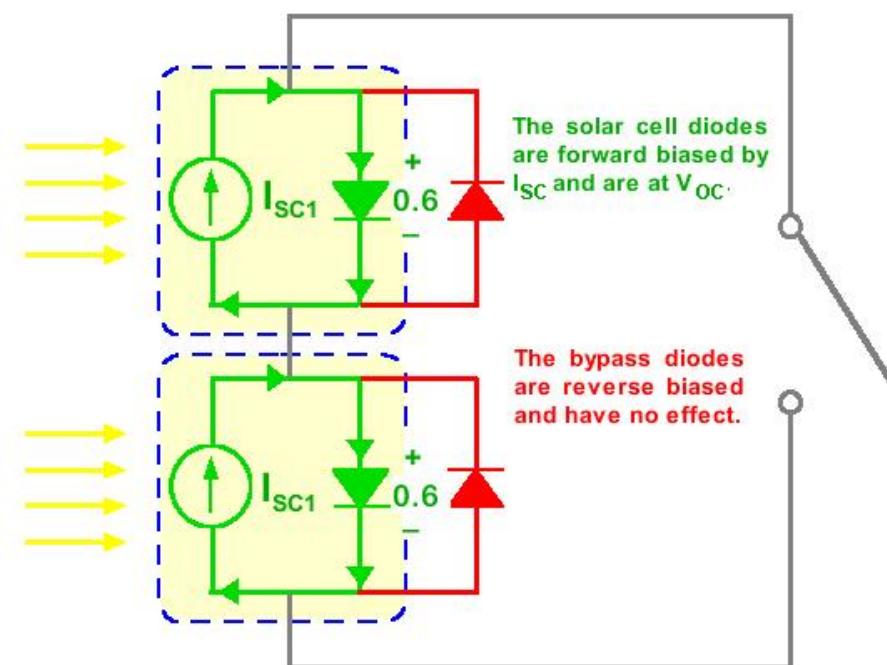
The circuit elements contained within the blue dotted lines model a solar cell. The current source is the light generated current,  $I_{SC}$ .



### SERIES CONNECTED SOLAR CELLS WITH BYPASS DIODES

- Matched currents at short circuit
- Mismatched currents at short circuit
- Matched currents at open circuit
- Mismatched currents at open circuit

At open circuit conditions and with matched currents, the short circuit current from each solar cell forward biases the solar cell. The bypass diodes are reverse biased and have no effect on the circuit.



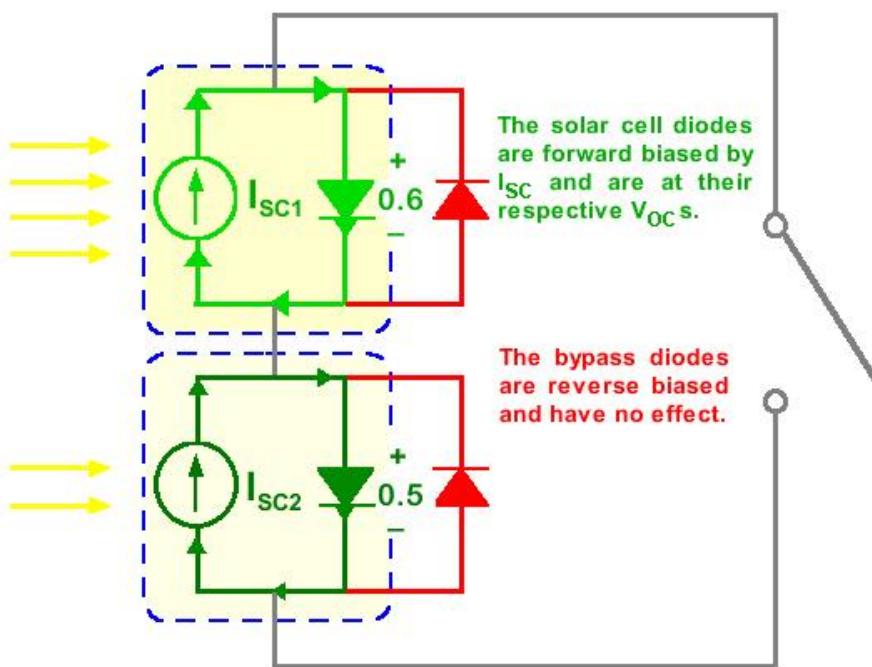
# Celula solara (fotovoltaica)

## ▶ Diode bypass

### SERIES CONNECTED SOLAR CELLS WITH BYPASS DIODES

- Matched currents at short circuit
- Mismatched currents at short circuit
- Matched currents at open circuit
- Mismatched currents at open circuit

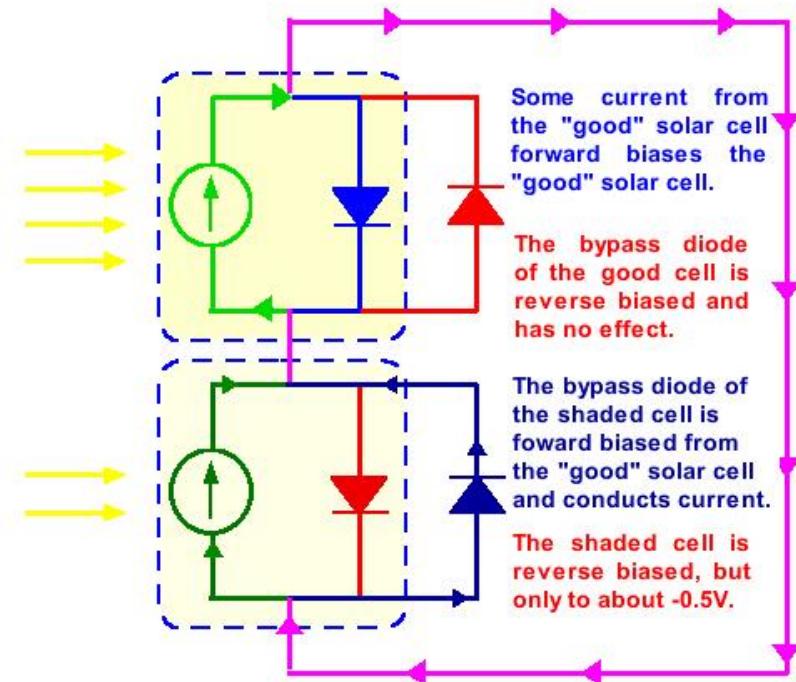
At open circuit conditions and with mismatched currents, the shaded solar cell has a reduced  $V_{OC}$ . The by-pass diodes are reverse biased and have no effect.



### SERIES CONNECTED SOLAR CELLS WITH BYPASS DIODES

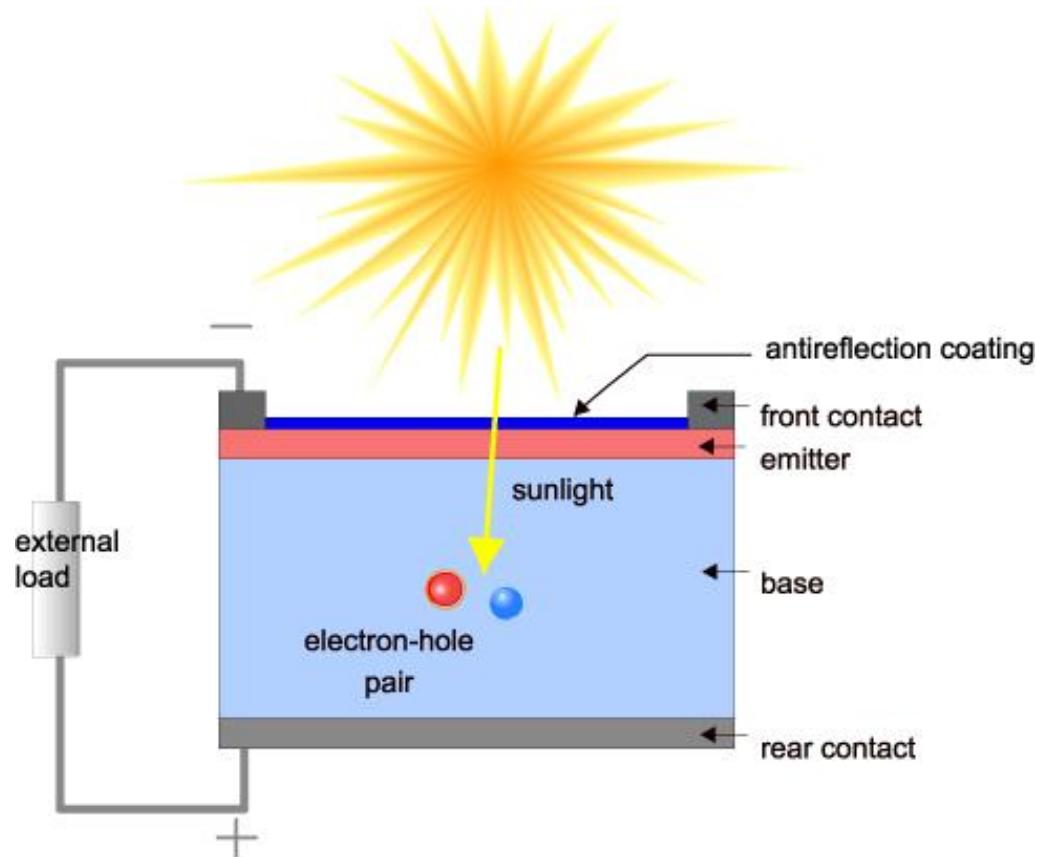
- Matched currents at short circuit
- Mismatched currents at short circuit
- Matched currents at open circuit
- Mismatched currents at open circuit

At short circuit with mismatched  $I_{SC}$ , some current flows across the "good" solar cell junction, forward biasing the "good" solar cell. This voltage in turn forward biases the by-pass diode of the shaded cell, allowing it to conduct current.



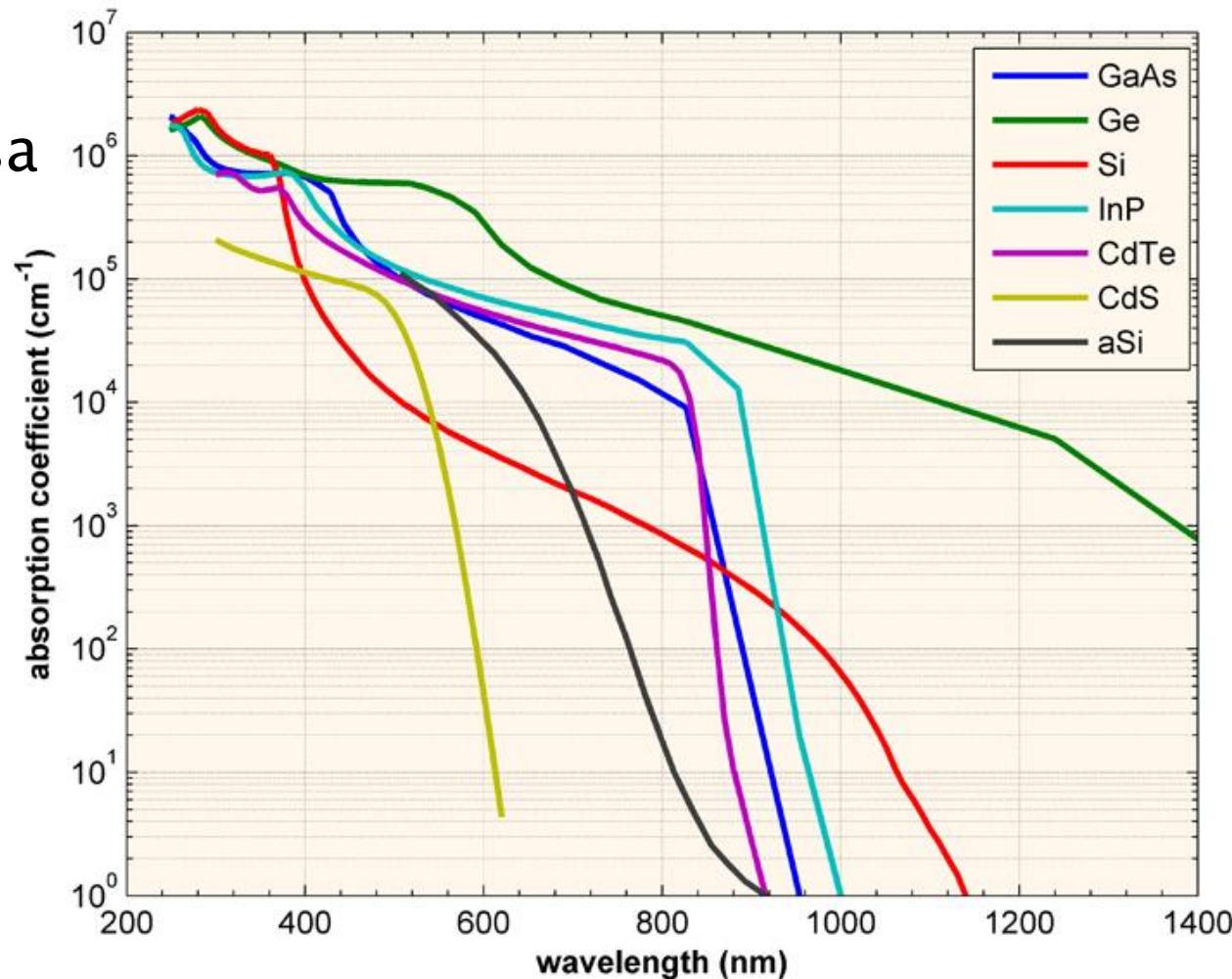
# Celula solară (fotovoltaica)

- ▶ în principiu o dioda



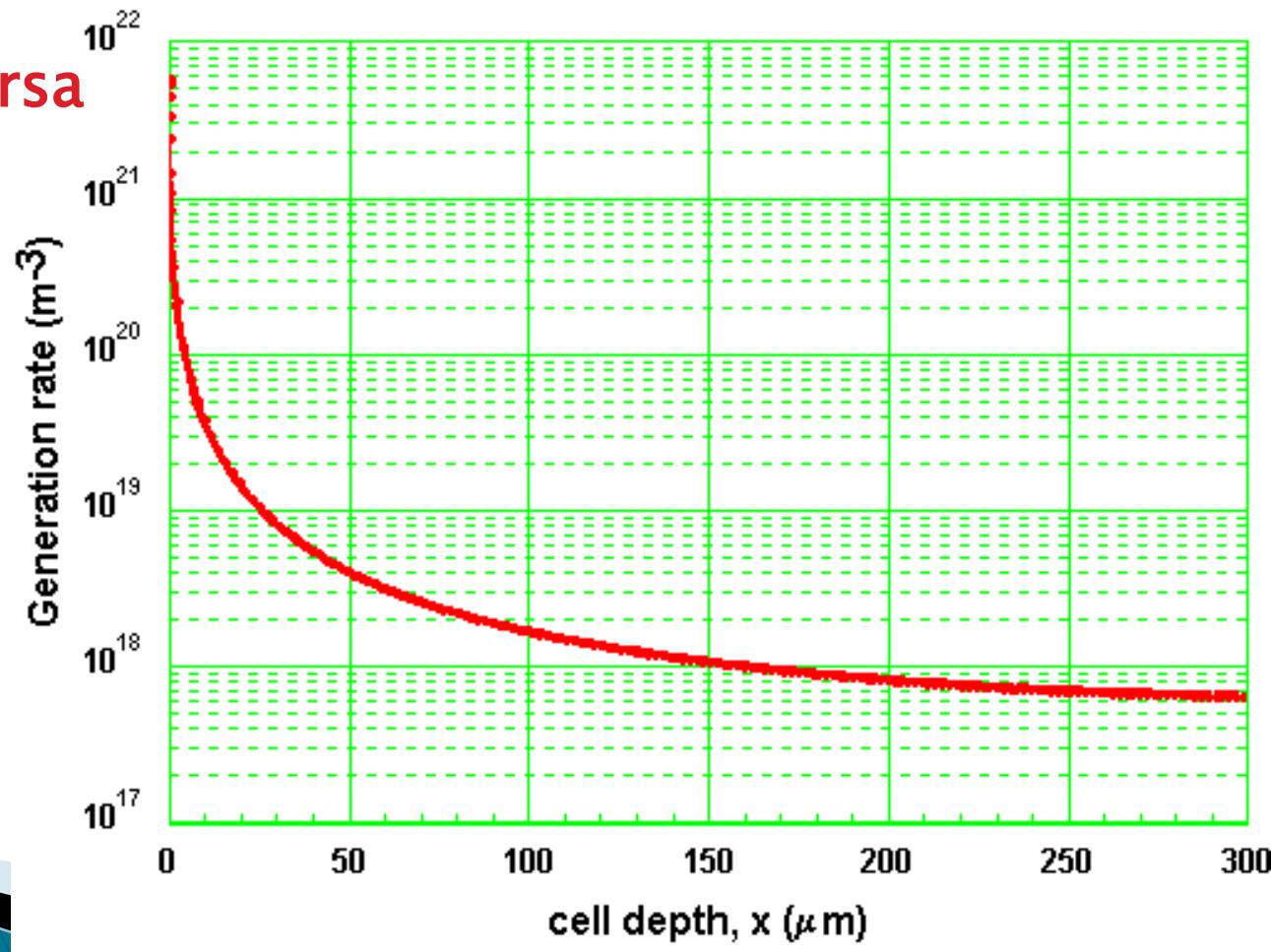
# Celula solară

- ▶ probabilitate de generare a purtatorilor depinde de
  - **material**
  - distanța parcursă



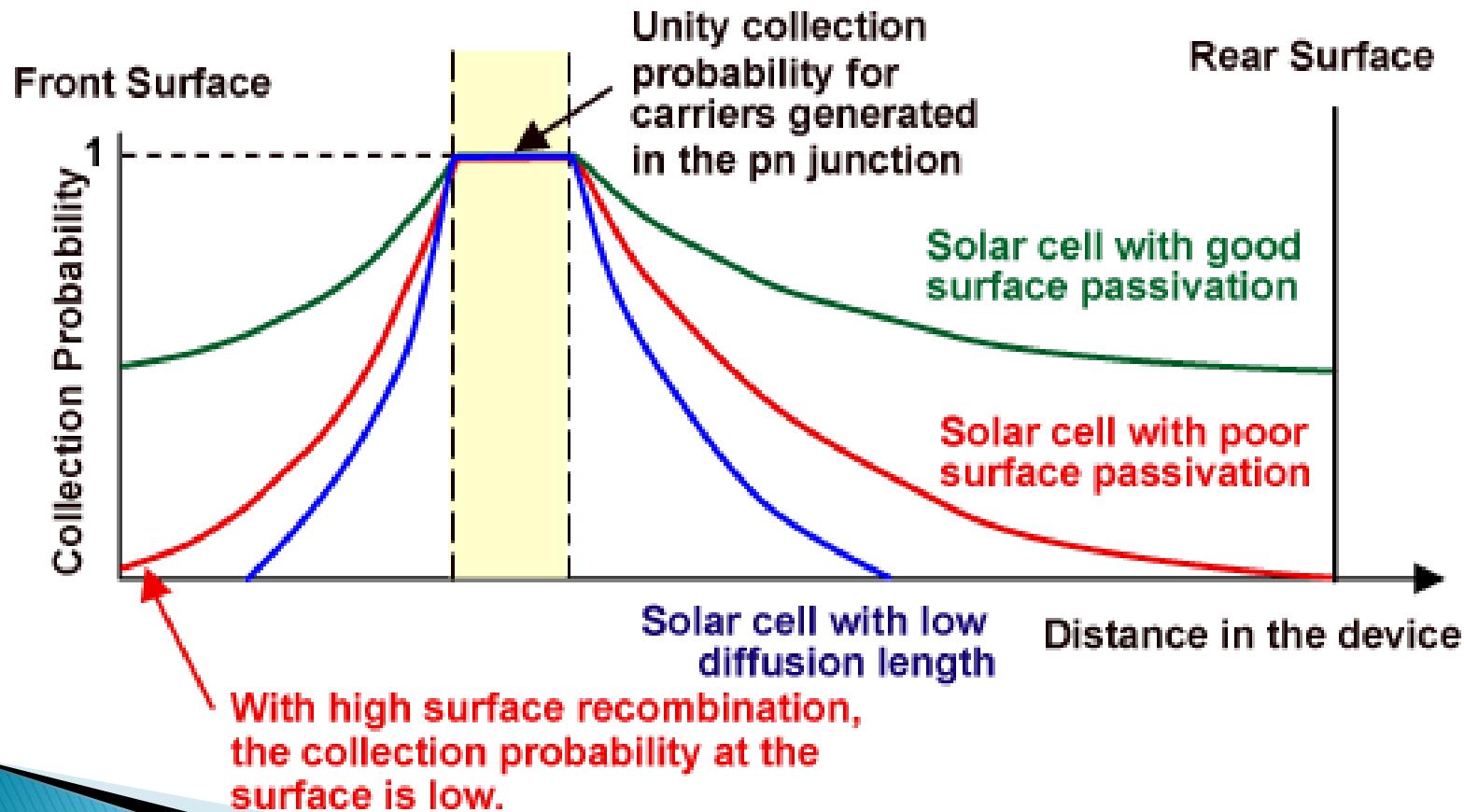
# Celula solara

- ▶ probabilitate de generare a purtatorilor depinde de
  - material
  - **distanța parcursă**



# Celula solara

- ▶ probabilitate de captura a purtatorilor



# Celula solară/Fotodioda

- ▶ Energia necesara pentru eliberarea unei perechi electron gol

$$h\nu = \frac{hc}{\lambda} \geq E_g$$

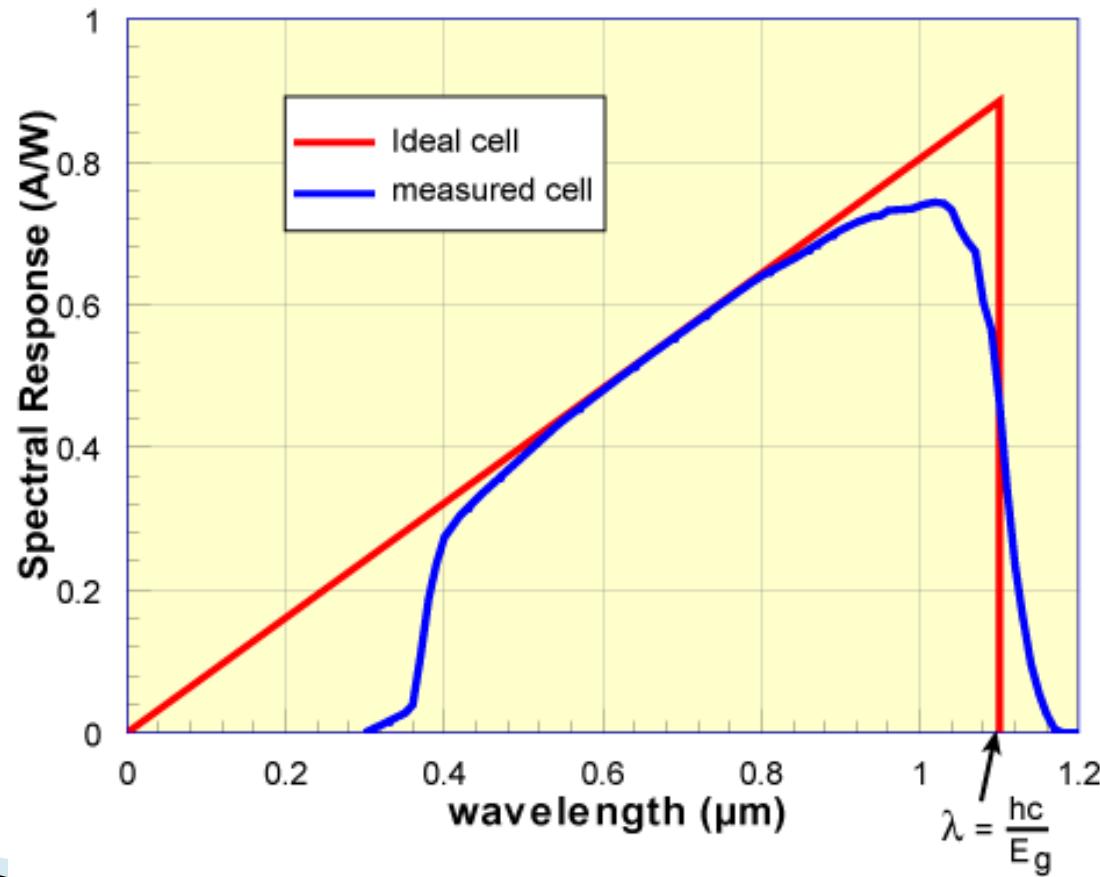
- ▶ Lungime de undă de taiere

$$\lambda_{\max} = \frac{hc}{E_g}$$

- ▶ Coeficientul de absorbtie are valoare mare la lungimi de undă reduse
- ▶ Ca urmare comportarea **tuturor** materialelor este de tip trece banda

# Celula solară

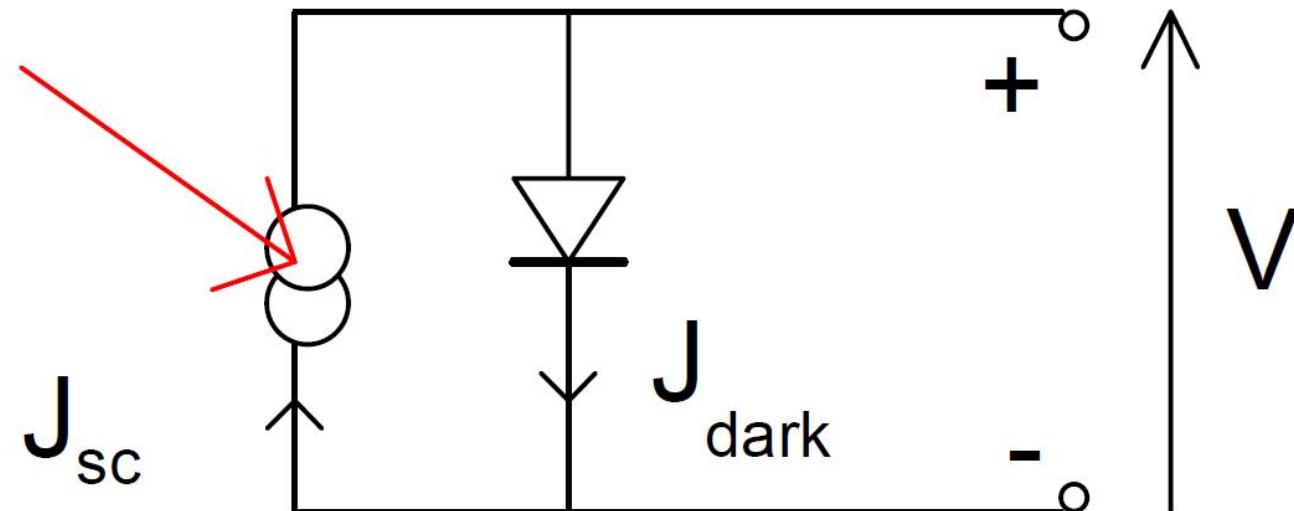
- ▶ raspuns spectral



# Celula solara

## ▶ Schema echivalenta

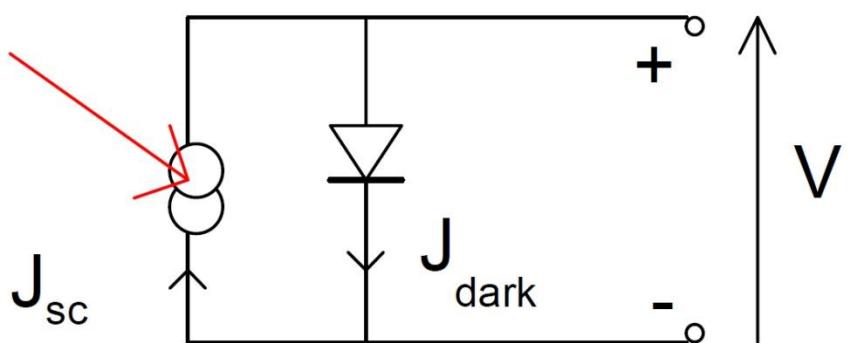
- dioda
- sursa de curent generat de fluxul de fotoni incident



# Celula solara

## ► Schema echivalenta

- dioda
- sursa de curent generat de iluminarea energetica incidenta
  - curent de intuneric



$$I_d(V) = I_0 \cdot (e^{eV/KT} - 1)$$

- adaugarea curentului generat de fotoni

$$I(E_e, V) = I_{sc}(E_e) - I_d(V)$$

- tensiunea in gol

$$V_{oc} = \frac{k \cdot T}{e} \cdot \ln \left( \frac{I_{sc}(E_e)}{I_0} - 1 \right)$$

# Celula solară

Current density,  $J$

$J_{sc}$

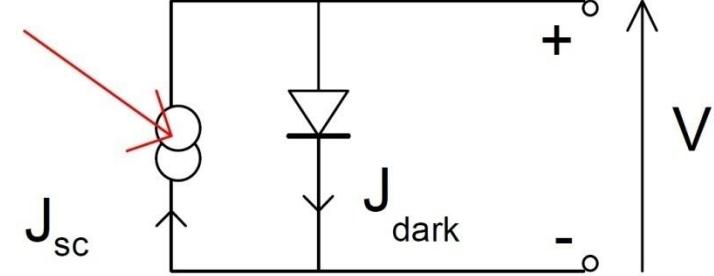
$$I(E_e, V) = I_{sc}(E_e) - I_d(V)$$

*Light current*

*Dark current*

$$I_d(V) = I_0 \cdot (e^{eV/KT} - 1)$$

Bias voltage,  $V$



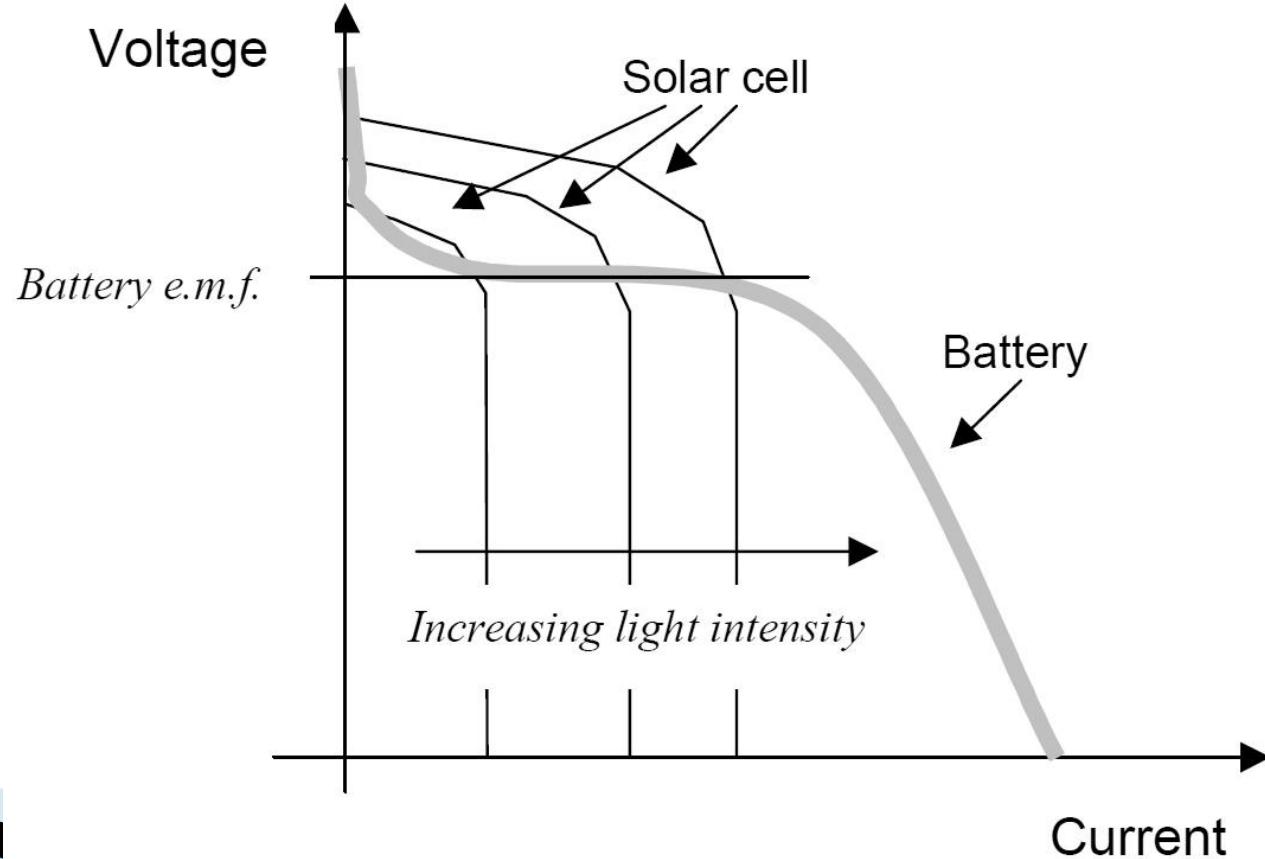
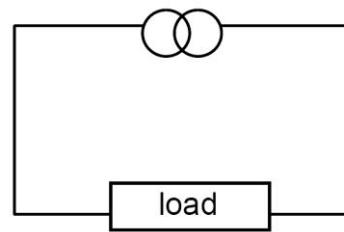
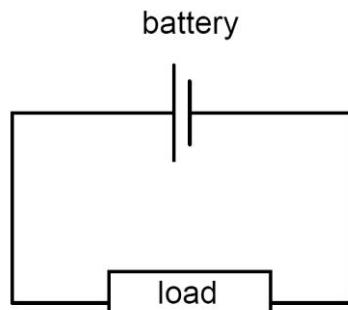
$J_{sc}$

$V_{oc}$

$$V_{oc} = \frac{k \cdot T}{e} \cdot \ln \left( \frac{I_{sc}(E_e)}{I_0} - 1 \right)$$

# Celula solara

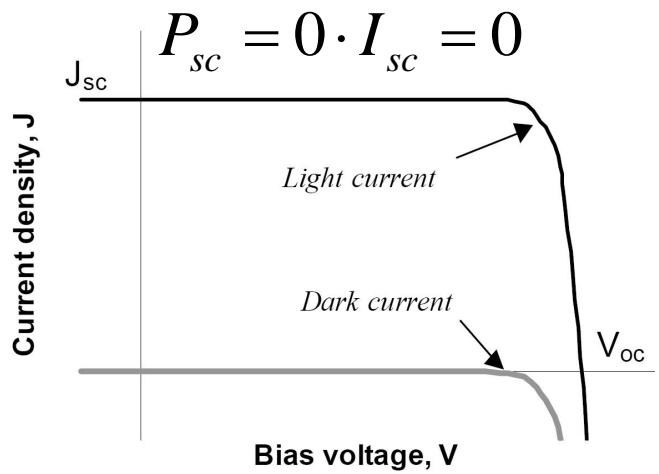
- ▶ poate fi folosita in loc de baterie intr-un circuit electric
  - cu anumite diferente



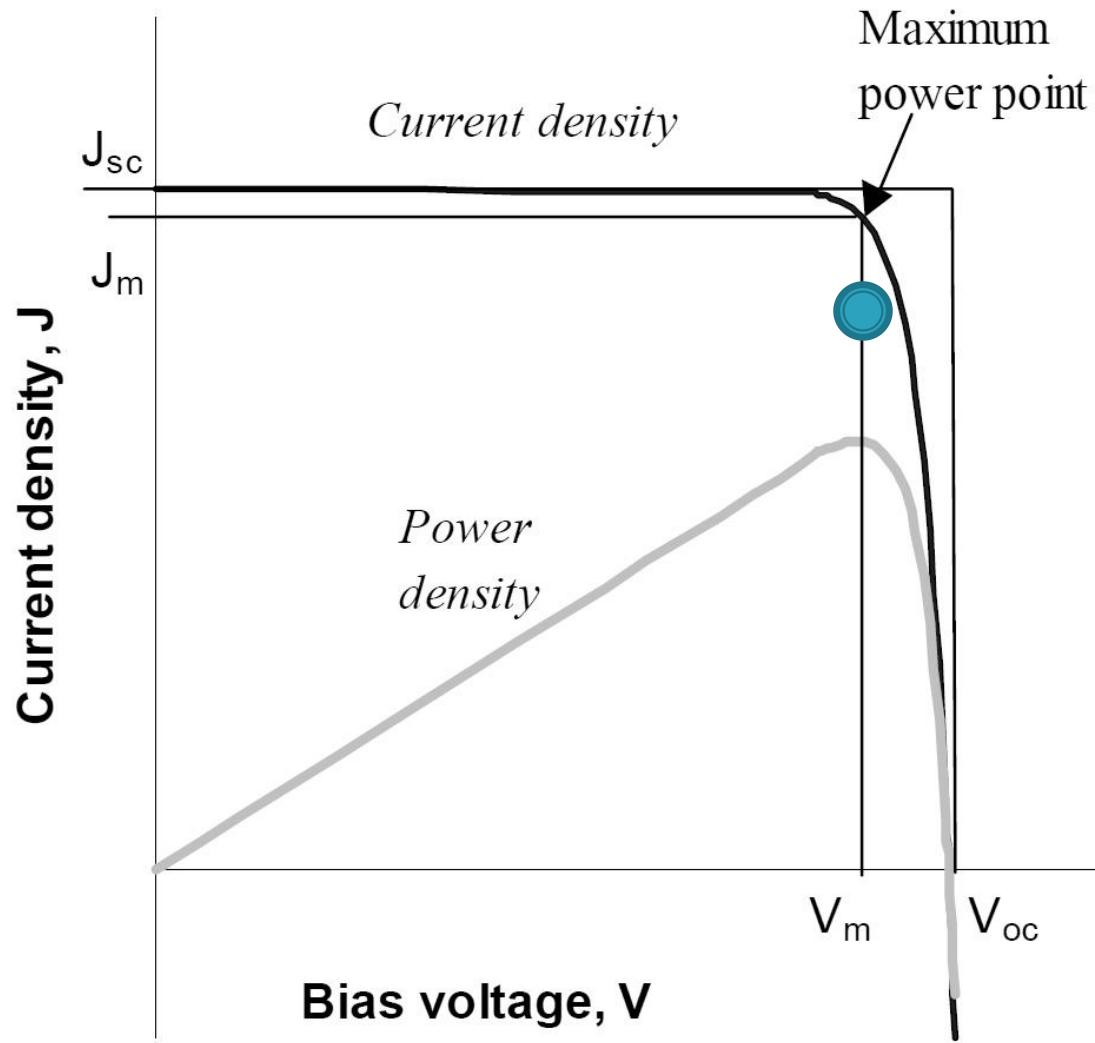
# Putere generata

## ▶ Putere generata

$$P = V \cdot I$$

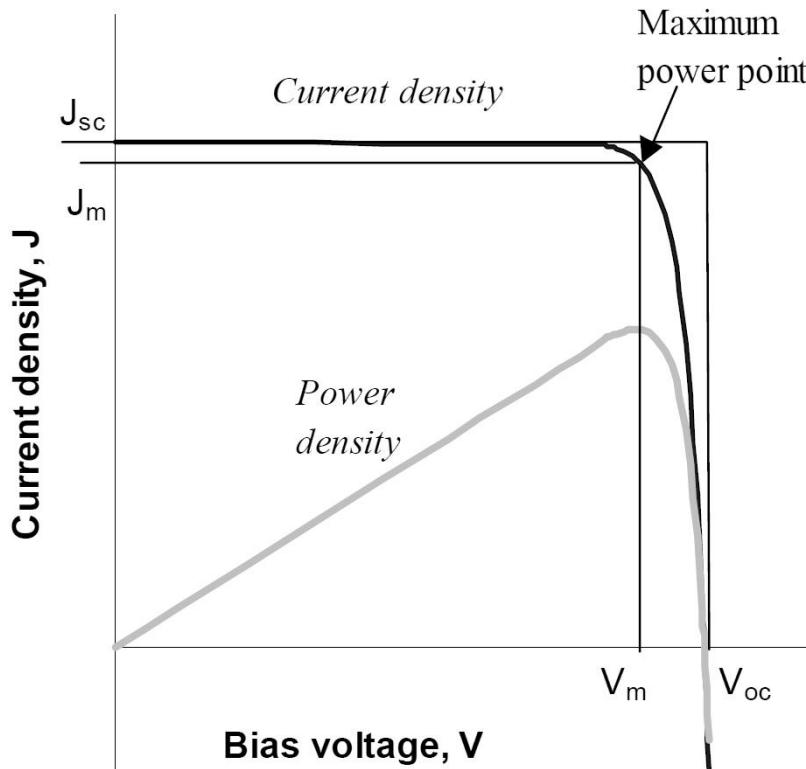


$$P_{oc} = V_{oc} \cdot 0 = 0$$



# Putere generata

## ▶ Putere generata

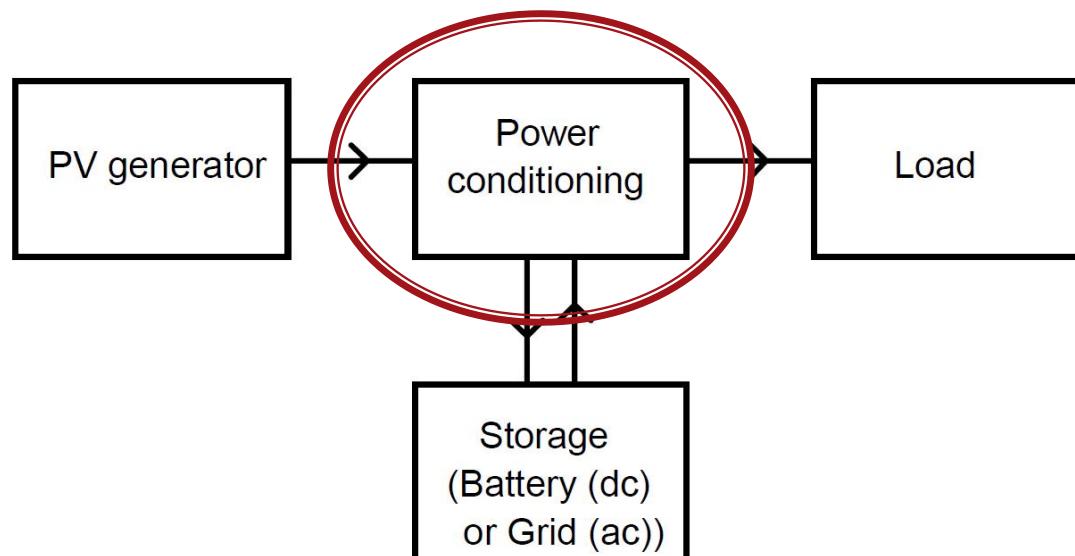


$$P_m = V_{pm} \cdot I_{pm}$$

▶ Valorile de curent si tensiune pentru putere maxima sunt date de catalog, circuitul de conditionare care urmeaza dupa celule poate fi **optimizat** sa functioneze la aceste valori

# Putere generata

- ▶ Controlerul de incarcare este responsabil pentru detectarea si urmarirea punctului de putere maxima
  - MPPT – Maximum power point tracking



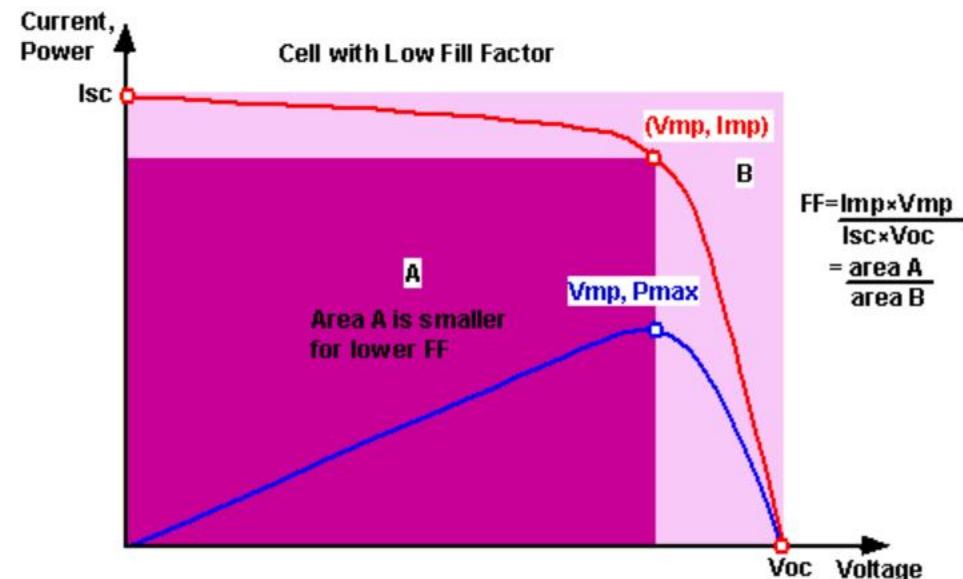
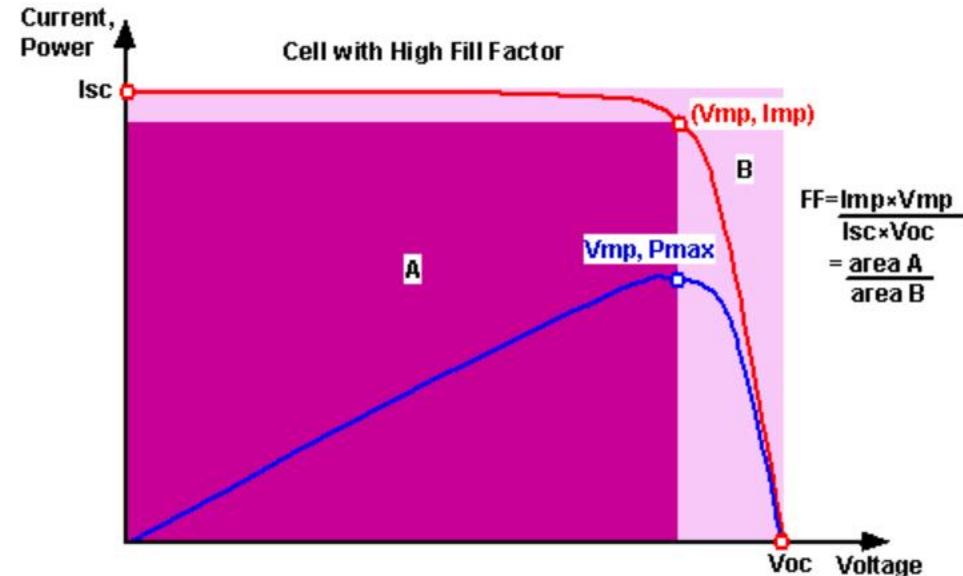
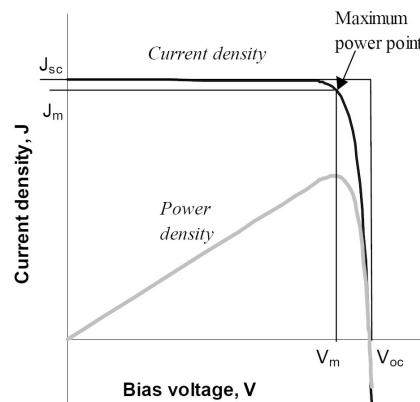
# Celula solara

- ▶ Factor de umplere

$$FF = \frac{V_{pm} \cdot I_{pm}}{V_{oc} \cdot I_{sc}}$$

- ▶ o masura a calitatii celulei
  - dependent de material

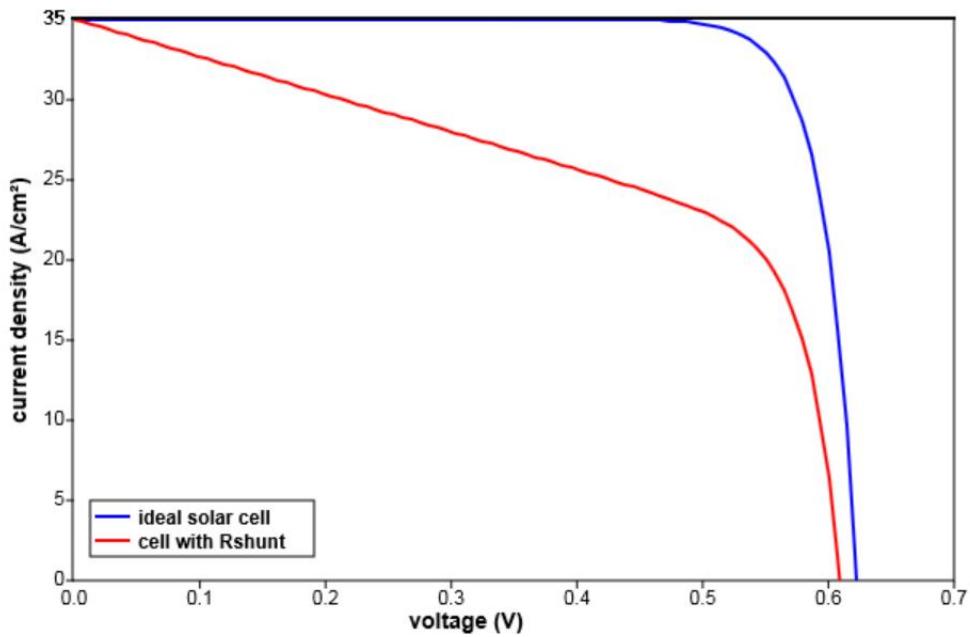
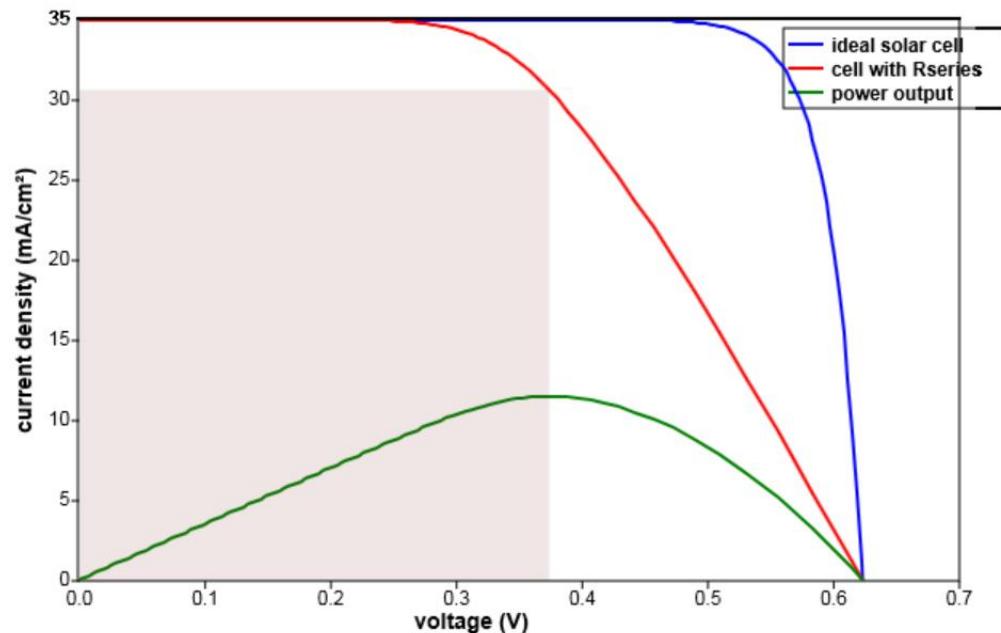
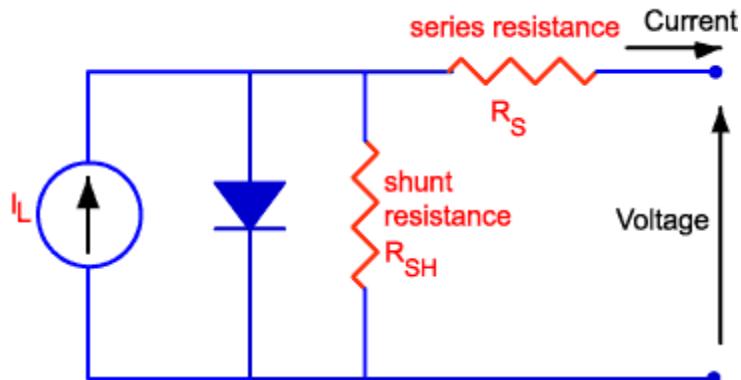
$$P_m = V_{pm} \cdot I_{pm}$$



# Efect pierderi

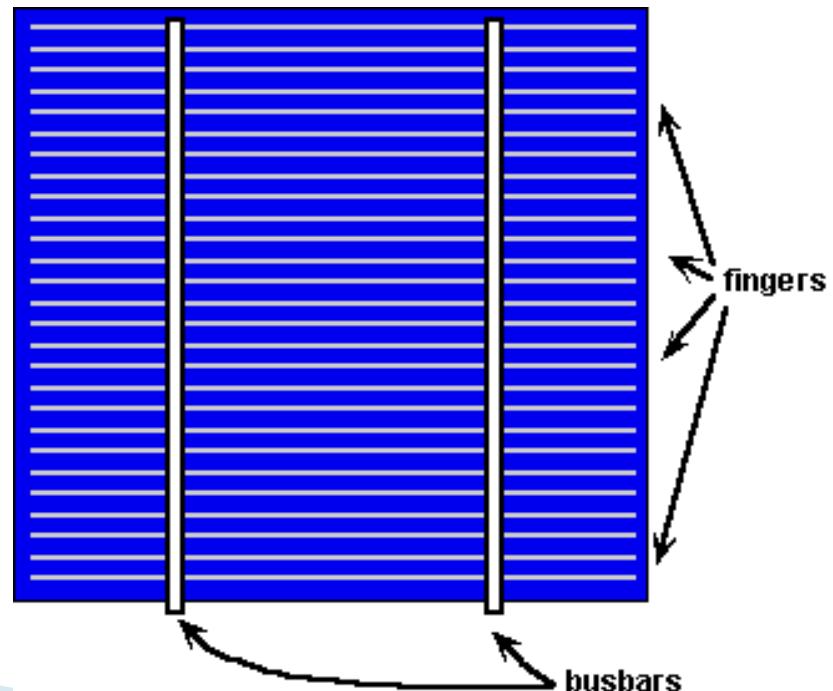
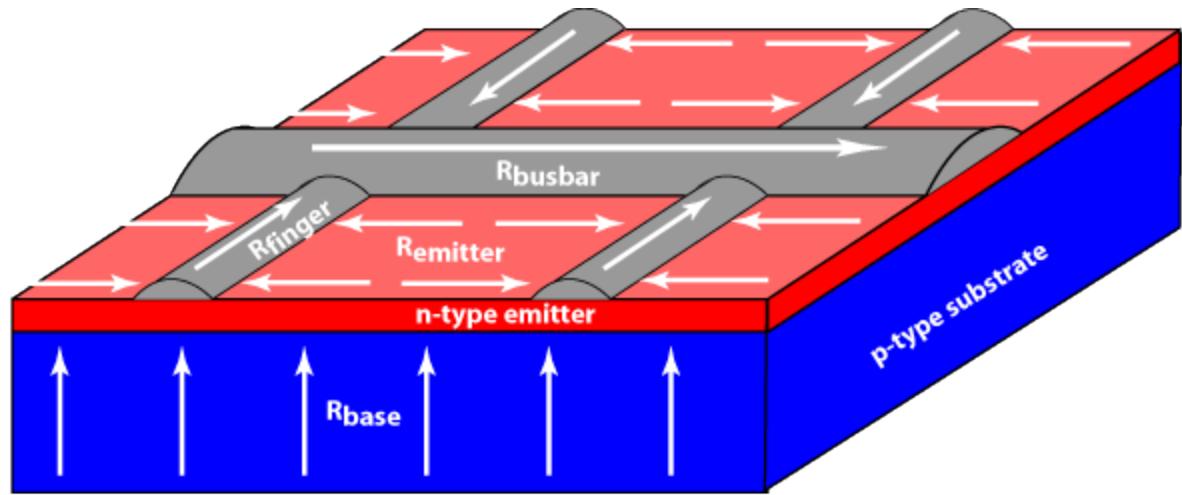
- ▶ Rezistenta serie
  - rezistenta echivalenta a semiconductorului utilizat
  - rezistenta jonctiunilor metal/semiconductor
  - rezistenta contactului metalic al anodului si colectorului
- ▶ Rezistenta paralel
  - generata de defecte de fabricatie

# Efect pierderi



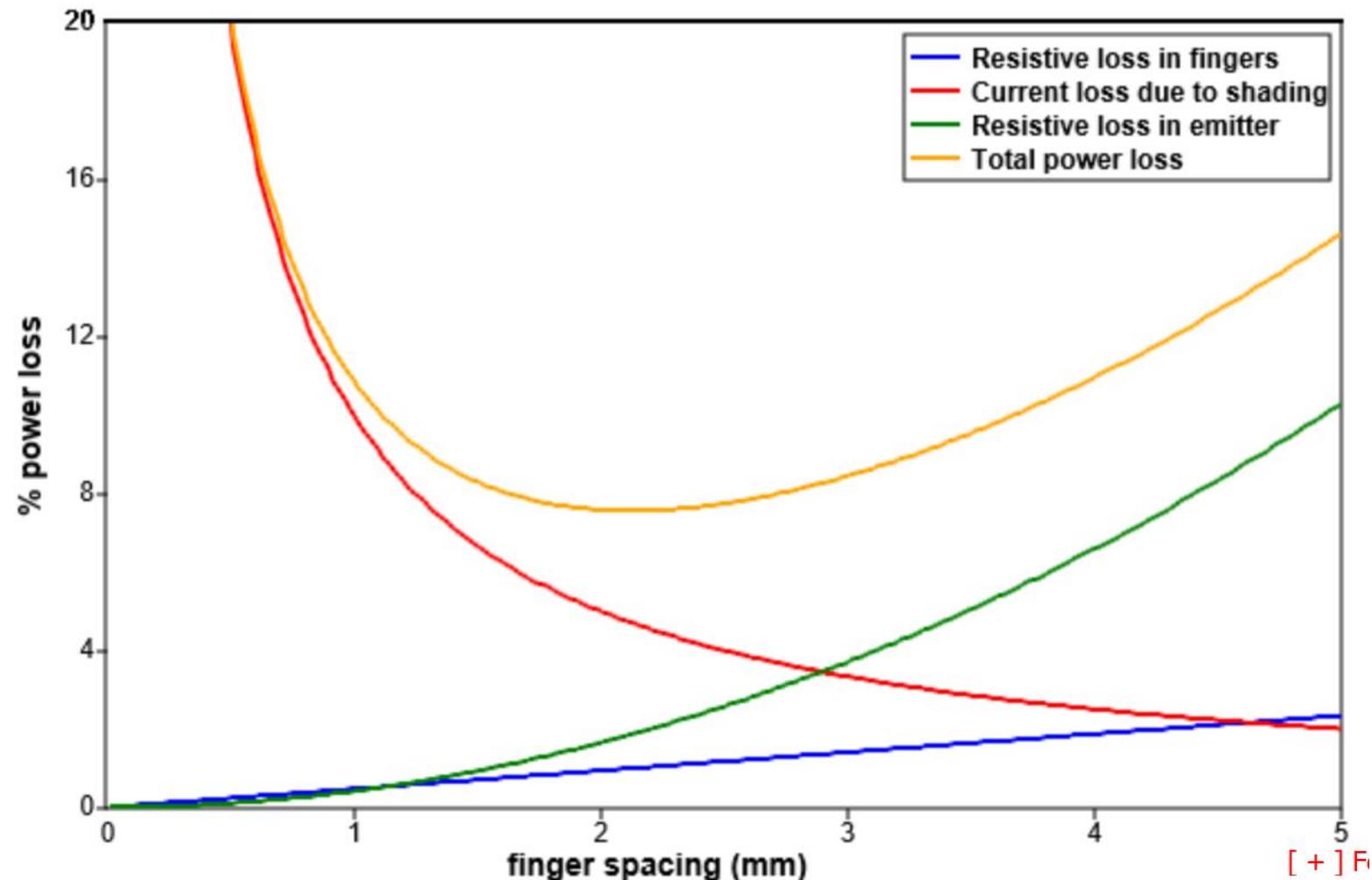
# Rezistenta serie

- ▶ Minimizare  $R_s$ 
  - bare colectoare
  - “degete”
- ▶ Compromis
  - rezistenta
  - suprafata metalica reflectorizanta



# Rezistenta serie

- ▶ Comprimis rezistenta/suprafata metalica



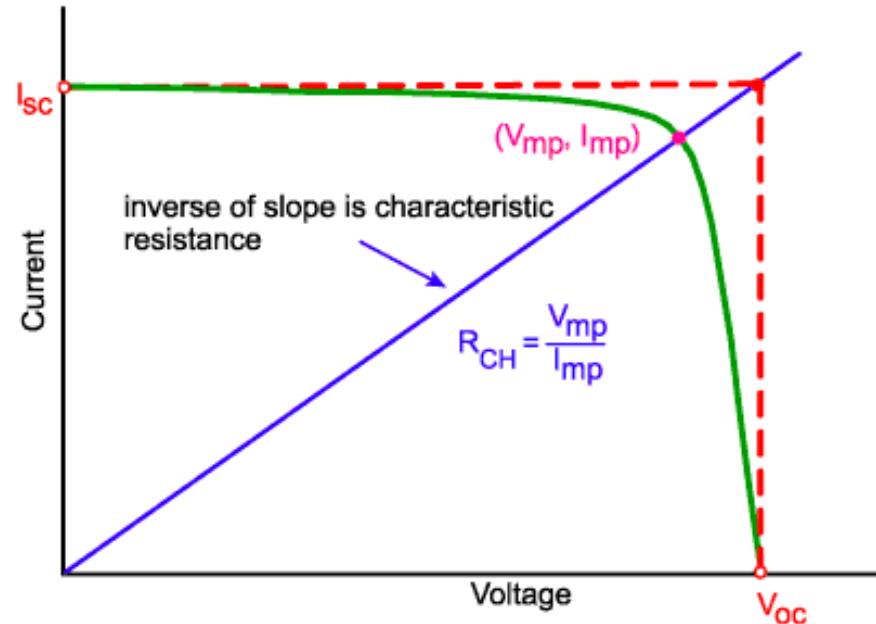
# Rezistenta caracteristica

- ▶ Raportul intre V si I cand celula lucreaza la eficienta maxima

$$R_C = \frac{V_{pm}}{I_{pm}} \approx \frac{V_{OC}}{I_{SC}}$$

- ▶ Daca sarcina este egala cu  $R_C$ , celula lucreaza la eficienta maxima

- ▶ Tipic, celulele comerciale opereaza la tensiune mica si curent mare
  - ▶ conexiunile la celule trebuie sa aiba rezistente de ordinul  $m\Omega$



$$R_C = \frac{0.6V}{9A} \approx 0.067\Omega$$

# Eficienta celulei solare

- ▶ raportul dintre puterea electrica generata si puterea optica incidenta

$$\eta = \frac{P_m}{P_o} = \frac{V_{pm} \cdot I_{pm}}{P_o}$$

$$\eta = \frac{P_m}{P_o} = \frac{V_{oc} \cdot I_{sc} \cdot FF}{P_o}$$

- ▶ Puterea optica depinde de fluxul energetic al luminii incidente si suprafata celulei

$$P_o = S \cdot \int_0^{\infty} \Phi_e(\lambda) d\lambda$$

# Eficiența celulei solare

- ▶ determină suprafața necesară pentru obținerea unei puteri dorite

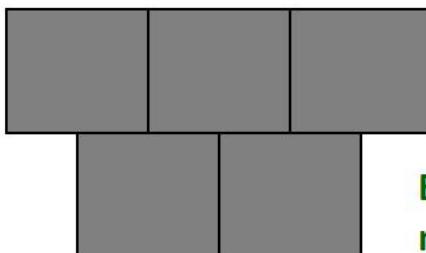
100% efficiency

(impossible to achieve)



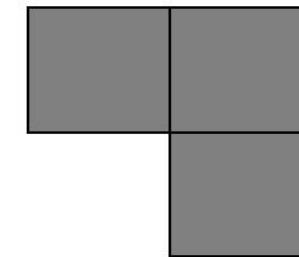
20% efficiency

(monocrystalline silicon solar cells)



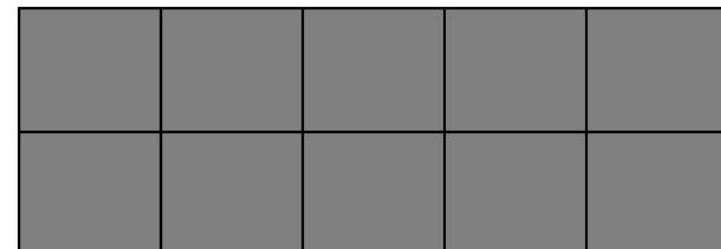
33% efficiency

(space-grade solar cells)



10% efficiency

(thin film material)



# Eficienta celulei solare

- ▶ Există o limită maximă teoretică pentru fiecare material semiconductor
  - fiecare material are o banda spectrală proprie, **mai mică** decât banda spectrală a soarelui
- ▶ valorile nu sunt foarte mari
  - din motive economice, recordurile nu sunt repetate în practică

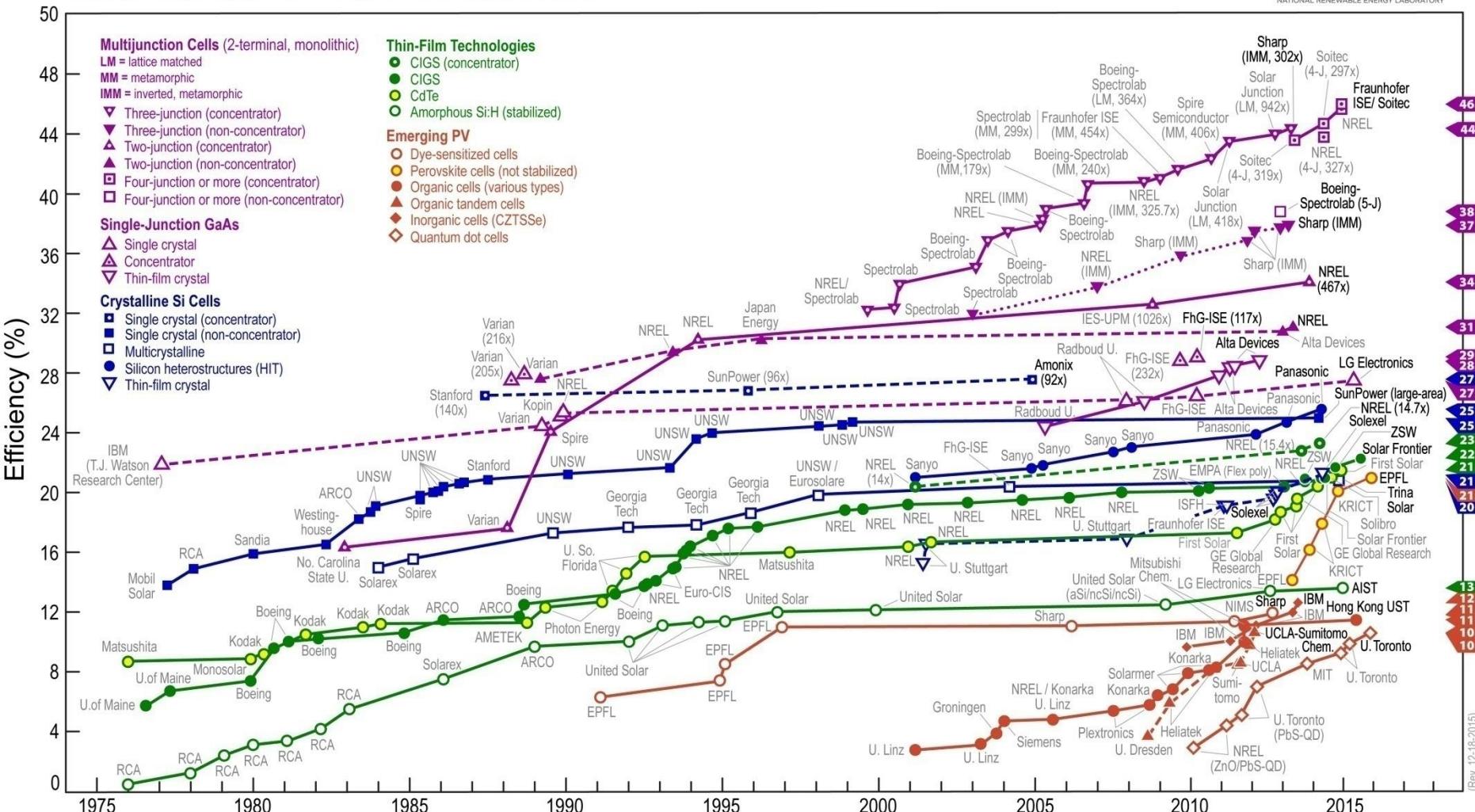
Table 1.1. Performance of some types of PV cell [Green *et al.*, 2001].

| Cell Type             | Area (cm <sup>2</sup> ) | V <sub>oc</sub> (V) | J <sub>sc</sub> (mA/cm <sup>2</sup> ) | FF   | Efficiency (%) |
|-----------------------|-------------------------|---------------------|---------------------------------------|------|----------------|
| crystalline Si        | 4.0                     | 0.706               | 42.2                                  | 82.8 | 24.7           |
| crystalline GaAs      | 3.9                     | 1.022               | 28.2                                  | 87.1 | 25.1           |
| poly-Si               | 1.1                     | 0.654               | 38.1                                  | 79.5 | 19.8           |
| a-Si                  | 1.0                     | 0.887               | 19.4                                  | 74.1 | 12.7           |
| CuInGaSe <sub>2</sub> | 1.0                     | 0.669               | 35.7                                  | 77.0 | 18.4           |
| CdTe                  | 1.1                     | 0.848               | 25.9                                  | 74.5 | 16.4           |

# Eficienta maxima a celulei solare

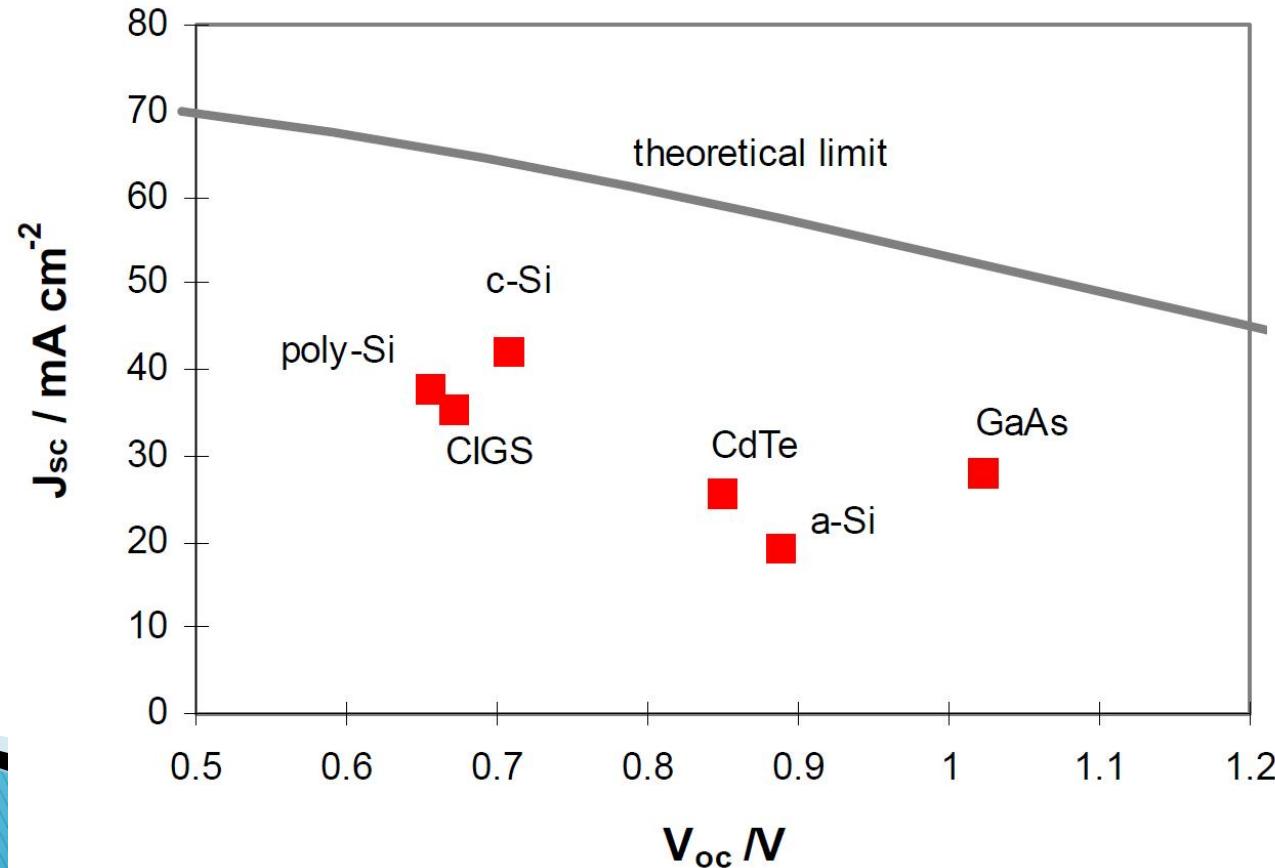
## Best Research-Cell Efficiencies

**NREL**  
NATIONAL RENEWABLE ENERGY LABORATORY



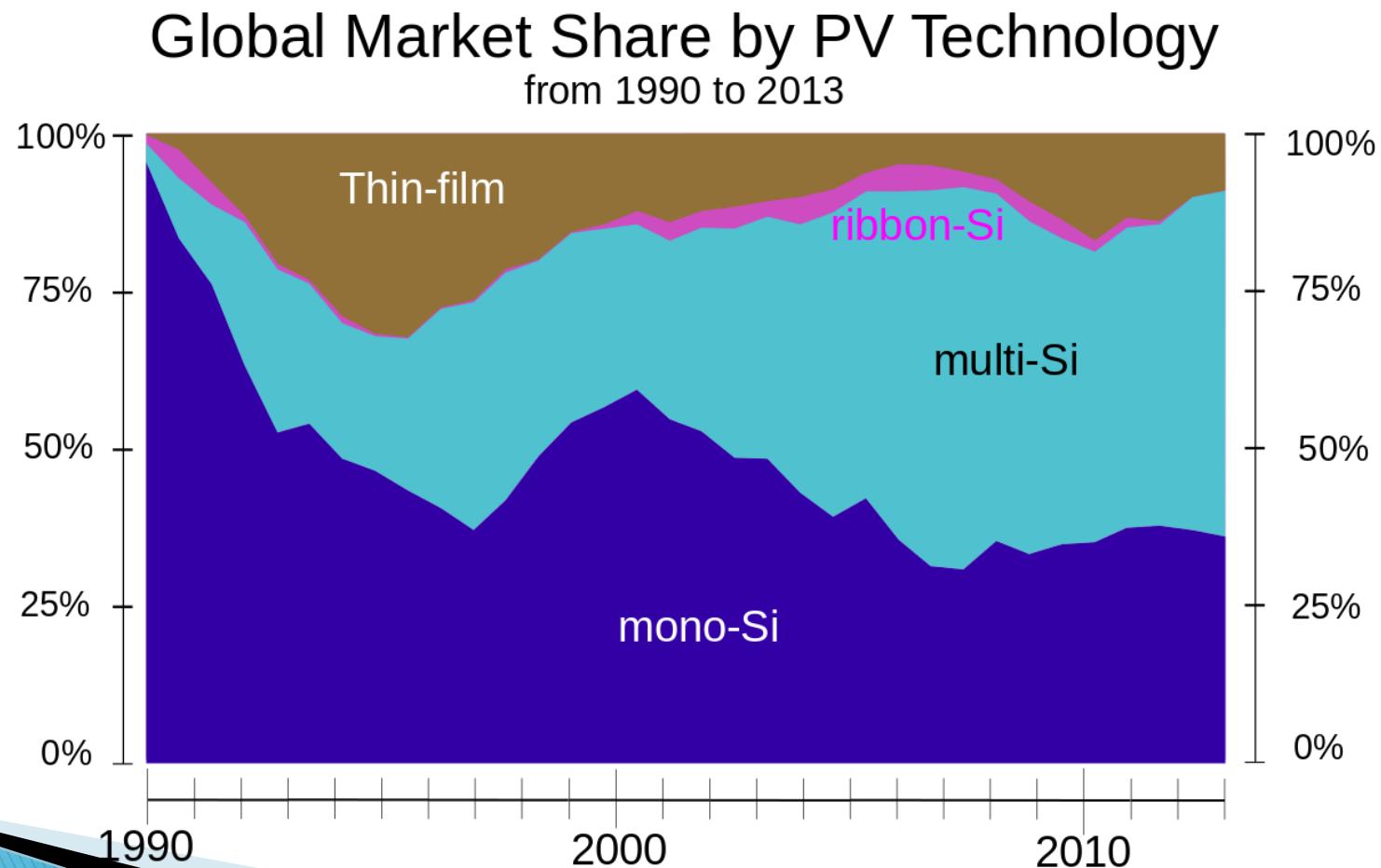
# Dependenta de material

- ▶ materialele care ofera tensiuni mari au de obicei curenti mai mici
  - dependent de latimea benzii interzise



# Realizari practice

- ▶ materialul preferat este Si



# Tipic

# 80 WATT

POWERFUL PERFORMANCE. SHARP RELIABILITY.

## **POLY-CRYSTALLINE SILICON PHOTOVOLTAIC MODULE WITH 80W MAXIMUM POWER**

Sharp's NE-80EJA photovoltaic modules offer industry-leading performance, durability, and reliability for a variety of electrical power requirements. Using breakthrough technology perfected by Sharp's 45 years of research and development, these modules incorporate an advanced surface texturing process to increase light absorption and improve efficiency. Common applications include cabins, solar power stations, pumps, beacons,



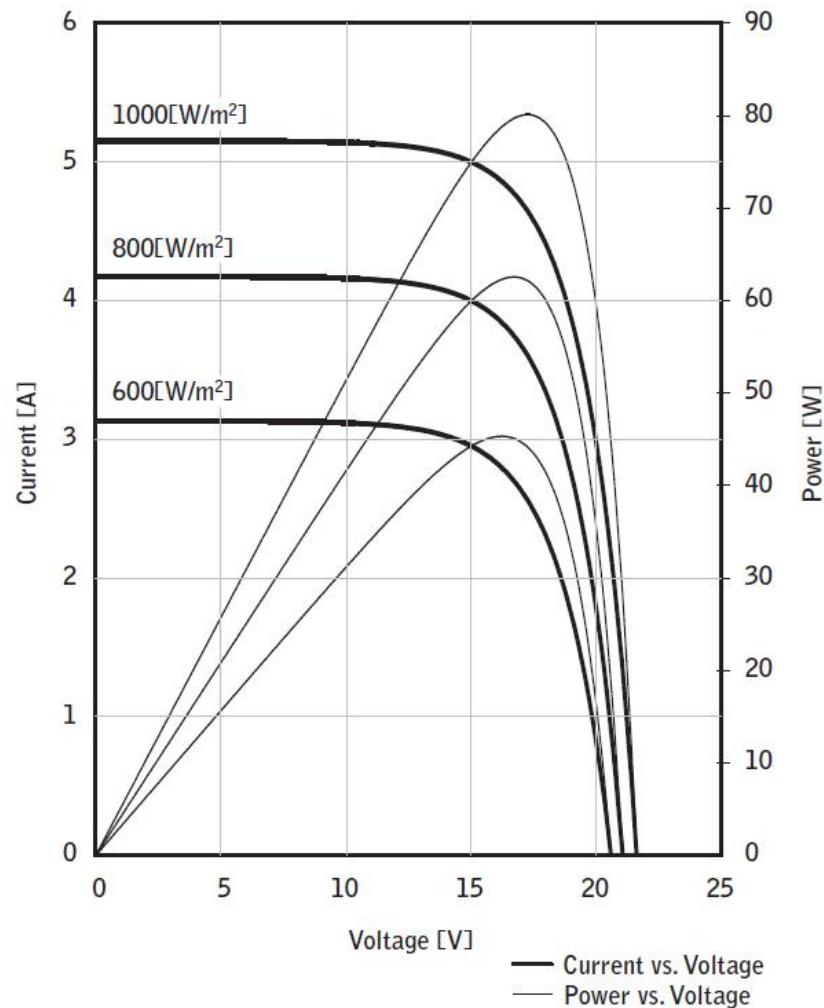
# Tipic

## ELECTRICAL CHARACTERISTICS

|                                |                          |
|--------------------------------|--------------------------|
| Cell                           | Poly-crystalline silicon |
| No. of Cells and Connections   | 36 in series             |
| Open Circuit Voltage (Voc)     | 21.6V                    |
| Maximum Power Voltage (Vpm)    | 17.3V                    |
| Short Circuit Current (Isc)    | 5.16A                    |
| Maximum Power Current (Ipm)    | 4.63A                    |
| Maximum Power (Pmax)*          | 80W (+10% / -5%)         |
| Module Efficiency ( $\eta_m$ ) | 12.40%                   |
| Maximum System Voltage         | 600VDC                   |
| Series Fuse Rating             | 10A                      |
| Type of Output Terminal        | Junction Box             |

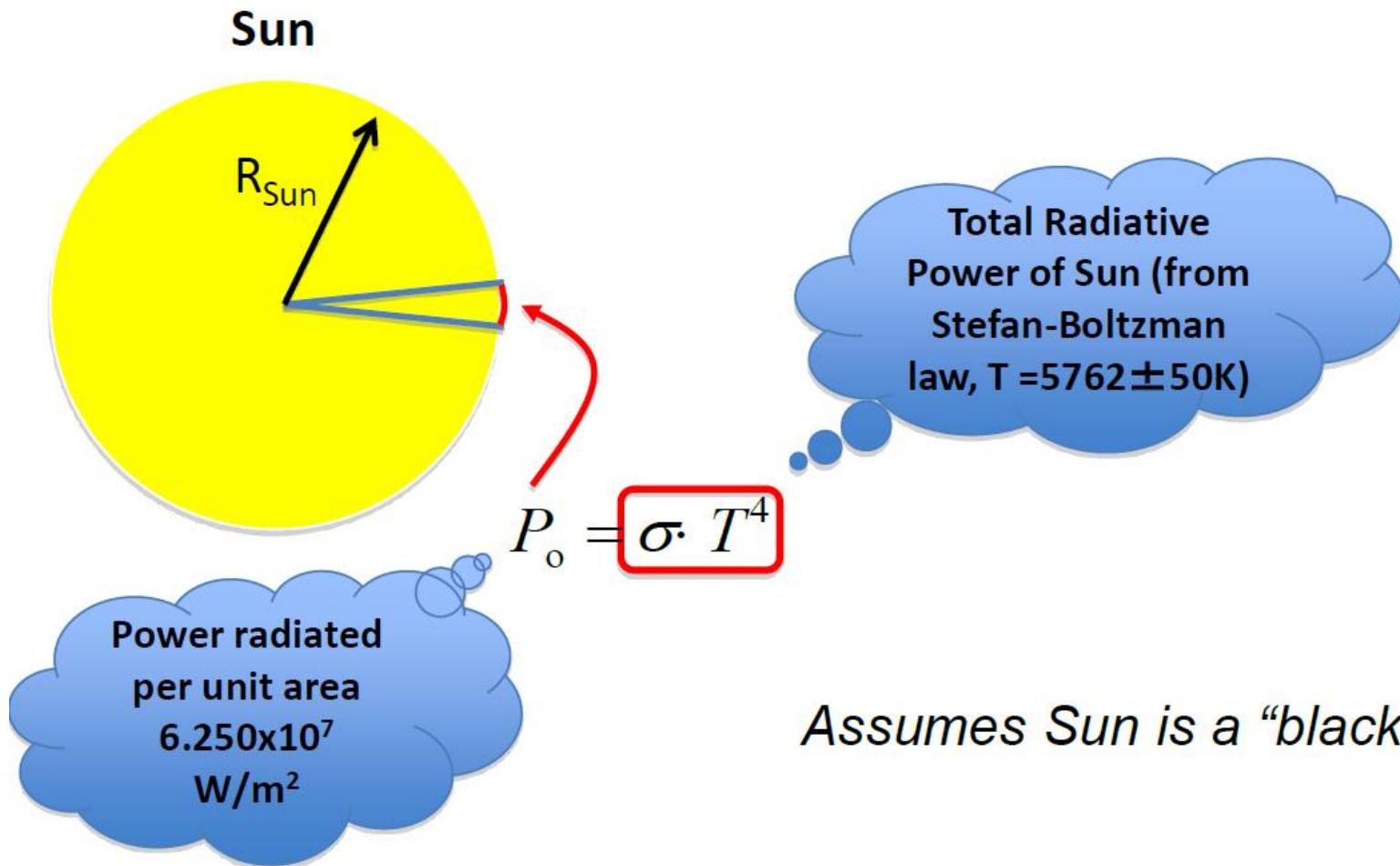
## IV CURVES

Cell Temperature: 25°C



Current, Power vs. Voltage Characteristics

# Energia solară disponibilă



# Energia solara disponibila

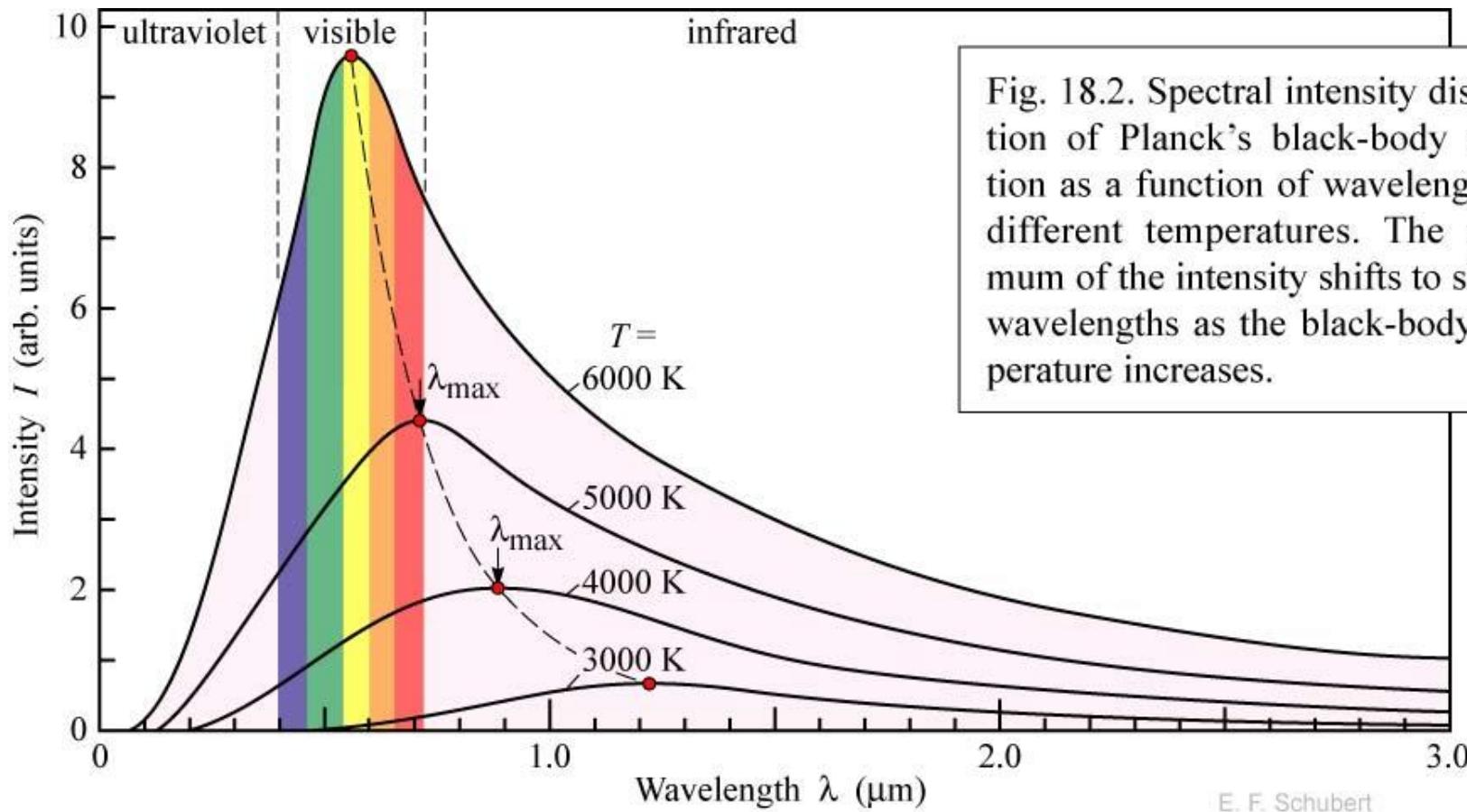
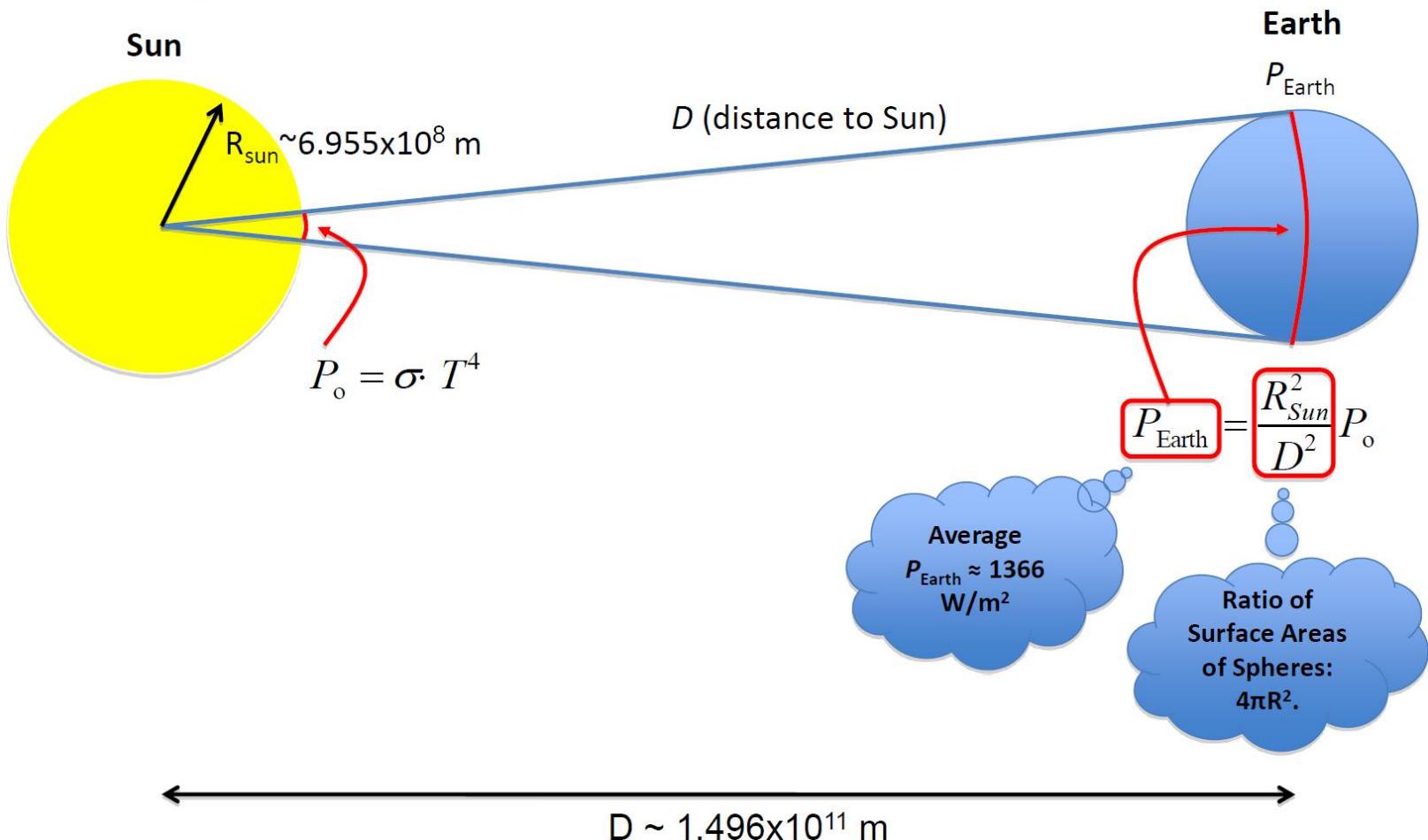


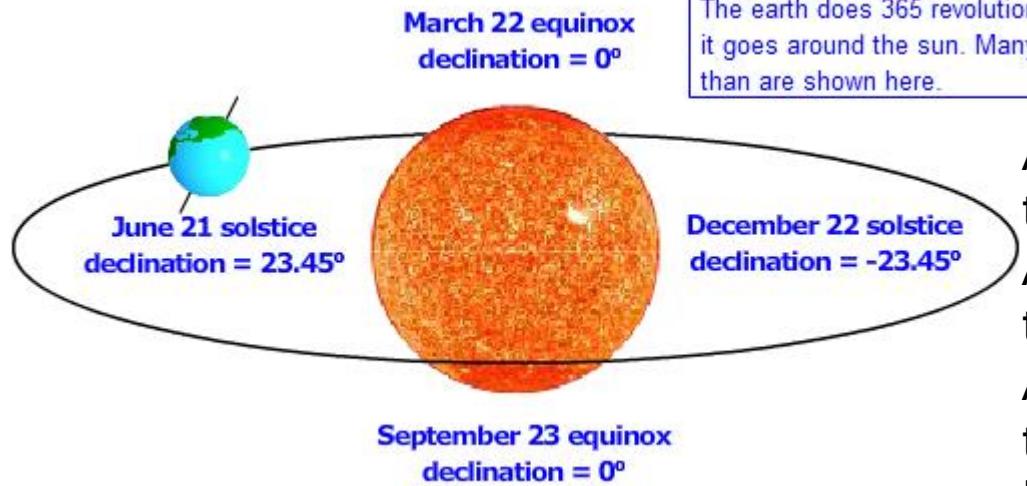
Fig. 18.2. Spectral intensity distribution of Planck's black-body radiation as a function of wavelength for different temperatures. The maximum of the intensity shifts to shorter wavelengths as the black-body temperature increases.

# Energia solară disponibilă



Energia receptionată pe toata suprafața Pamantului  
intr-**o ora** mai mare decat toata energia consumata  
de intreaga populatie intr-**un an**

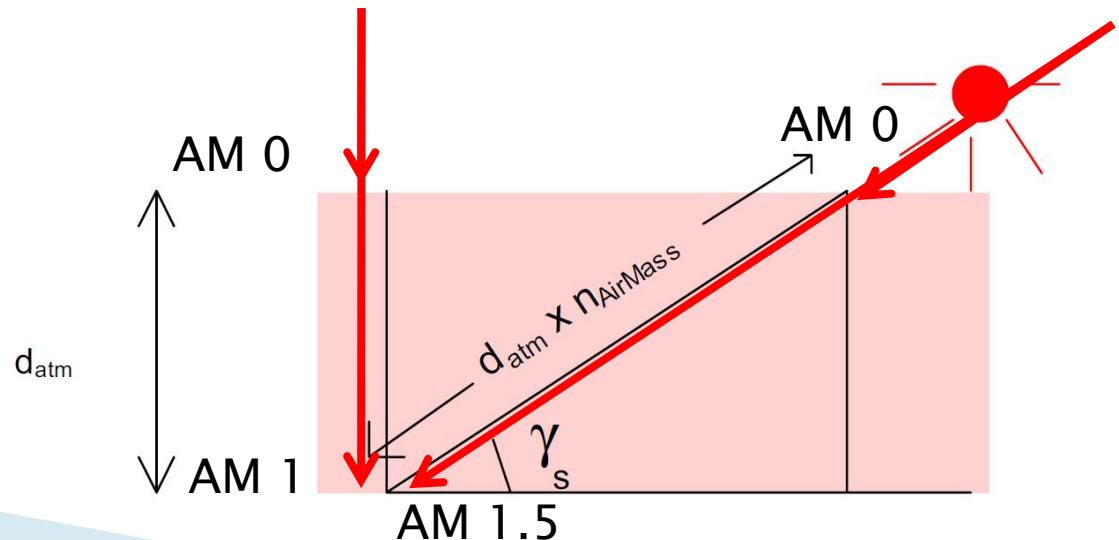
# Energia solară disponibilă



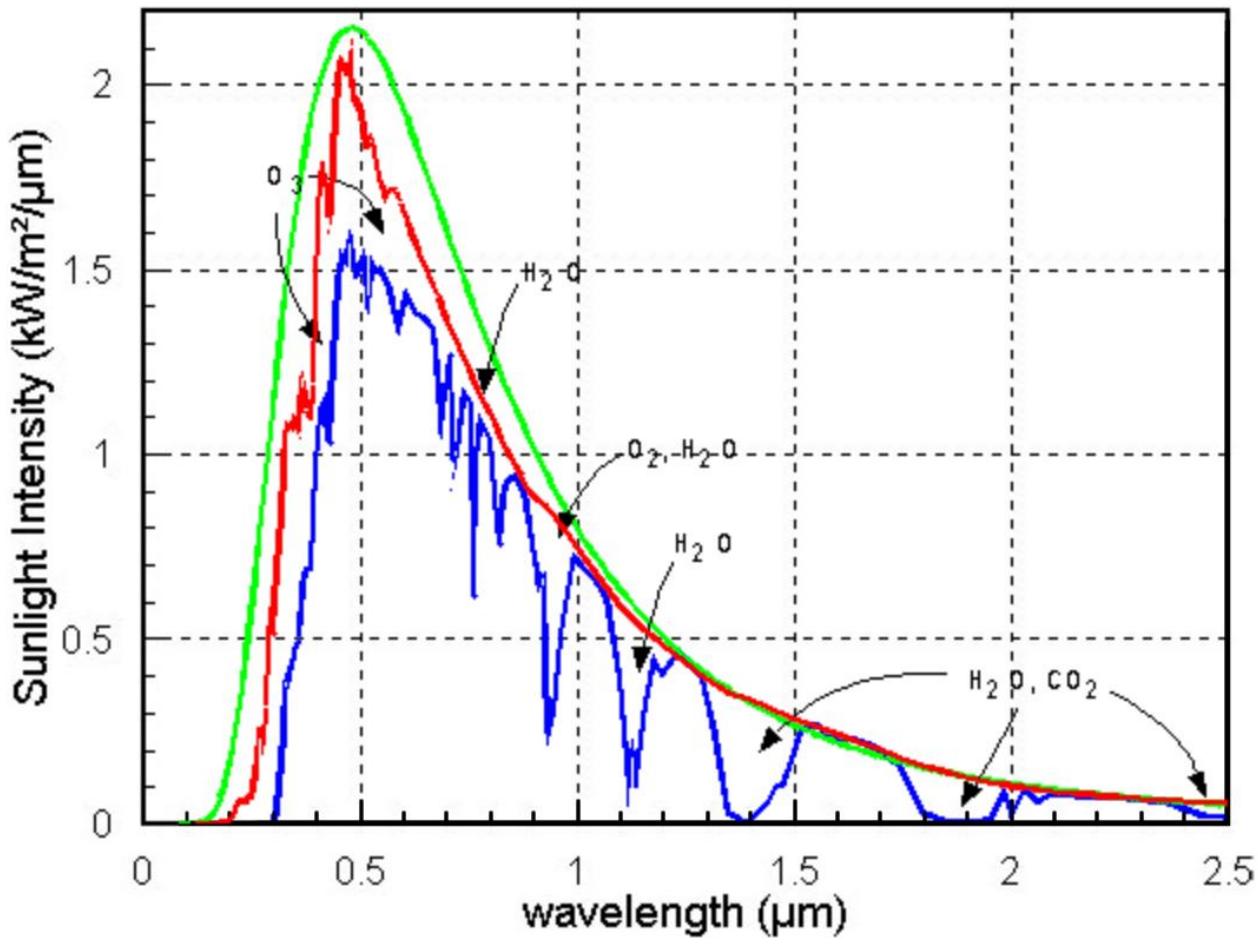
AM 0 = radiatia în afara atmosferei terestre

AM 1 = radiatia la suprafața terestră, incidentă normală

AM 1.5 = radiatia la suprafața terestră, incidentă corespunzătoare latitudinii de  $48^\circ$  (**standard**)

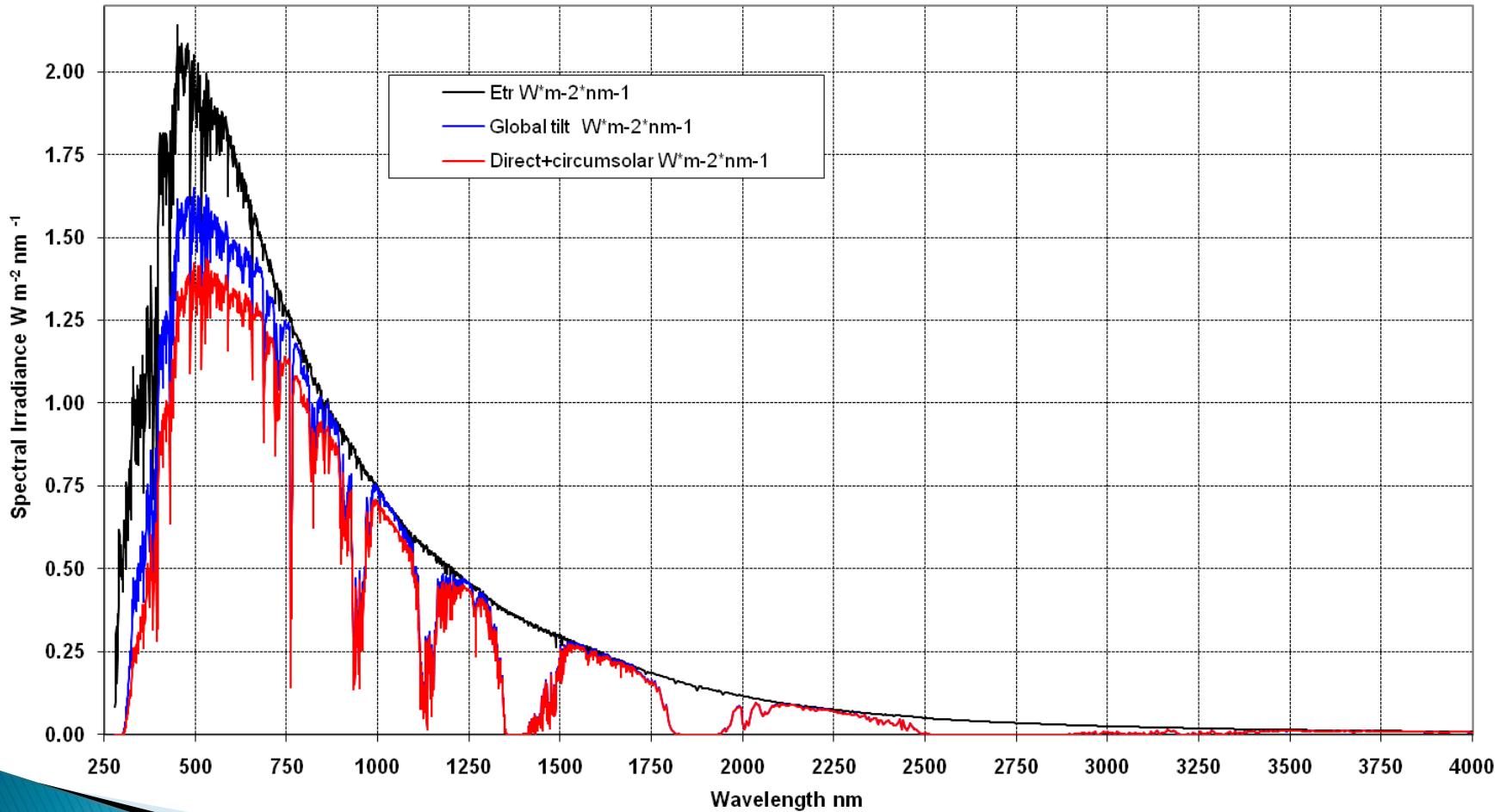


# Energia solara disponibila

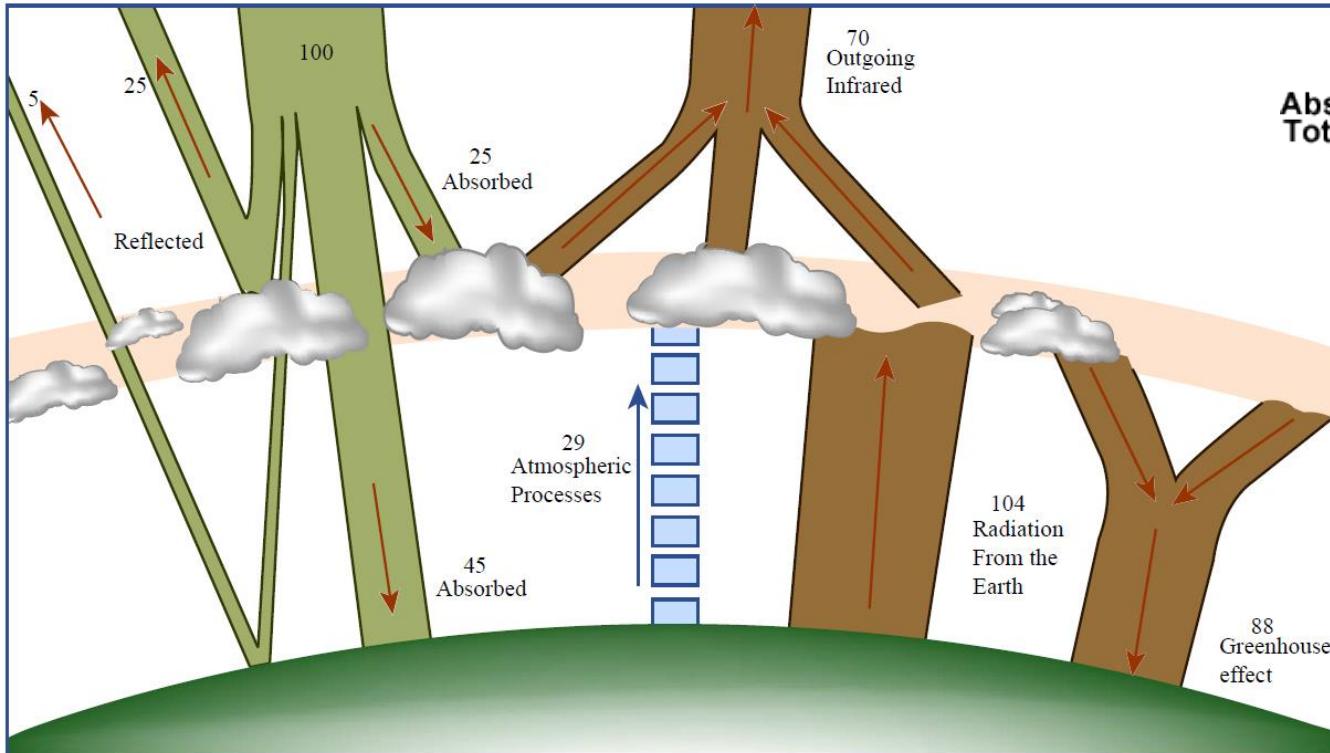


# Energia solar disponibila

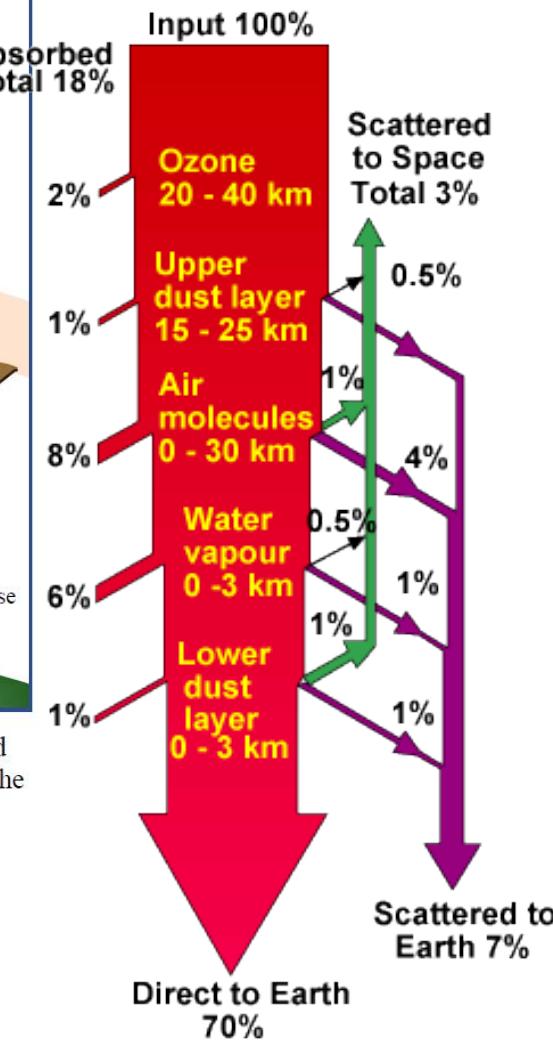
ASTM G173-03 Reference Spectra



# Energia solara disponibila



Heat trapping in the atmosphere dominates the earth's energy balance. Some 30% of incoming solar energy is reflected (left), either from clouds and particles in the atmosphere or from the earth's surface; the remaining 70% is absorbed. The absorbed energy is reemitted at infrared wavelengths by the atmosphere (which is also heated by updrafts and cloud formation) and by the surface. Because most of the surface radiation is trapped by clouds and greenhouse gases and returned to the earth, the surface is currently about 33 degrees Celsius warmer than it would be without the trapping.



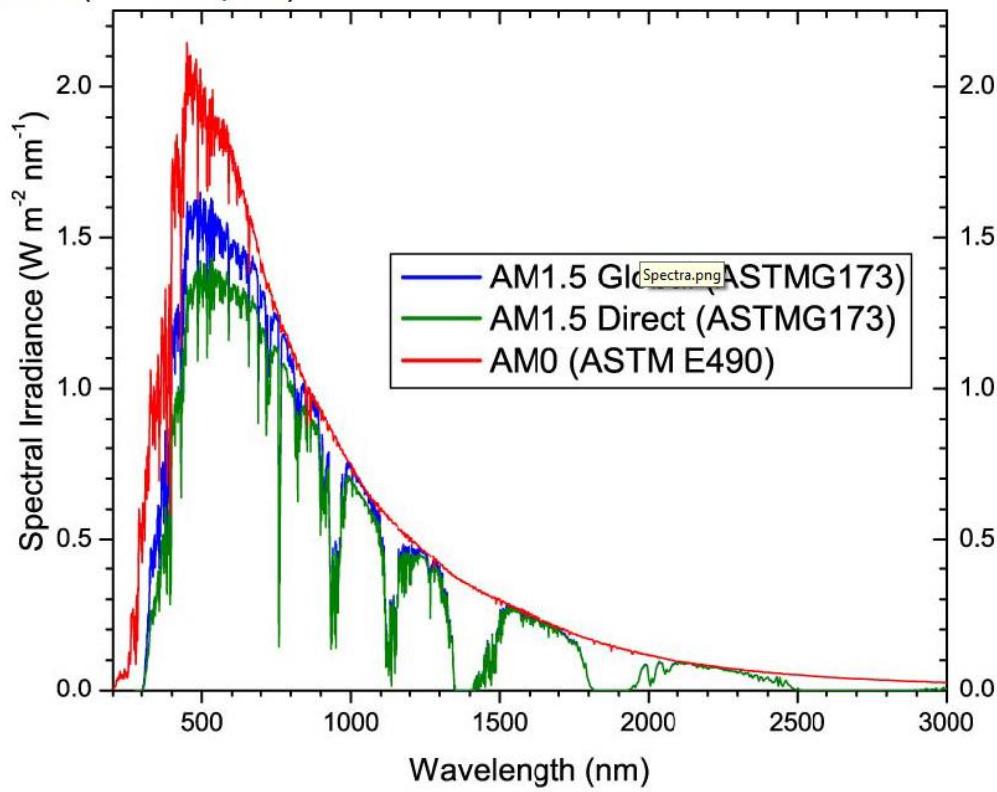
# Energia solara disponibila

## SOLAR SPECTRUM

AM1.5 Global: Used for testing of Flat Panels (Integrated power intensity: 1000 W/m<sup>2</sup>)

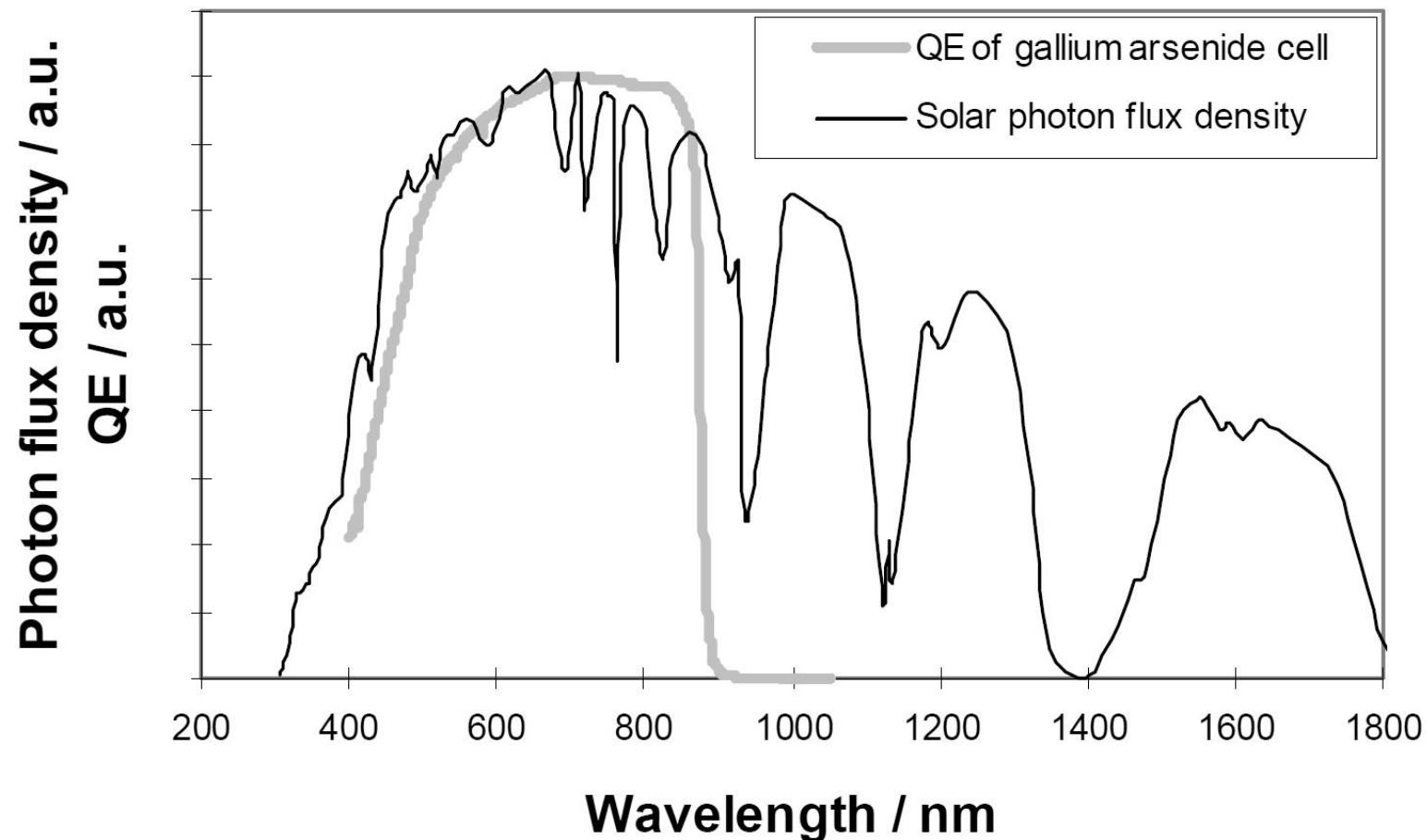
AM1.5 Direct: Used for testing of concentrators (900 W/m<sup>2</sup>)

AM0: Outer space (1366 W/m<sup>2</sup>)



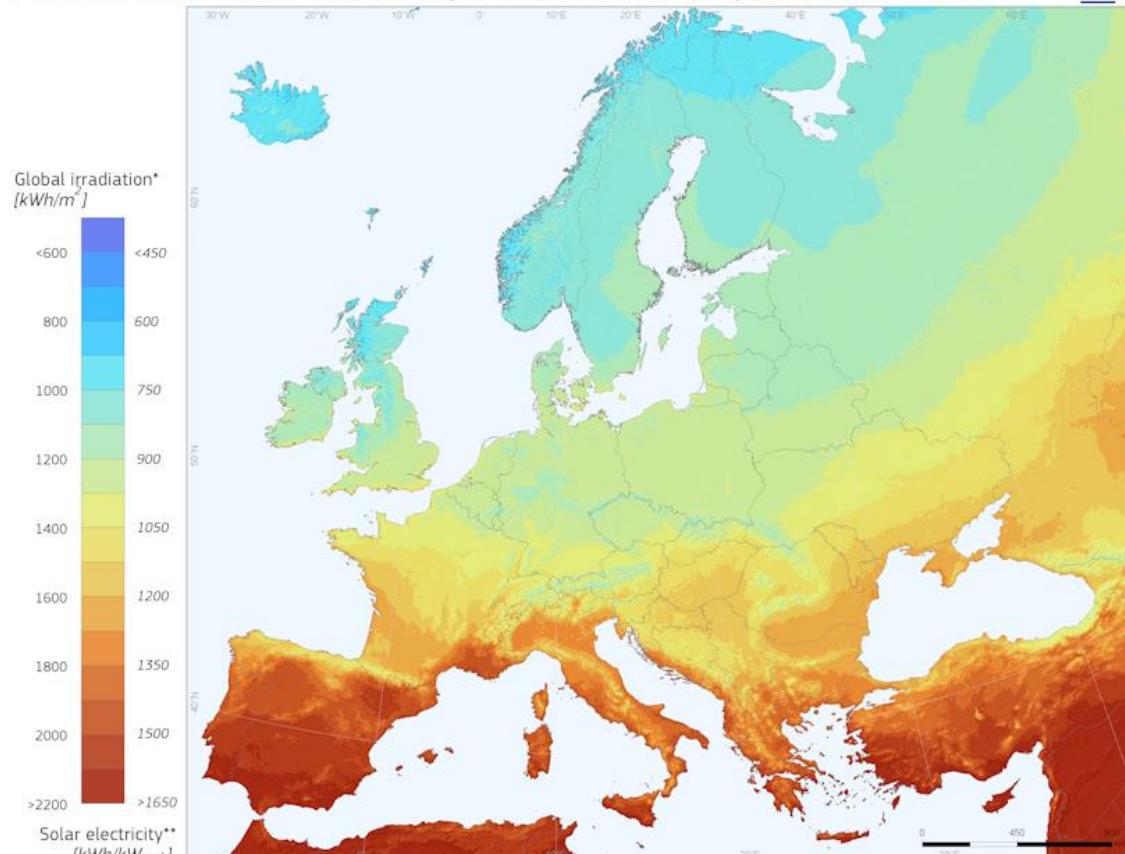
# Motivatie eficienta limitata

- ▶ Toate materialele utilizeaza o banda care acopera **doar** partial spectrul solar (ex. GaAs)



# Energia solara disponibila

Photovoltaic Solar Electricity Potential in European Countries



\* Yearly sum of global irradiation incident on optimally-inclined south-oriented photovoltaic modules

\*\* Yearly sum of solar electricity generated by optimally-inclined 1kW<sub>dc</sub> system with a performance ratio of 0.75

© European Union, 2012  
PVGIS <http://re.jrc.ec.europa.eu/pvgis/>

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<http://re.jrc.ec.europa.eu/pvgis/>

# Energia solară disponibilă



Global irradiation and solar electricity potential

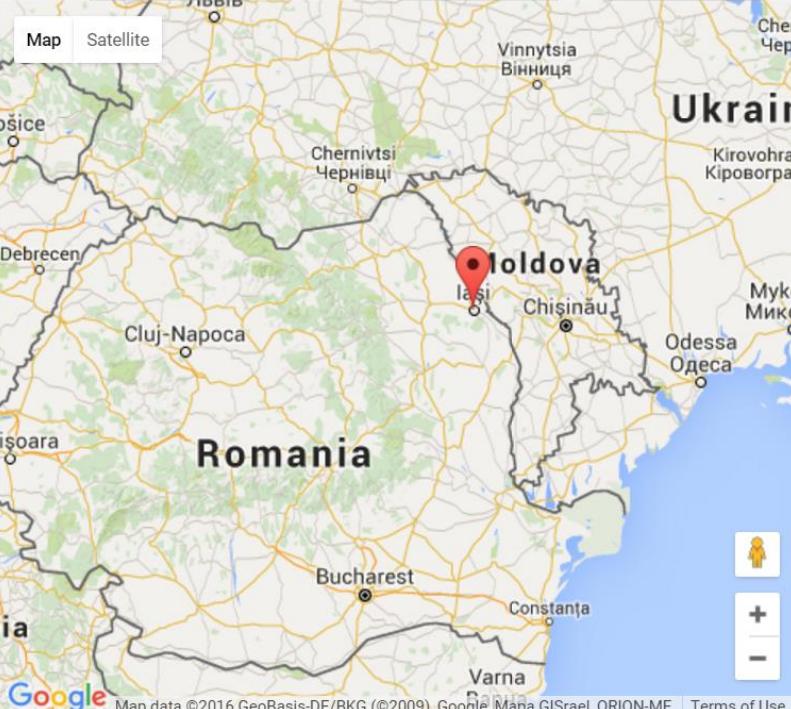
Optimally-inclined photovoltaic modules

ROMANIA / ROMÂNIA



# Energia solară disponibilă

JRC  
EUROPEAN COMMISSION  
CM SAF  
Photovoltaic Geographical Information System - Interactive Maps  
EUROPA > EC > JRC > IE > RE > SOLAREC > PVGIS > Interactive maps > europe  
cursor position:  
46.725, 31.882  
selected position:  
47.158, 27.601

lasi  
e.g., "Ispra, Italy" or "45.256N, 16.9589E"  
Search  
Latitude: \_\_\_\_\_ Longitude: \_\_\_\_\_ Go to lat/lon  
Map Satellite  
  
Google Map data ©2016 GeoBasis-DE/BKG (©2009), Google, Mapa GISrael, ORION-ME Terms of Use  
Solar radiation Temperature Other maps

Contact Important legal notice  
PV Estimation Monthly radiation Daily radiation Stand-alone PV

### Monthly global irradiation data

Radiation database: Climate-SAF PVGIS ▾

- Horizontal irradiation
- Irradiation at opt. angle
- Direct normal irradiation
- Irradiation at chosen angle: 90 deg.
- Linke turbidity
- Dif. / global radiation
- Optimal inclination angle

### Monthly ambient temperature data

- Average daytime temperature
- Daily average of temperature
- Number of heating degree days

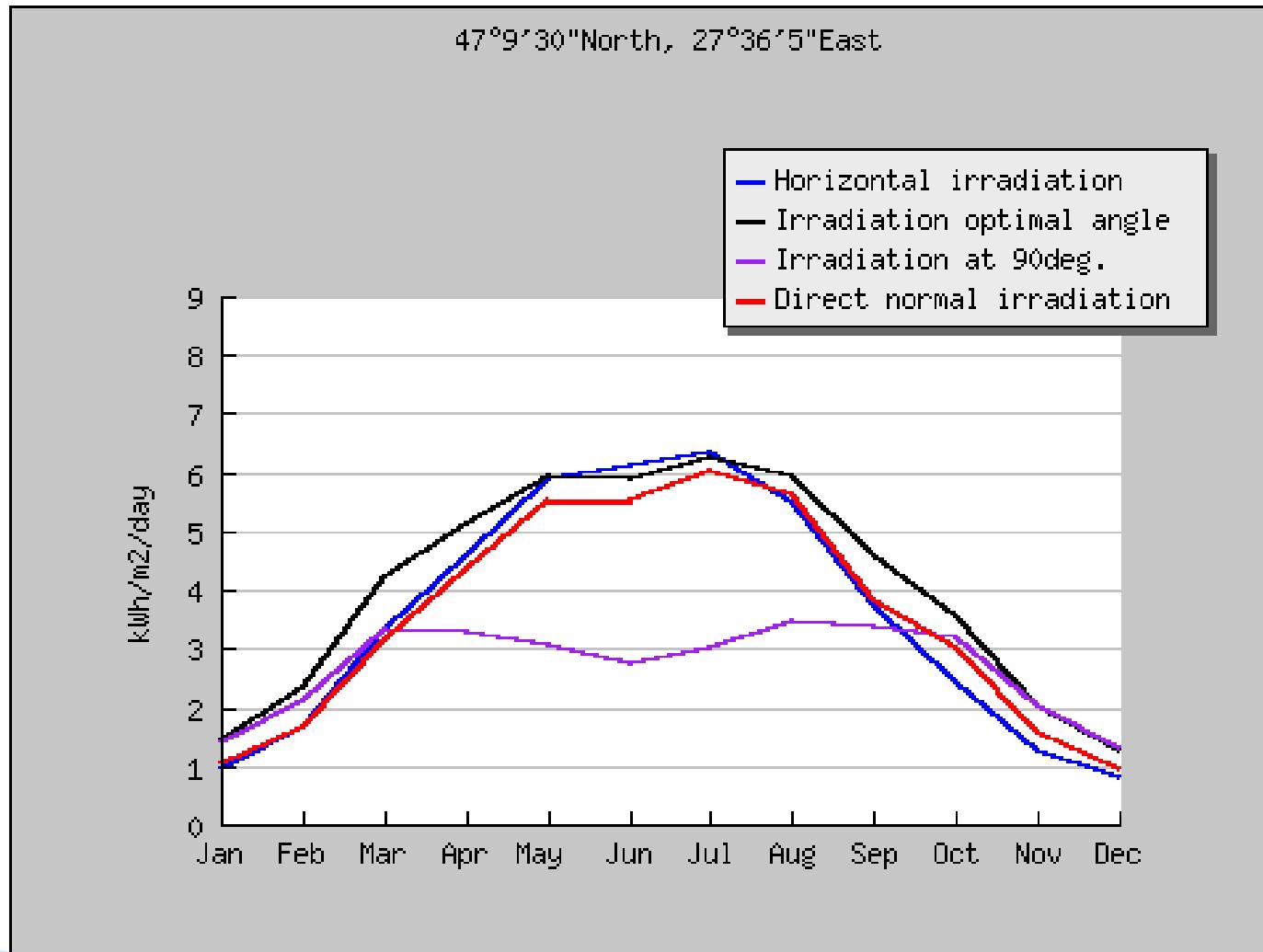
### Output options

Show graphs       Show horizon  
 Web page       Text file       PDF

**Calculate** [help]

Photovoltaic Geographical Information System (PVGIS)  
<http://re.jrc.ec.europa.eu/pvgis/>

# Energia solara disponibila – Iasi



# Unghi optim de inclinare

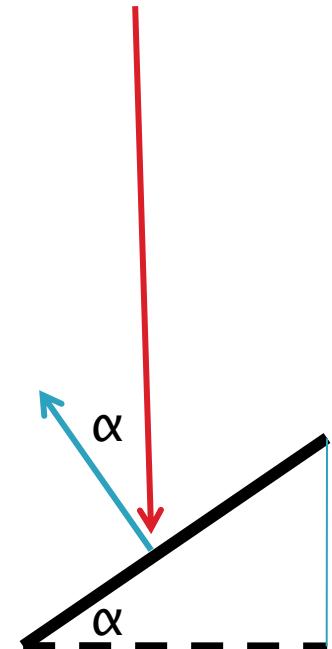
- ▶ Puterea optica depinde de fluxul energetic al luminii incidente si suprafata celulei
  - la **incidenta normală**
  - la **incidenta oarecare**

$$P_o = S \cdot \int_0^{\infty} \Phi_e(\lambda) d\lambda$$

- la **incidenta oarecare**

$$\Phi_e(\lambda) = \int_{\Sigma} \vec{S} \cdot \vec{n} dA = |S| \cdot A \cdot \cos \alpha$$

$$\vec{S} = \vec{E} \times \vec{H}$$



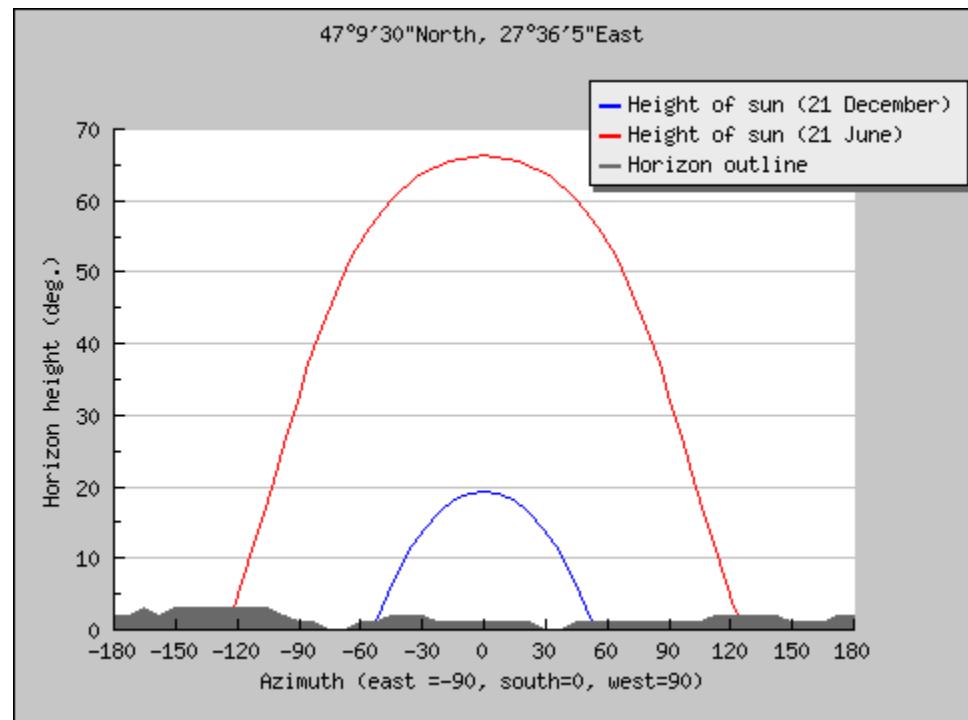
# Unghi optim de inclinare

- ▶ Pozitia soarelui este diferita
  - in functie de ora
  - in functie de anotimp

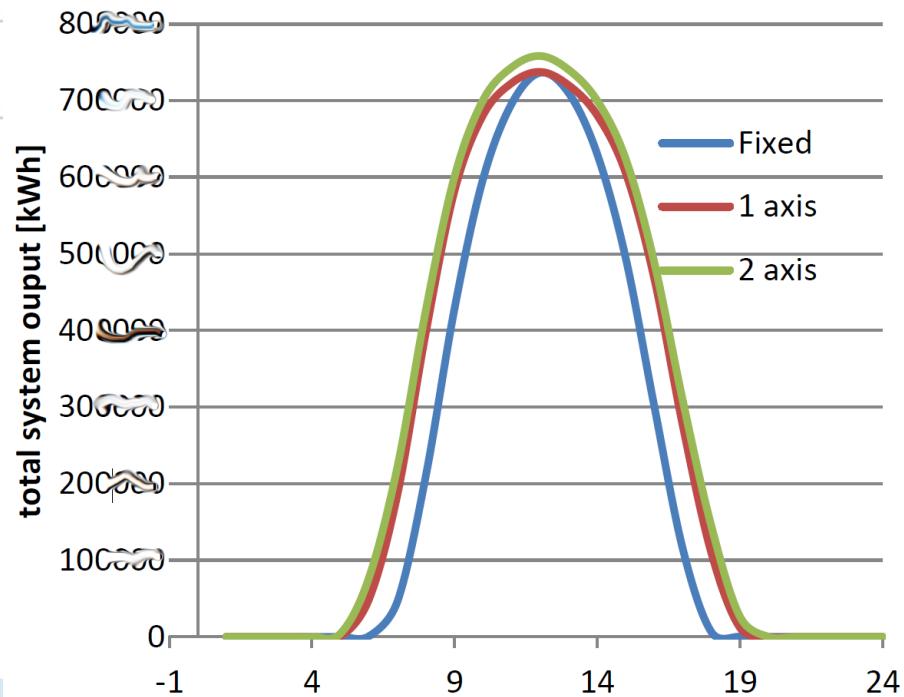
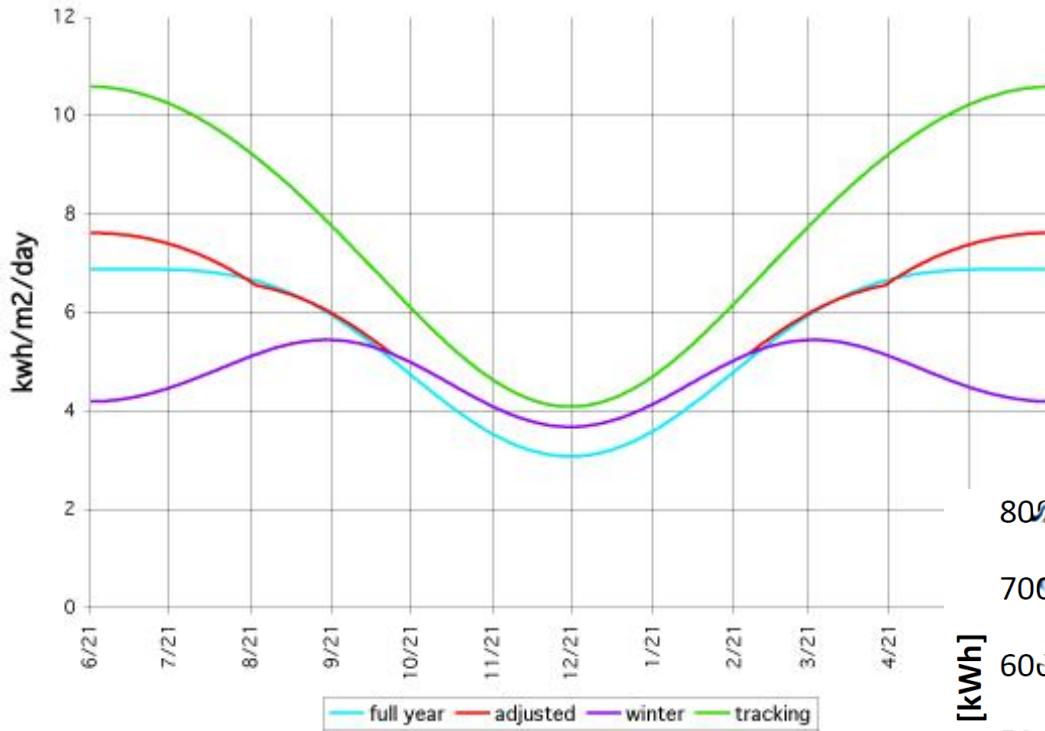


# Sisteme de urmarire

- ▶ Sisteme motorizate de urmarire a soarelui
  - o axă
  - două axe
- ▶ Reglaj
  - fix (optim an)
  - două pozitii (anotimp)

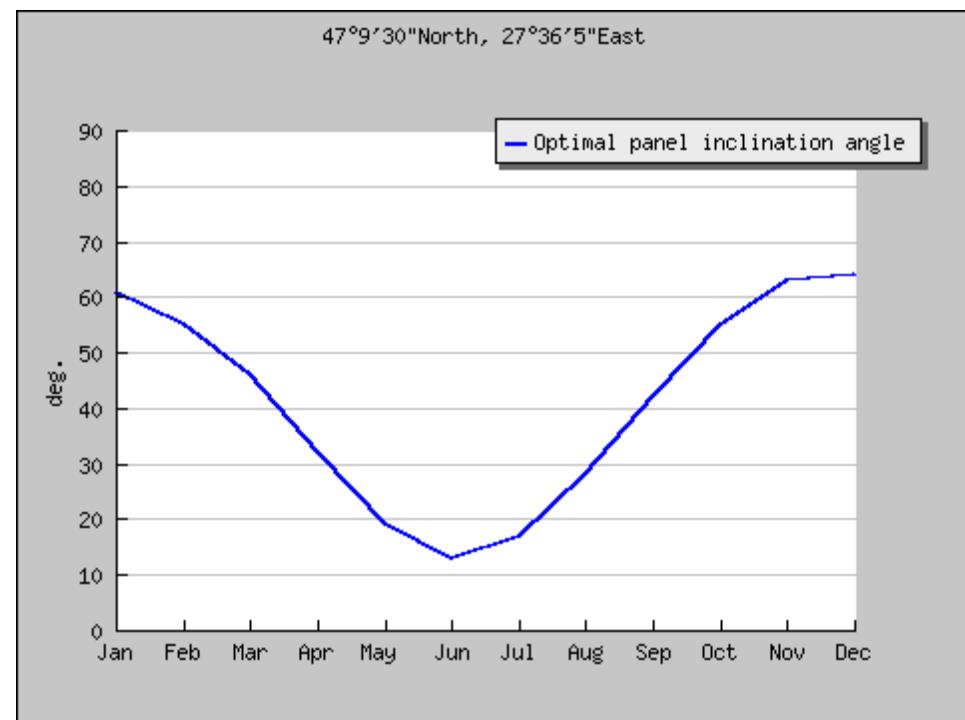


# Sisteme de urmarire

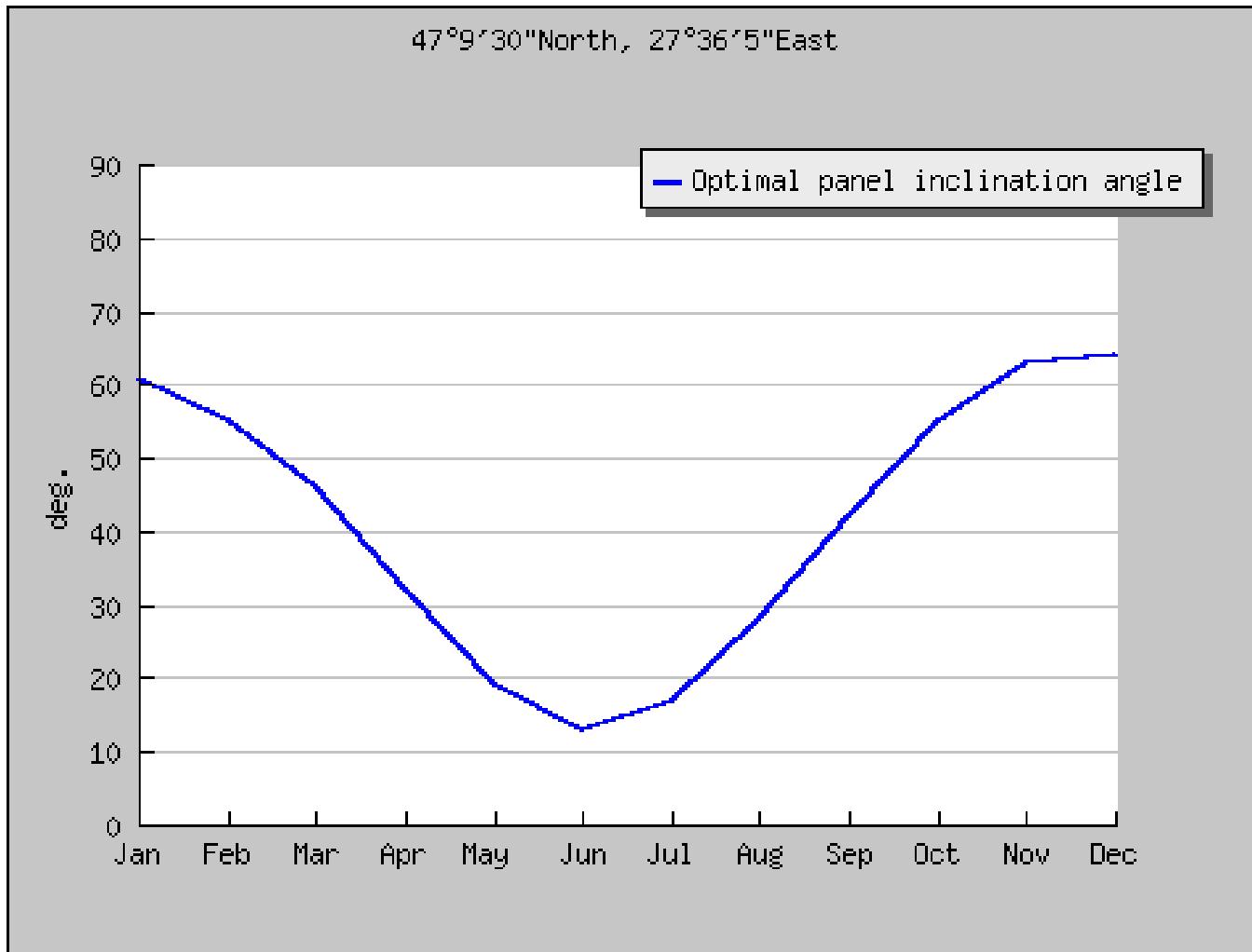


# Unghi optim de inclinare

- ▶ Panourile se orienteaza spre sud (**geografic**)
- ▶ Inclinarea pe verticala se poate calcula din considerente
  - geometrice
  - astronomice

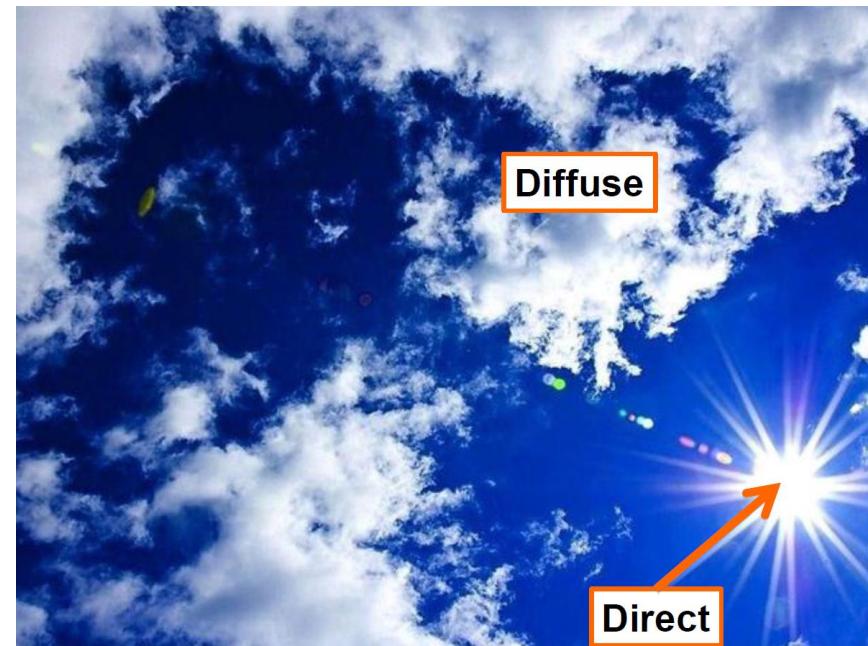
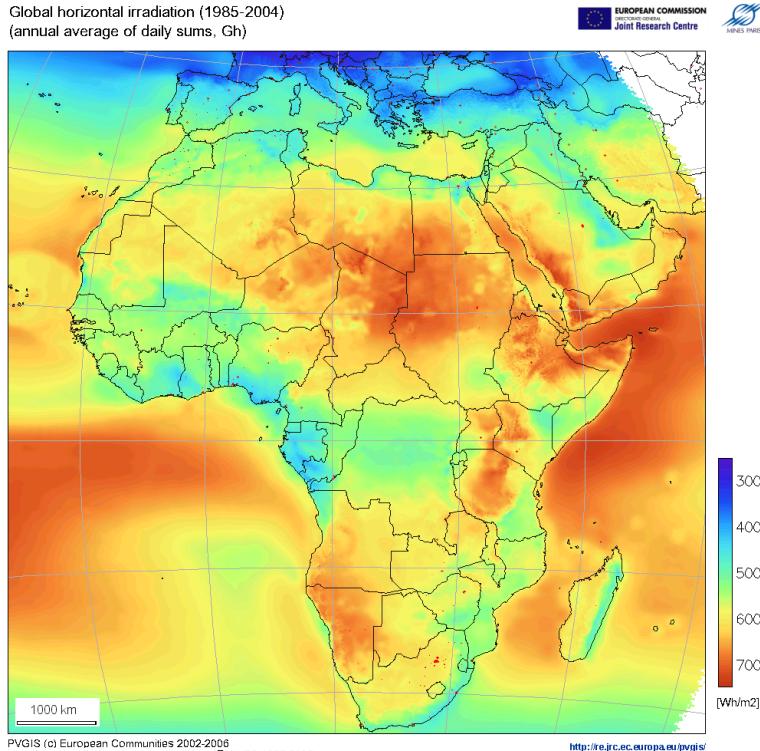


# lasi

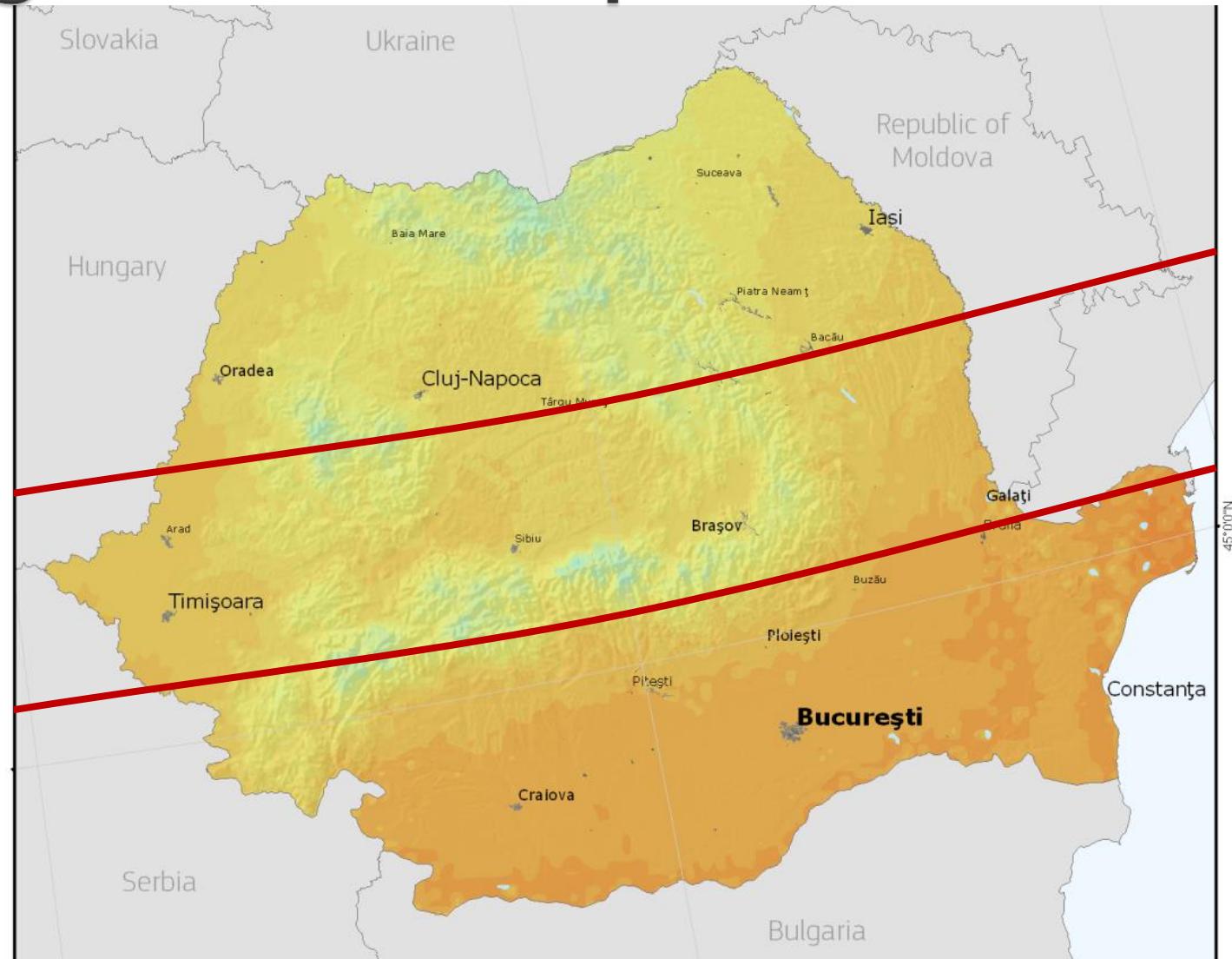


# Tip de sistem de urmarire

- ▶ depinde de tipul de sistem solar
  - cu concentrare
  - fara concentrare
- ▶ depinde de conditii meteorologice



# Energia solară disponibilă



# lasí

| Month | H <sub>h</sub> | H <sub>opt</sub> | H(90) | DNI  | I <sub>opt</sub> | T <sub>24h</sub> |
|-------|----------------|------------------|-------|------|------------------|------------------|
| Jan   | 956            | 1440             | 1410  | 1020 | 61               | -2.5             |
| Feb   | 1680           | 2350             | 2130  | 1670 | 55               | -1.4             |
| Mar   | 3310           | 4210             | 3330  | 3150 | 46               | 4.0              |
| Apr   | 4580           | 5150             | 3280  | 4380 | 32               | 10.6             |
| May   | 5900           | 5960             | 3070  | 5530 | 19               | 16.7             |
| Jun   | 6140           | 5900             | 2760  | 5530 | 13               | 20.0             |
| Jul   | 6320           | 6240             | 3010  | 6010 | 17               | 22.3             |
| Aug   | 5470           | 5960             | 3460  | 5630 | 28               | 21.4             |
| Sep   | 3720           | 4600             | 3390  | 3820 | 42               | 16.1             |
| Oct   | 2450           | 3570             | 3210  | 3000 | 55               | 10.2             |
| Nov   | 1260           | 2000             | 2010  | 1600 | 63               | 5.5              |
| Dec   | 802            | 1280             | 1310  | 959  | 64               | -0.8             |
| Year  | 3560           | 4070             | 2700  | 3540 | 35               | 10.2             |

| Mont<br>h | $H_h$ | $H_{opt}$ | $H(90)$ | DNI  | $I_{opt}$ | $T_{24h}$ |
|-----------|-------|-----------|---------|------|-----------|-----------|
| Jan       | 956   | 1440      | 1410    | 1020 | 61        | -2.5      |
| Feb       | 1680  | 2350      | 2130    | 1670 | 55        | -1.4      |
| Mar       | 3310  | 4210      | 3330    | 3150 | 46        | 4.0       |
| Apr       | 4580  | 5150      | 3280    | 4380 | 32        | 10.6      |
| May       | 5900  | 5960      | 3070    | 5530 | 19        | 16.7      |
| Jun       | 6140  | 5900      | 2760    | 5530 | 13        | 20.0      |
| Jul       | 6320  | 6240      | 3010    | 6010 | 17        | 22.3      |
| Aug       | 5470  | 5960      | 3460    | 5630 | 28        | 21.4      |
| Sep       | 3720  | 4600      | 3390    | 3820 | 42        | 16.1      |
| Oct       | 2450  | 3570      | 3210    | 3000 | 55        | 10.2      |
| Nov       | 1260  | 2000      | 2010    | 1600 | 63        | 5.5       |
| Dec       | 802   | 1280      | 1310    | 959  | 64        | -0.8      |
| Year      | 3560  | 4070      | 2700    | 3540 | 35        | 10.2      |

$H_h$ : Irradiation on horizontal plane (Wh/m<sup>2</sup>/day)

$H_{opt}$ : Irradiation on optimally inclined plane (Wh/m<sup>2</sup>/day)

$H(90)$ : Irradiation on plane at angle: 90deg. (Wh/m<sup>2</sup>/day)

DNI: Direct normal irradiation (Wh/m<sup>2</sup>/day)

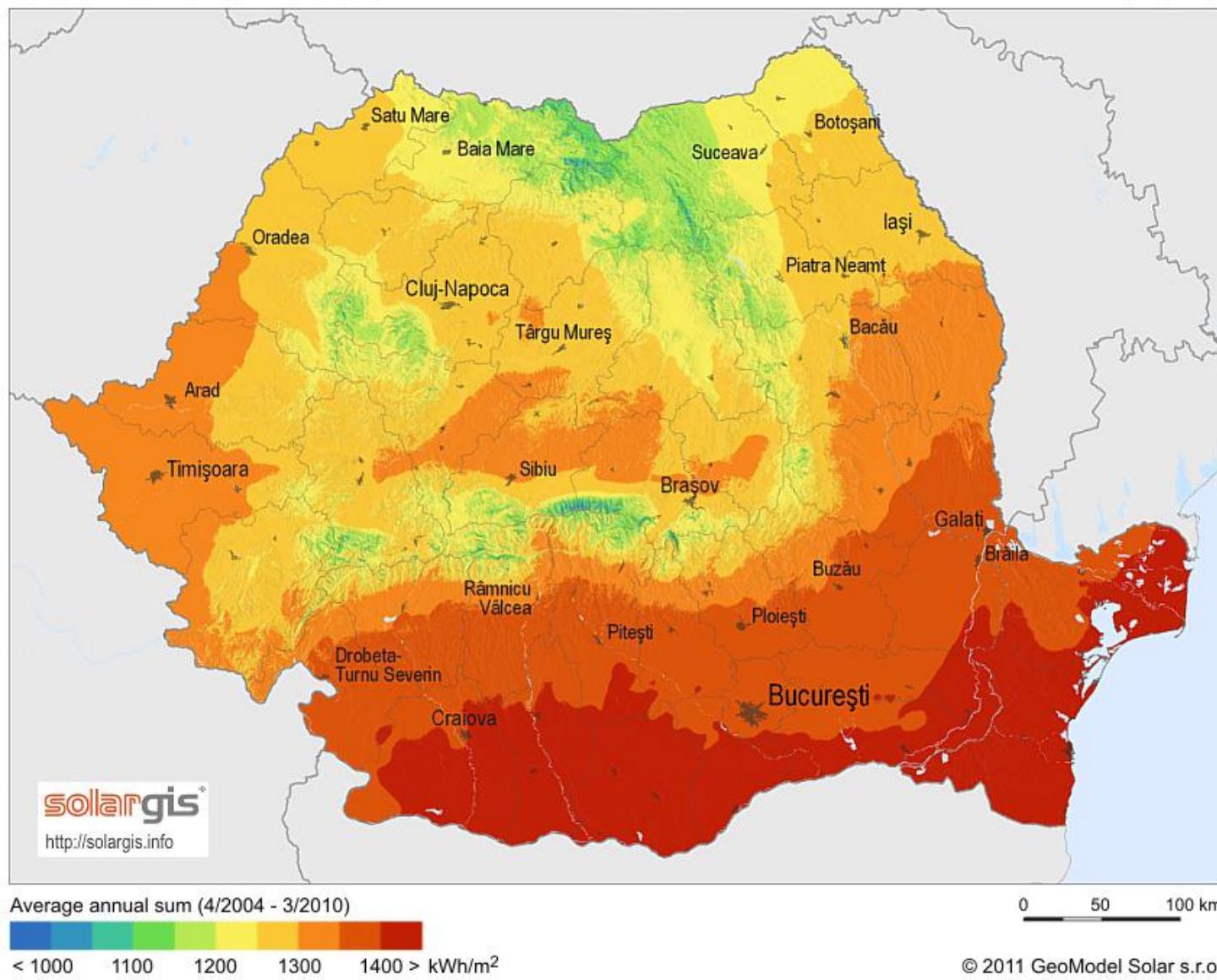
$I_{opt}$ : Optimal inclination (deg.)

$T_{24h}$ : 24 hour average of temperature (°C)

# Romania

Global horizontal irradiation

Romania



# 2019

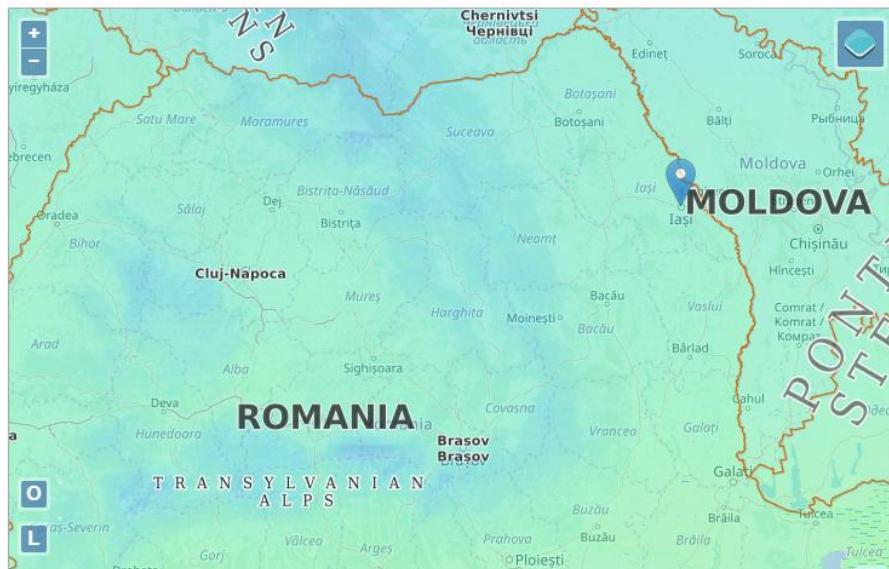
- ▶ Schimbare de:
  - adresa
  - aplicatie
- ▶ Alte modalitati de prezentare a rezultatelor
  - acces la date individuale 2007 – 2016
  - unitati de masura diferite (kWh/m<sup>2</sup>/**luna**)
  - lipsesc unele date (unghi optim lunar, H90)

[http://re.jrc.ec.europa.eu/pvg\\_tools/en/tools.html](http://re.jrc.ec.europa.eu/pvg_tools/en/tools.html)

# 2019

[re.jrc.ec.europa.eu/pvg\\_tools/en/tools.html#MR](http://re.jrc.ec.europa.eu/pvg_tools/en/tools.html#MR)

Home Tools Download Documentation About us News



Address: Eg.Ispira, Italy Go! Lat/Lon: Eg. 45.815 Eg. 8.611 Go!

Cursor:

Selected: 47.160, 27.585

Elevation (m): 57

Use terrain shadows:

Calculated horizon

Upload horizon file

[Download csv](#)

[Choose File](#) No file chosen

GRID CONNECTED

TRACKING PV

OFF-GRID

MONTHLY DATA

DAILY DATA

HOURLY DATA

TMY

## MONTHLY IRRADIATION DATA

Solar radiation database\*

PVGIS-CMSAF

Start year.\*

2007

End year.\*

2007

### Irradiation:

- Global horizontal irradiation
- Direct normal irradiation
- Global irradiation optimum angle
- Global irradiation at angle:

(0-90)

### Ratio:

- Diffuse/global ratio

### Temperature:

- Average temperature

[Visualize results](#)

[Download csv](#)

## MONTHLY IRRADIATION DATA: RESULTS

Radiation

Diffuse/Global

Temperature

Info

PDF

### Summary

#### Provided inputs:

Location [Lat/Lon]: 47.160, 27.585

Calculated

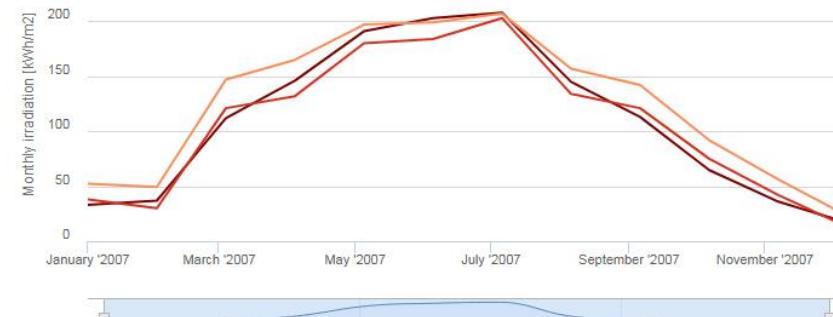
Horizon: PVGIS-CMSAF

Database used: PVGIS-CMSAF

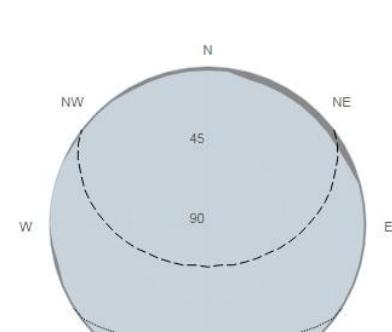
Start year: 2007

End year: 2007

### Monthly solar irradiation estimates



### Outline of horizon



# Iasi, date 2016

| Month | H <sub>h</sub> | H <sub>opt</sub> | DNI | D/G  | T <sub>24h</sub> |
|-------|----------------|------------------|-----|------|------------------|
| Jan   | 34.8           | 55.5             | 39  | 0.67 | -2.3             |
| Feb   | 50.5           | 72.2             | 50  | 0.63 | 4.1              |
| Mar   | 100            | 128              | 94  | 0.51 | 5.2              |
| Apr   | 147            | 167              | 141 | 0.43 | 12.4             |
| May   | 168            | 169              | 141 | 0.46 | 14.2             |
| Jun   | 184            | 180              | 162 | 0.4  | 20.2             |
| Jul   | 215            | 215              | 216 | 0.33 | 21.7             |
| Aug   | 174            | 191              | 185 | 0.35 | 20.4             |
| Sep   | 130            | 164              | 149 | 0.38 | 17               |
| Oct   | 55.2           | 73.7             | 54  | 0.59 | 6.6              |
| Nov   | 36.3           | 58.5             | 44  | 0.62 | 2.8              |
| Dec   | 29.6           | 49.2             | 35  | 0.68 | -1               |
|       |                |                  |     |      |                  |

# Iasi, date 2015

| Month | H <sub>h</sub> | H <sub>opt</sub> | DNI | D/G  | T <sub>24h</sub> |
|-------|----------------|------------------|-----|------|------------------|
| Jan   | 29.5           | 45.6             | 31  | 0.71 | -0.9             |
| Feb   | 50.6           | 73.5             | 53  | 0.61 | -0.2             |
| Mar   | 95.4           | 123              | 94  | 0.51 | 4.1              |
| Apr   | 142            | 160              | 134 | 0.44 | 9.1              |
| May   | 190            | 193              | 177 | 0.39 | 16.6             |
| Jun   | 209            | 205              | 200 | 0.35 | 19.7             |
| Jul   | 199            | 200              | 187 | 0.36 | 22.8             |
| Aug   | 173            | 189              | 180 | 0.35 | 22.6             |
| Sep   | 113            | 140              | 118 | 0.42 | 17.6             |
| Oct   | 73.7           | 107              | 85  | 0.51 | 8                |
| Nov   | 38.3           | 61.6             | 48  | 0.59 | 6.1              |
| Dec   | 34.7           | 64               | 52  | 0.6  | 1.1              |

# lasi, date 2016

| Month | H <sub>h</sub> | H <sub>opt</sub> | DNI | D/G  | T <sub>24h</sub> |
|-------|----------------|------------------|-----|------|------------------|
| Jan   | 34.8           | 55.5             | 39  | 0.67 | -2.3             |
| Feb   | 50.5           | 72.2             | 50  | 0.63 | 4.1              |
| Mar   | 100            | 128              | 94  | 0.51 | 5.2              |
| Apr   | 147            | 167              | 141 | 0.43 | 12.4             |
| May   | 168            | 169              | 141 | 0.46 | 14.2             |
| Jun   | 184            | 180              | 162 | 0.4  | 20.2             |
| Jul   | 215            | 215              | 216 | 0.33 | 21.7             |
| Aug   | 174            | 191              | 185 | 0.35 | 20.4             |
| Sep   | 130            | 164              | 149 | 0.38 | 17               |
| Oct   | 55.2           | 73.7             | 54  | 0.59 | 6.6              |
| Nov   | 36.3           | 58.5             | 44  | 0.62 | 2.8              |
| Dec   | 29.6           | 49.2             | 35  | 0.68 | -1               |
|       |                |                  |     |      |                  |

Hh: Irradiation on horizontal plane (kWh/m<sup>2</sup>/month)

H<sub>opt</sub>: Irradiation on optimally inclined plane (kWh/m<sup>2</sup>/month)

DNI: Direct normal irradiation (kWh/m<sup>2</sup>/month)

D/G: Ratio of diffuse to global irradiation (-)

T<sub>24h</sub>: 24 hour average of temperature (-C)

# lasi, date 2020

| Month | H(h)_m | H(i_opt)_m | Hb(n)_m | Kd   | T2m  |
|-------|--------|------------|---------|------|------|
| Jan   | 42.42  | 84.29      | 77.65   | 0.48 | 0.2  |
| Feb   | 61.58  | 97.82      | 82.35   | 0.48 | 3.4  |
| Mar   | 112.28 | 150.87     | 130.45  | 0.41 | 6.6  |
| Apr   | 175.65 | 205.88     | 199.18  | 0.33 | 11.3 |
| May   | 145.46 | 144.31     | 112.26  | 0.5  | 14.2 |
| Jun   | 181.37 | 173.26     | 148.87  | 0.44 | 21.4 |
| Jul   | 196.06 | 192.45     | 171.95  | 0.4  | 22.7 |
| Aug   | 186.03 | 202.9      | 189.24  | 0.36 | 23.6 |
| Sep   | 137.27 | 177.73     | 161.36  | 0.35 | 19.2 |
| Oct   | 69.29  | 97.6       | 70.7    | 0.55 | 13.6 |
| Nov   | 36.67  | 59.98      | 44.53   | 0.6  | 4.6  |
| Dec   | 20.75  | 31.54      | 20.21   | 0.74 | 2.4  |

# lasi, date 2020

| Month | H(h)_m | H(i_opt)_m | Hb(n)_m | Kd   | T2m  |
|-------|--------|------------|---------|------|------|
| Jan   | 42.42  | 84.29      | 77.65   | 0.48 | 0.2  |
| Feb   | 61.58  | 97.82      | 82.35   | 0.48 | 3.4  |
| Mar   | 112.28 | 150.87     | 130.45  | 0.41 | 6.6  |
| Apr   | 175.65 | 205.88     | 199.18  | 0.33 | 11.3 |
| May   | 145.46 | 144.31     | 112.26  | 0.5  | 14.2 |
| Jun   | 181.37 | 173.26     | 148.87  | 0.44 | 21.4 |
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| Nov   | 36.67  | 59.98      | 44.53   | 0.6  | 4.6  |
| Dec   | 20.75  | 31.54      | 20.21   | 0.74 | 2.4  |

H(h)\_m: Irradiation on horizontal plane (kWh/m<sup>2</sup>/mo)

H(i\_opt)\_m: Irradiation on optimally inclined plane (kWh/m<sup>2</sup>/mo)

Hb(n)\_m: Monthly beam (direct) irradiation on a plane always normal to sun rays (kWh/m<sup>2</sup>/mo)

Kd: Ratio of diffuse to global irradiation (-)

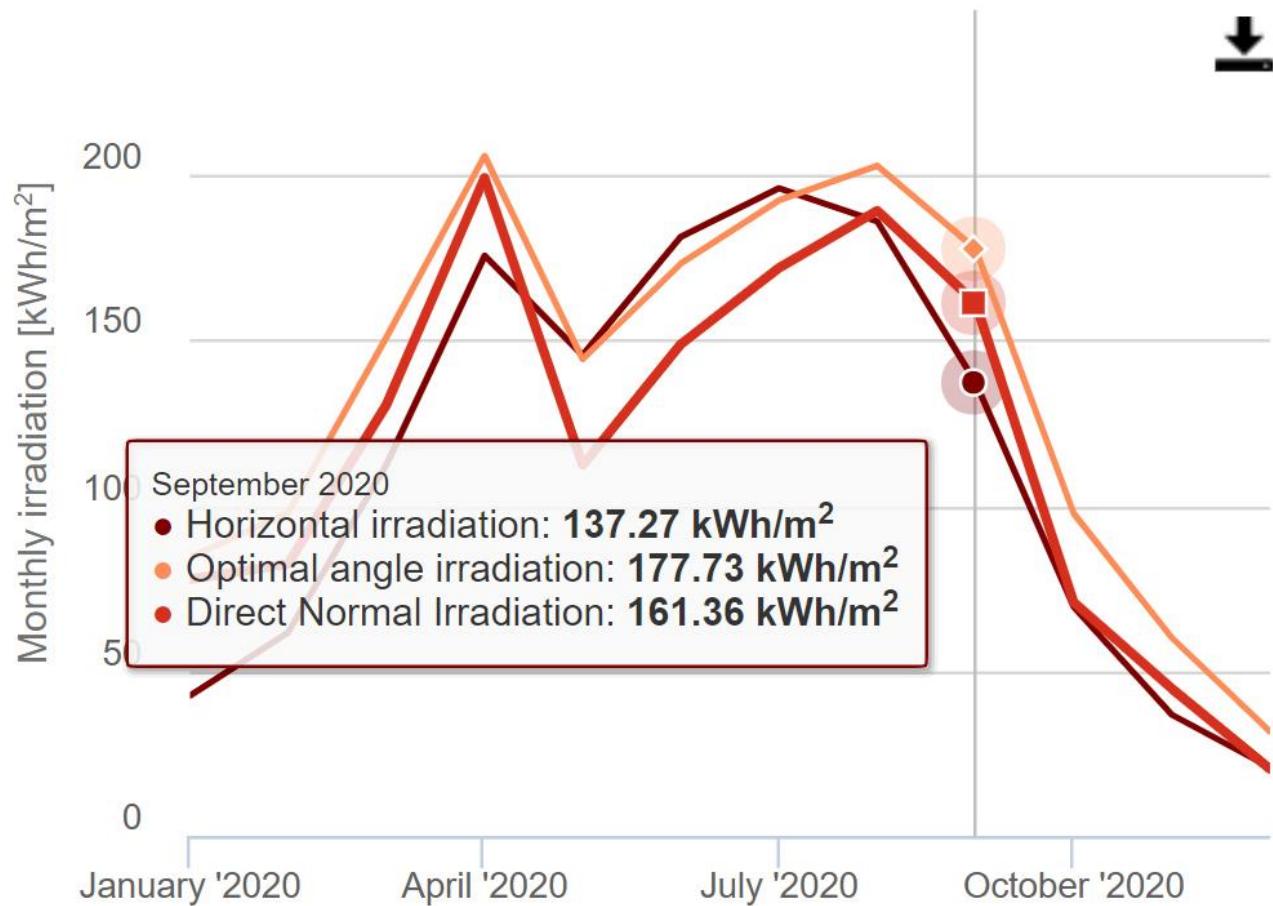
T2m: 24 hour average of temperature (degree Celsius)

# lasi, date 2020

## ► Lunar

- kWh/m<sup>2</sup>/luna
- Unghi optim  
(an) in csv

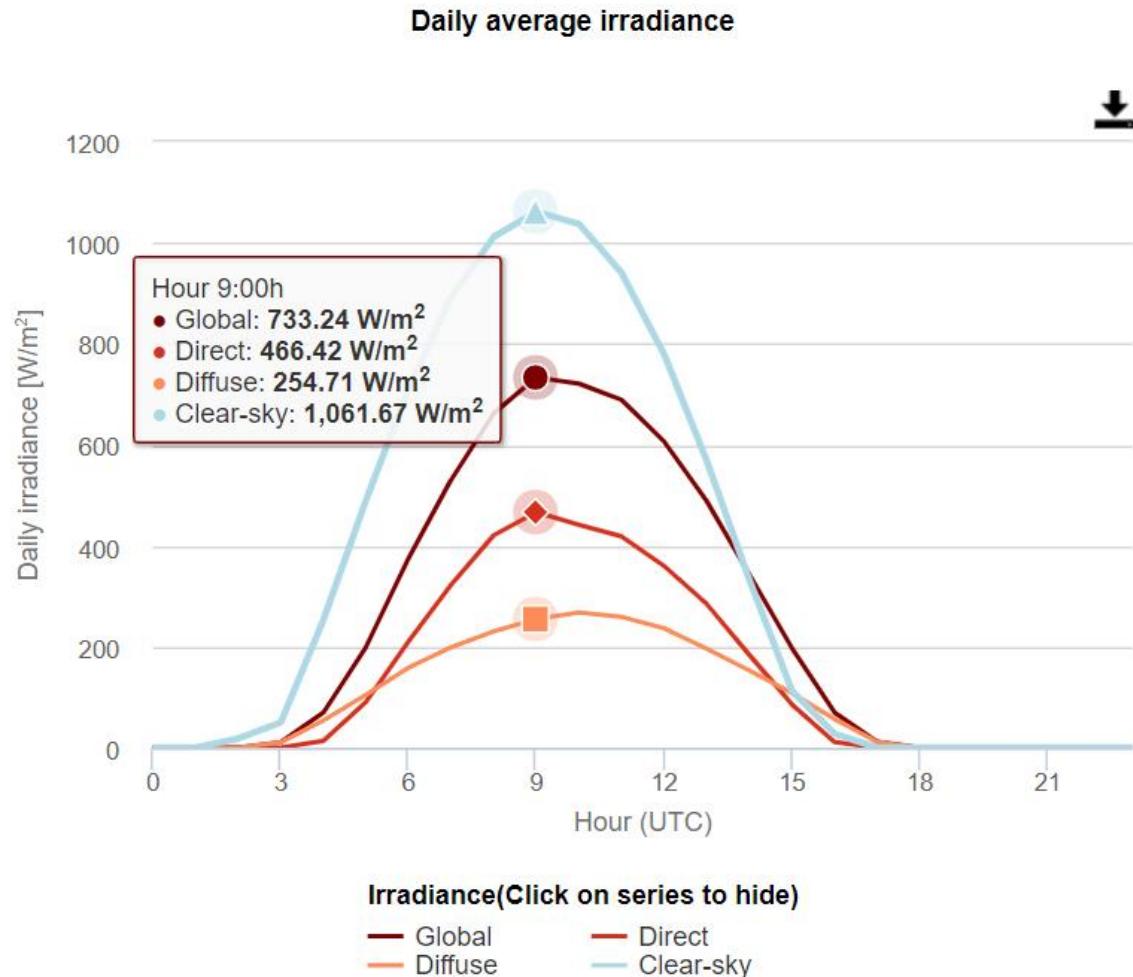
Monthly solar irradiation estimates



# lasi, date 2020

## ► Zi (mai)

- W/m<sup>2</sup>
- Ore in UTC!!  
(-3h)
- Clear sky –  
conditii  
ideale



# Contact

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- ▶ [http://re.jrc.ec.europa.eu/pvg\\_tools/en/tools.html](http://re.jrc.ec.europa.eu/pvg_tools/en/tools.html)
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